



# MONOLITHIC MICROWAVE PREAMPLIFIER FINAL REPORT

**JULY 1981** 

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#### 1. INTRODUCTION AND SUMMARY

This report describes TRW's monolithic microwave preamplifier development performed under contract No. NO0014-77-C-0645 for the Office of Naval Research. The report covers the period from 1 July 1979 to 31 December 1980; which corresponds to the third and final phase of this program.

Phases 1 and 2 covered periods 1 September 1977 to 31 March 1978 and 1 April 1978 to 30 June 1979, respectively, with corresponding Monolithic Microwave Preamplifier Technical Reports 1 and 2.

During Phase I of this program, TRW developed a computer model for GaAs Microwave Field Effect Transitors in order to study the noise and gain properties of such devices for different channel doping densities and geometry configurations. During Phase 2, TRW used this computer model to carry out the design of a low noise integrated preamplifier to operate at X-Band. The third and final phase of this contract encompasses the fabrication and characterization of this integrated preamplifier as well as its' active and passive components. The results of this third and final activity are the subject of the present report.

#### 2. SIGNIFICANT CHANGES FROM ORIGINAL DESIGN

Since the issue of "Technical Report No. 2," September 1979, the monolithic microwave preamplifier was subjected to one more redesign cycle for reasons of process feasibility and compatibility existing at the time.

The major changes from the original design were:

- a) Uniform doping profile of 1 x  $10^{17}$  cm<sup>-3</sup> for the FET devices instead of the selective doping profile of 4.0 x  $10^{16}$  cm<sup>-3</sup> in the channel and 5.0 x  $10^{17}$  cm<sup>-3</sup> under the source and drain contacts.
- b) Source and drain contact lengths of 15  $\mu m$  instead of 10  $\mu m$ .
- c) All inductor values have been modified to be less than 2.5 nH. This upper bound for inductance was found to be necessary in order to keep the electrical length of the inductor below one-quarter wavelength.
- d) The 10 nH inductor on the drains of stages 3 through 8 were replaced by tank circuits for the reason specified in c).

The FET devices with this new doping density and contact length under the biasing conditions  $V_{DD}=2.89~V$ ,  $V_{GG}=-1.90~V$ , and  $I_d=4.7~mA$  had a set of S-parameters in the frequency range of 8 to 11 GHz as predicted by TRW's FET computer model (Table 2-1).

Table 2-1. Predicted S-Parameters for FET Devices

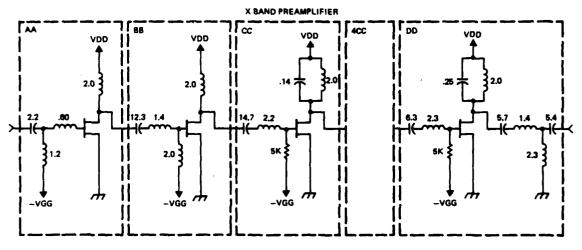
F (GHz)	S <sub>11</sub>	<sup>S</sup> 21	S <sub>12</sub>	S <sub>22</sub>
8	0.848 -70.6	1.417 121.4	0.084 53.2	0.930 -24.0
9	0.826 -76.9	1.340 [116.0	0.090 50.3	0.922 -26.6
10	0.805 -82.6	1.267 111.0	0.095 47.8	0.915 -29.0
11	0.787 [-87.9	1.199 106.4	C.100 45.6	0.909 <u>-31.5</u>

The noise figure, optimum source reflection coefficient for minimum noise, and the noise resistance of the FET devices were predicted as shown in Table 2-2.

Table 2-2. Predicted Noise Parameters for FET Devices

F (GHz)	NF (dB)	Γ <sub>s</sub> opt	$R_n(\Omega)$
8	3.02	0.706 33.4	12.0
9	3.28	0.681 37.4	12.0
10	3.53	0.658 41.4	12.0
11	3.76	0.637 45.3	12.0

With these scattering and noise parameters, the preamplifier was redesigned and computer-optimized; the resulting schematic is shown in Figure 2-1 with the preamplifier's predicted performance (Table 2-3).



TES:
ALL RESISTOR VALUES ARE IN OHMS
ALL INDUCTOR VALUES ARE IN NANOMENRIES
ALL CAPACITOR VALUES ARE IN PICOFARADS
ALL FET DEVICES

GATE LENGTH = 1 

GATE SOURCE SEPARATION = 1 

GATE ADRAIN SEPARATION = 1 

BOURCE CONTACT LENGTH = 15 

DOPING UNDER CONTACTS = 1 

CHANNEL DOPING DENSITY = 1 

CHANNEL DEPTH = 0.20 

ME IN DOMING VALUES

CHANNEL DEPTH = 0.20 

CHANNEL

Figure 2-1. Preamplifier Schematic Diagram

Table 2-3. Preamplifier's Predicted Performance

F (GHz)	Gain (dB)	Noise Figure (dB)
8	28.4	5.6
9	28.4	5.5
10	31.2	5.6
11	29.2	5.7

The comparison of actual and predicted performances and the analysis of discrepancies will be covered in Sections 5 and 6, respectively.

#### 3. PROCESS DEVELOPMENTS

The processing of monolithic microwave integrated circuits using GaAs materials and device technology is the primary objective of this program. During the early part of this program, work was aimed at refining and standardizing the process technology. Those aspects of the technology considered to be of particular importance to optimize microwave analog integrated circuit performance were identified and addressed. An attempt has been made to define a standard process for GaAs analog IC fabrication; this is a difficult task due to the rapid evolution of technology. The optimized process sequence which was used to fabricate the microwave IC preamplifier is shown in Figure 3-1, and major processing steps illustrated in Figure 3-2.

#### 3.1 MATERIAL PREPARATION

The fabrication of GaAs integrated circuits using a mesa isolation process has been achieved using three approaches:

- Epitaxial technology
- Ion-implantation into epitaxially grown, undoped buffer layers on semi-insulating substrates
- Ion-implantation into semi-insulating substrates.

The first approach is a direct extension of early techniques used to fabricate high performance discrete GaAs devices. The second technique has been used to offset the poor quality of early semi-insulating substrates. With recent improvements in substrate materials development and characterization, the third approach is emerging as the most desirable method for fabricating high density circuits with small device geometries. Secondary ion mass spectroscopy (SIMS) has been a key element in the development of improved substrate materials and in the understanding of the empirical procedures used to select acceptable crystals for the direct ion-implantation approach.

STEP NO.	OPERATION
1.	CRYSTAL QUALIFICATION
2.	CLEAN WAFERS
3.	SILICON IMPLANTATION - 3 x 10 <sup>12</sup> cm <sup>-2</sup> , 100 keV
4.	CAP AND ANNEAL — SIO <sub>7</sub> /SI <sub>3</sub> N <sub>4</sub> , 860°C, 30 MINUTES
5.	STRIP CAP AND CLEAN WAFERS
6.	PHOTORESIST
7.	mesa isolation mask
	MESA ETCH
9.	CHECK ISOLATION
10.	STRIP PHOTORESIST AND CLEAN WAFERS
11.	PHOTORESIST
12.	OHMIC CONTACT MASK
13.	CLEAN WAFERS
14.	DEPOSIT OHMIC METALS - AUGONIAU
15.	metal liftoff
16.	ALLOY CONTACTS
17.	TEST PROBE FET - I AND V AT 9 POINTS
18.	CLEAN WAFERS
19.	DEPOSIT SILOX
20.	PHOTORESIST
21.	fet gate and first level interconnect mask
22.	ETCH SILOX
23.	DEPOSIT GATE METALS — CIPLAUPI
24.	METAL LIFTOFF
25.	SINTER GATE METALS
26.	STRIP SILOX AND CLEAN WAFERS
27.	TEST PROBE FET - I DSS AND V <sub>P</sub> AT 9 POINTS
28.	DEPOSIT SILOX
29.	PHOTORESIST
30.	VIA MASK
31.	ETCH VIAS
32.	STRIP PHOTORESIST AND CLEAN WAFERS
33.	DEPOSIT BOND METALS — TIAI
34.	PHOTORESIST
35.	INTERCONNECT AND BOND PAD MASK
36.	ETCH METALS
37.	ALLOY METALS
38.	TEST PROBE FET AND RESISTOR BAR - IDSS' Vp. Gm'
	R <sub>SH</sub> AND R <sub>C</sub> AT 9 POINTS

Figure 3-1. Standard GaAs Microwave Integrated Circuit Process Sequence

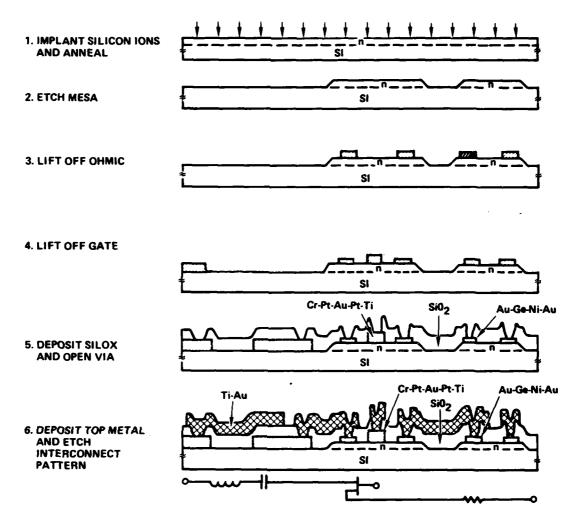


Figure 3-2. GaAs Standard Mesa Process

#### 3.1.1 Substrate Qualification

The standard qualification procedure for a crystal shown in Figure 3-3 uses wafers from both ends of the crystal ingot for thermal conversion and standard implantation tests. For the thermal conversion tests, the samples are coated with a  $\mathrm{Si_3N_4/SiO_2}$  cap and annealed at 850°C for 30 minutes in  $\mathrm{N_2}$ . After stripping the films, capacitance-voltage measurements are made on aluminum Schottky diodes formed on the wafer to determine if the material converts from semi-insulating to conducting. It has been TRW's experience that material which does not pass this first test will give irreproducible ion-implanted profiles. Additional samples are ion-implanted with Si+ ions at an energy and dose similar to the one being used for device

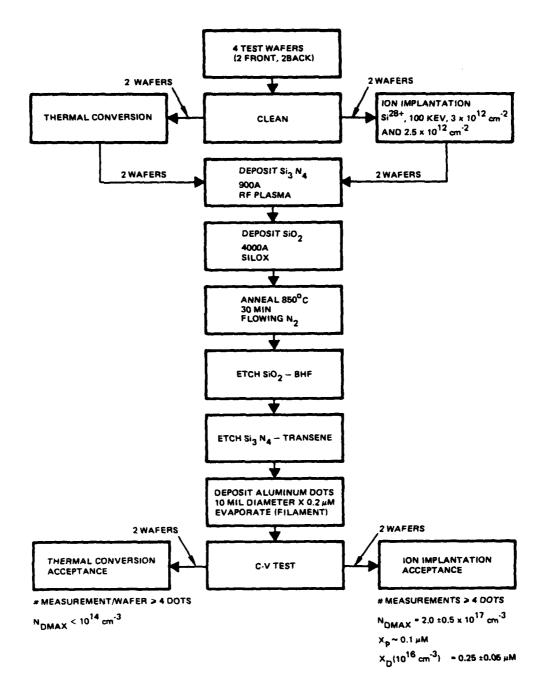


Figure 3-3. GaAs Crystal Qualification Procedure

fabrication (typically 100 keV and 3 x  $10^{12}$  cm $^{-2}$ ). The samples are capped, annealed, and stripped, and C-V measurements are conducted again. Careful inspection of the resulting dopant profiles determines if the material will produce sharp profiles or profiles with deep "tails" which are inadequate for device fabrication. Figure 3-4 compares an acceptable profile versus nonacceptable profiles.

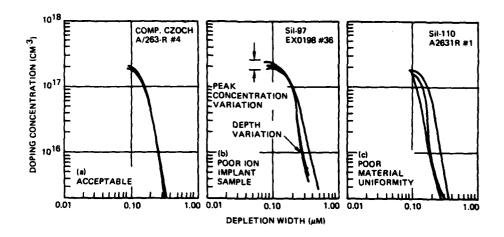


Figure 3-4. Concentration Profiles for Silicon-Implanted GaAs Substrates

SIMS measurements have been conducted on as-received wafers, wafers following the thermal conversion test, and wafers following the silicon implantation test. The SIMS studies were conducted by TRW and Charles Evans and Associates. These studies have clarified the reasons for the wide variability of Cr-doped semi-insulating material. The material variability is related to the variability of background donors (typically silicon) ranging from  $10^{15}$  to  $10^{17}$  cm<sup>-3</sup> and the redistribution of chromium during thermal annealing. During thermal cycling, chromium atoms are found to pile up at the surface ( $10^{19}$  cm<sup>-3</sup>, 50 to 100 Å) and to deplete just below the surface, (100 to 1500 Å). If the depleted chromium concentration falls below the background doping concentration, thermal conversion is observed. Variations in the tail region of ion-implanted profiles result from the interaction with the background donors and the profile of the redistributed chromium atoms.

Figure 3-5 shows an example of the SIMS evaluation of a thermally-annealed, unimplanted Cr-doped GaAs substrate. The background silicon doping

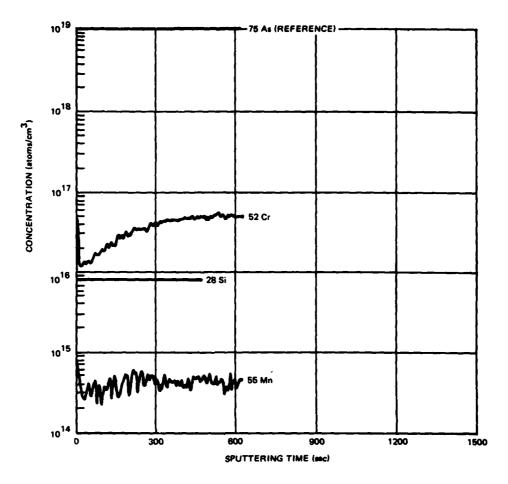


Figure 3-5. SIMS Impurity Profiles for Unimplanted, Cr-Doped GaAs Substrates

is seen to be 5 x  $10^{15}$  cm<sup>-3</sup>. The bulk chromium concentration was high enough to prevent surface conversion under heat treatment. The profile of a typical silicon implantation (peak concentration of 1.5 to 2 x  $10^{17}$  cm<sup>-3</sup>) into this wafer will be significantly disturbed as the implanted concentration falls below 5 x  $10^{16}$  cm<sup>-3</sup>.

The results of the SIMS study suggest that the best Cr-doped substrates come from ingots with a low background donor concentration (1 x  $10^{15}$  cm $^{-3}$ ) and a low chromium doping concentration (5 x  $10^{15}$  cm $^{-3}$ ). This hypothesis is supported in part by the improved uniformity and reproducibility observed for ion-implanted LEC wafers which contain no intentional chromium doping.

Most wafers processed for this program were Cr-doped horizontal Bridgeman-grown material obtained from Crystal Specialties. Sample wafers

from seven different suppliers were evaluated; complete ingots were purchased only when the corresponding wafers passed the standard qualification tests, unacceptable samples generally failed the thermal conversion tests following our 850°C annealing treatment.

#### 3.1.2 <u>Ion-Implantation</u>

The active layer for FET's and resistors in integrated circuits is formed by ion-implantation. The pinchoff voltage, device current, and semiconductor resistivity depend on the implanted dose, range, and profile as well as the activation efficiency. The uniformity of the concentration profile of the implanted donors depends on the implanted species, the substrate quality, and the annealing techniques used to remove the implantation damage. TRW has selected Si+ as the implanted species, since it can be implanted into substrates at room temperature with good activation and minimal redistribution with heat treatment.

The annealing technique in the standard process uses 900 Å of plasmadeposited  $\mathrm{Si}_3\mathrm{N}_4$  covered with 4000 Å of  $\mathrm{SiO}_2$ . This annealing cap has provided high doping efficiencies and has been used with temperatures up to 900°. The standard annealing conditions for N-Channel implantation are 850° for 30 minutes. For highly doped N+ contact implants, 900°C annealing temperature is used to achieve high activation. Figure 3-6 shows the variations of the doping efficiency versus implantation dose and annealing temperature for Si+ ions at 100 keV,  $\mathrm{Si}_3\mathrm{N}_4/\mathrm{SiO}_2$  cap, and 30 minute annealing time.

#### 3.1.3 Characterization

#### N-D Profile

After ion-implantation, capping, and annealing, each wafer is subject to C-V measurements to determine the doping profile; aluminum is E-beam deposited through a metal mask to form a Schottky barrier diode. A typical doping profile obtained by C-V measurements on an aluminum Schottky diode is shown in Figure 3-7. In the capacitance-voltage measurement of a Schottky diode, the concentration is expressed as

$$N = \frac{c^3}{A \varepsilon \varepsilon_0 q} \times \frac{dV}{dC}$$

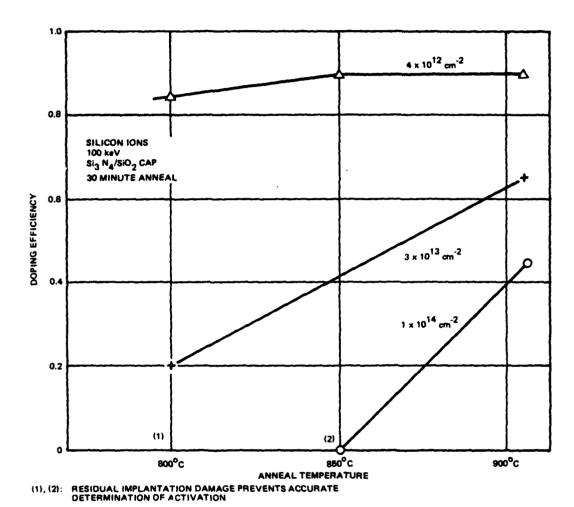


Figure 3-6. Doping Efficiency for Silicon Ion-Implantation

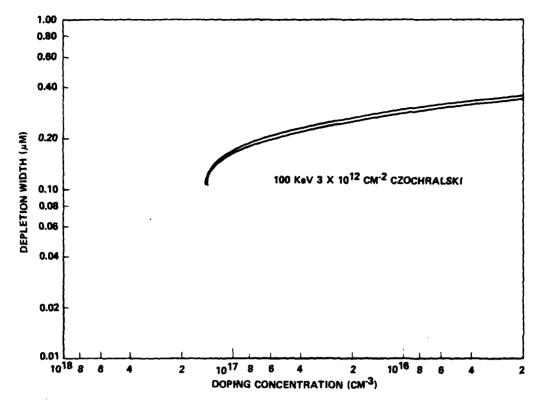


Figure 3-7. Capacitance-Voltage Profile for Ion-Implantation into Liquid Encapsulated Czochralski Grown Substrate

Where the capacitance C is the average of two differential capacitance measurements,  $\epsilon$  is the dielectric constant,  $\epsilon_0$  is the permittivity of free space, q is the electronic charge, and A is the diode area. The variation of diode capacitance with applied voltage is used to determine the electrical thickness of the implanted layer. The depletion width is expressed as

$$W = \frac{\varepsilon \varepsilon_0 A}{C}$$

The C-V data is computed and plotted automatically on a profiler.

# Mobility Measurements

the same

The N-D profile obtained by C-V techniques can be verified by mobility and concentration measurements. The mobility and doping profile is measured by a combination of the Van der Pawe method and etch back technique. The Hall sample is fabricated by mesa etch followed by ohmic contact metal liftoff

and sintering. The resistivity is then measured by the Hall effect technique; a layer of anodic oxide is grown and the thickness is determined by ellipsometer. This oxide is then removed in a  $\mathrm{HC1:H_2O}$  (1:1) solution. The active layer removed is empirically determined to be 2/3 of the oxide thickness. Resistivity is measured again. By repeating this resistivity measurement and anodic etching of the active layer, the mobility and concentration profile can be determined. A typical mobility and concentration profile is shown in Figure 3-8.

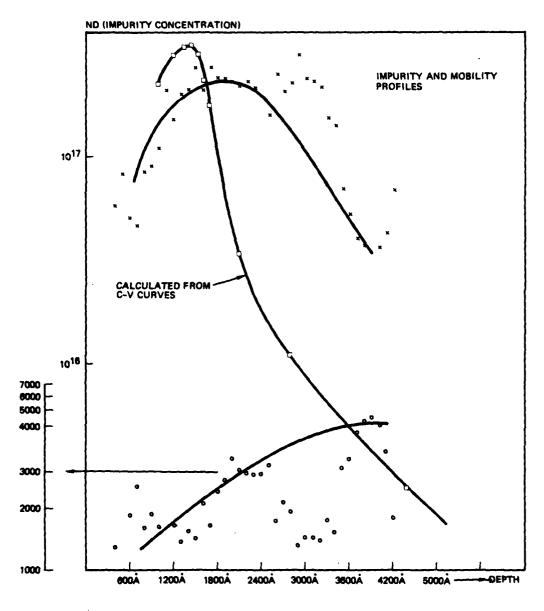


Figure 3-8. Impurity Concentration and Mobility Profile

## Resistivity and Saturation Current of Probe FET Measurements

The mobility and impurity concentration profiling by Hall measurement technique is very tedious and not practical in characterizing each wafer. An economical and simple way to monitor the quality of ion-implantation is by measuring the sheet resistivity and FET saturation current after ohmic contact formation.

#### Resistor Bar Measurements

The channel sheet resistivity is a valuable process control parameter as well as a necessary design parameter for resistors. This parameter is measured using a 50  $\mu m$  wide resistor bar consisting of three ohmic contacts separated by a one square channel region and a three squares channel region. Figure 3-9 shows the sheet resistivity distribution across the wafer. The variation is less than 10 percent which indicates the uniformity of ion-implantation. Of the same importance as sheet resistivity is the saturation current measurements. The saturation current of an FET can serve as an indication of good or bad ohmic contacts and quality of the wafers. As shown in Figure 3-9, the average saturation current is 44.5 mA for a 100  $\mu m$  FET. The standard deviation is less than 10 percent across the wafer.

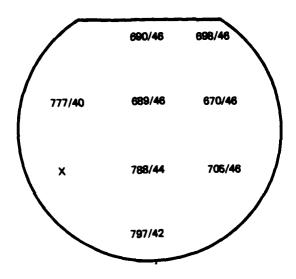


Figure 3-9. Sheet Resistivity and Saturation Current of 100 µm FET Across a Wafer of 1.5 in. in Diameter

#### 3.2 ACTIVE DEVICES

FET's are the only active devices used in the X-band low noise amplifier. The primary development effort was directed toward improving the design criteria and minimizing parasitics to achieve the desired circuit performance. The device development was concentrated in two specific areas: 1-micron gate fabrication and improving ohmic contacts.

# 3.2.1 Device Isolation

The first step of the process sequence after ion-implantation and annealing is device isolation. The device isolation is accomplished by mesa etch in a solution of HF:  $H_2O_2$ :  $H_2O$  (1:1:3) at room temperature. This etch is known to be isotropic and has a gradual slope. These mesas are etched at a rate of about 1.8 micron per minute. Photolithographic patterns are used to delineate the mesas during this isolation etch. The depth of etch must be sufficient to go completely through the active layer to ensure device isolation.

# 3.2.2 Ohmic Contact Metallization

Ohmic contacts to GaAs have been extensively studied at TRW on an internally funded program and in other laboratories. The objective of these studies was to achieve metal semiconductor contacts which exhibit linear current-voltage characteristics and a contact resistance low in comparison to the resistance of the semiconductor device. This, in principle, is achieved either by:

- The choice of a metal which forms a low barrier with the semiconductor (thermionic emission)
- A high concentration region in the semiconductor near the contact so that the barrier is readily penetrated by quantum mechanical tunneling.

The tunneling approach was taken for the GaAs materials. In general, the objective was to reduce the specific contact resistance  $r_c$  to a value below  $10^{-5}$  ohms-cm<sup>2</sup> by doping the semiconductor.

The low specific contact resistance was achieved by doping the GaAs with Ge from an AuGe contact. The Ge, an amphoteric dopant, goes substitutionally on vacant Ga sites to form donors. The doping occurs as the Au and Ge alloy with the topmost layer of the GaAs. When the GaAs-AuGe alloy

solidifies, Ge is distributed in the GaAs regrowth layer. Contacts formed in this manner yield a low ( $\approx 10^{-5}$  ohm-cm<sup>2</sup>) specific contact resistance.

The basic AuGe contact metallization has been used with and without variations in the structure. The variations included the use of additives such as Ag, In, Pt, and Ni to reduce the surface tension and minimize "balling" in the contact areas. For many of the early devices and the early circuit development, as shown in the process flow, the AuGe contact was used with a simple coating of Au for bonding purposes. These contacts are not uniform throughout the contact area or across the wafer but had many islands of contact metal in the ohmic contact region. This causes the ohmic contact resistance to be higher than that achievable with a more uniform contact.

The nonuniformity was, in part, attributed to cleanliness of the wafer prior to metal deposition and to localized segregation of metal clusters due to the high surface tension of the metal. A cleaning technique which removed surface oxides was developed and employed during the circuit fabrication. This technique uses dilute HCl to remove the oxides. The new cleaning procedure gave a higher yield of good contacts across a given wafer but the balling still existed. Balling was eliminated with the use of our present metal configuration and different sintering conditions. Metals with various thicknesses of Au, Ge, Au (top metal), and Ni or Pt were investigated. The system of Au-Ge-Ni-Au was employed in the monolithic circuits developed on this program.

After mesa etch, photoresist is coated onto the substrate and ohmic contact patterns are exposed and developed. 1700 Å of ohmic contact metal is then E-beam deposited and the excess metal is lifted off followed by alloying in nitrogen at 400°C for 30 seconds. Typical values of specific contact resistances achieved is of the order of 2 x  $10^{-5}$  ohm cm<sup>2</sup> or less.

# 3.2.3 <u>Gate Metallization (First Level Metal)</u>

In the early stage of this program, our standard Schottky contact metallization was evaporated aluminum. This metal has been widely used in discrete GaAs MESFET's. It is easily evaporated, well defined by the standard liftoff techniques, adheres well to GaAs, and makes a good Schottky junction. The major drawback for this metal system is the difficulty

experienced in trying to make consistent, reliable, low-resistance via connections between metal-1 and metal-2. This problem is caused by the rapid oxidation of aluminum during deposition and subsequent processing steps. After exploring several alternatives, the Cr-Pt-Au metal system was adopted. This process has been refined such that we can routinely fabricate monolithic microwave integrated circuits with 1-micron gate length FET's.

The gate metal is 4500~Å thick and is produced by silox assisted photoresist liftoff technique. After ohmic contact formation, 4000~Å silox is deposited. Photoresist is spin coated and gate patterns are delineated. Silox is intentionally undercut to assist the gate metal liftoff. Cr-Pt-Au-Pt is then E-beam-deposited and the excess metal is lifted off in acetone.

Figure 3-10(a) shows the interdigited 360-micron FET with each finger of 90 microns. Figure 3-10(b) depicts a 1-micron gate line crossing over the mesa step. The measured metal resistivity is  $4.2 \times 10^{-6}$  ohm-cm and the sheet resistivity is 0.01 ohm per square. A typical I-V characteristics of the interdigited 360 micron FET is shown in Figure 3-11.



Figure 3-10 (a) Microphotograph of 360 µm Interdigeted FET (750X)

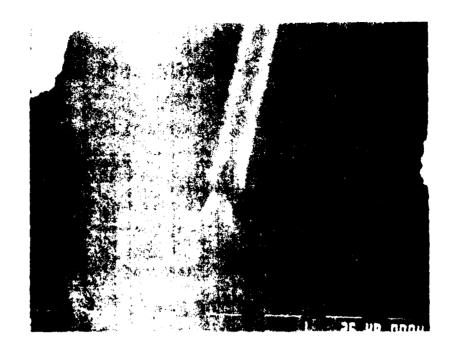


Figure 3-10 (Figure 3-10 (Figur

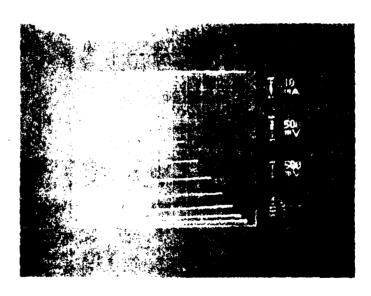


Figure 3-11. The or a 360 pm (intensity) ted FET

#### 3.3 PASSIVE COMPONENTS FABRICATION

Passive devices used in the X-band low noise preamplifier include resistors, capacitors and inductors. Two types of resistors, thin film and implanted bulk, were investigated. The capacitors are of metal-oxide-metal structure. The most serious problem encountered in IC fabrication was the cracking of silox in the large capacitors because of stress induced by thick aluminum deposited. This problem was solved by changing the top metal system from Ti-Al to Ti-Au, and using a thin layer of Ti as the topmost metal of the gate metal system. The inductor fabrication etch is straightforward. It uses a wet etch process to define the inductor patterns because of the undercut nature of wet etch process, metal thickness cannot be too thick. Our standard process uses 500  $\mathring{\rm A}$  of titanium and 1  $\mu{\rm m}$  gold.

# 3.3.1 Resistors

Two types of resistors are used in fabricating GaAs IC's: Ion-implanted bulk resistors and thin film resistors. The n-doped (ion-implanted) GaAs material used as the active region of the MESFET has a sheet resistance in the order of 750  $\Omega$ / $\Box$  and is appropriate for noncritical high value resistors. Deposited Cr-Ge which sheet resistance of 100 to 200  $\Omega$ / $\Box$  can be used where precision resistors are required. These thin film resistors can be accurately trimmed and have good temperature and radiation stability. The penalties paid for the improved properties are added process complexity and additional metal evaporation. Since precise resistor values were not required the implanted bulk resistors were used.

# 3.3.2 Capacitors

A metal-oxide-metal capacitor plan view and cross-section are shown in Figure 3-12. The bottom plate of the capacitor is the same as the gate metal. After gate metal (or first level metal) lift off and sintering, silox is pyrolytically deposited to a thickness of 3000  $\mathring{\rm A}$  followed by top metal deposition. The top capacitor plate is defined by photoresists pattern and etching the top metal.

The control of the capacitance value depends on the precision of silox deposition and the capacitor plate definition. Although a wet chemical etch process is employed to pattern the plate, the variation of plate size

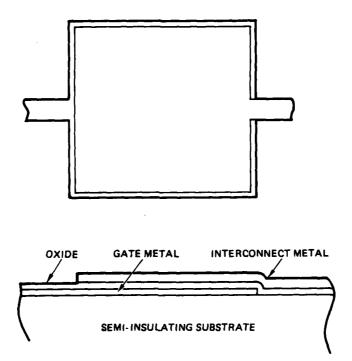


Figure 3-12. Metal-Oxide-Metal Capacitor

due to undercut is negligible. Most of the variation of capacitance value is due to silox thickness variation. The relative dielectric constant of silox is assumed to be 4.0.

A comparison of capacitance value measured and the design value is shown in Table 3-1, typically the discrepancy is within 10 percent of the designed value.

Initially, the top metal consisted of 500 Å Ti and 10,000 Å Al and the bottom plate was Cr-Pt-Au-Pt. The topmost layer of the bottom plate serves as a barrier to prevent Al alloying with gold in the gate in the via interconnect area. Because of the poor adhesion between platinum and silox, the stress induced by thick aluminum causes the silox to crack and peel off from the surface of bottom plate. Since the stress increases with the size of the plate, this cracking and peeling occurred mostly on the large capacitors. By adding a thin layer of titanium on top of platinum to improve the silox adhesion and change Ti-Al system to Ti-Au we are able to eliminate this problem.

Table 3-1. Measured Capacitance Value as Compared to the Designed Value

SAMPLES	CCALCULATED (pf)	CMEASURED (pf)	% ERROR
ONRPA-20	0.55	0.53	-3.6
	2.94	2.60	-11.6
	0.11	0.14	+27.3
ONRPA-38	0.19	0.21	+10.5
	0.42	0.38	+9.5
	1.14	0.92	+19.3
L3	0.82	0.76	-7.3
	0.27	0.27	0.0

IN CALCULATING OXIDE CAPACITANCE, RELATIVE DIELECTRIC CONST OF 4.0 IS USED

# 3.3.3 Inductors Process Development

At the beginning of this program, the standard metallization thickness for the top metal interconnection and inductor fabrication was 0.5 µm. It was recognized that this is less than one skin depth even at 12 GHz and therefore not optimum for microwave loss. However, the standard evaporation and pattern definition techniques made fabrication of thicker layers difficult. A straightforward extension of the standard processing has been successful in increasing the top metal thickness to 1 micron. This is approximately one skin depth at 10 GHz. Because fields can extend into the line from both sides, a thickness of 2 or more microns is desired for optimum inductor Q at 10 GHz. Doubling the thickness will nearly double the Q. However, to regain the top metal thickness will require longer etch time. Consequently, more undercut occurred and the line width is narrower. As a compromise 1 µm thick metal is used. Figure 3-13 shows a 2-1/4 turn inductor pattern. Gate metal is used as a center feed to the center of the inductor.

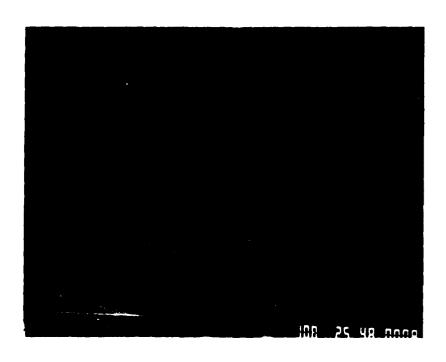


Figure 3-13. Microphotograph of a 2-1/4 Turns Inductor Pattern. The Magnification is 1000X

In order to evaluate the quality of the metallization at microwave frequencies, a series of LC test patterns such as those shown in Figure 3-14 were fabricated and measured. The S-parameters of the test pattern shunting a  $50\Omega$  line were measured to determine the equivalent circuit. The first order values for R, L, and C in a series connection were determined from the transmission resonance characteristic (DeLoach method). A more complex model was then derived which includes the parasitic bonding inductances and parasitic capacitance of the planar spiral inductor. This derivation uses COMPACT to optimally fit the equivalent circuit element values to the measured S-parameters. An example of the theoretical, first order, and complete equivalent circuits is shown in Figures 3-15 and 3-16. This data was generated for a test inductor pattern having a 1  $\mu$ m thick metallization pattern. The DeLoach model is shown to give a reasonable approximation to the computer optimized value. However, the theoretical value is approximately 0.7 nH less than that measured. Excess wire bond inductance is suspected to be at least part of the explanation. In the computer optimization, it is difficult to separate the wire bond inductance from the inductor pattern. If it is assumed that the added inductance is a

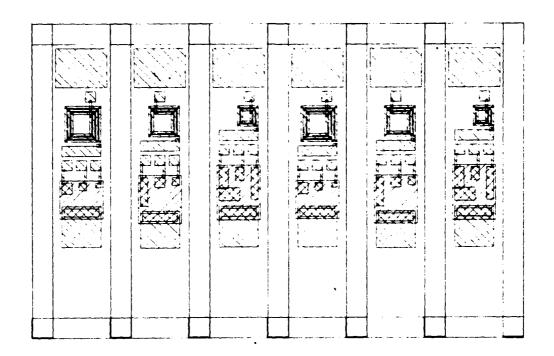


Figure 3-14. Layout of the L-C Test Patterns

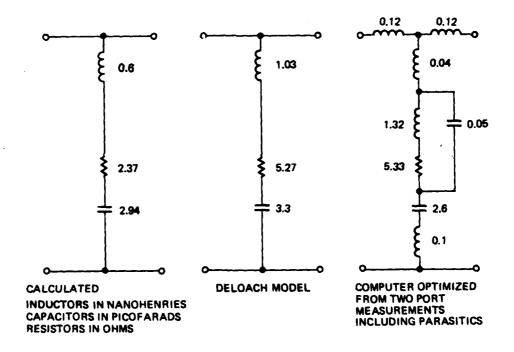


Figure 3-15. Inductor Measurement Sample No. 1 Equivalent Circuits

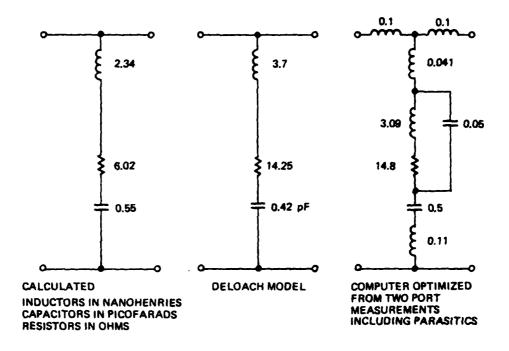


Figure 3-16. Inductor Measurement Sample No. 2 Equivalent Circuits

parasitic, a Q at 10 GHz can be estimated. The experimental Q is approximately 40 percent of the theoretical value and ranges from 7 to 9. At this time the source of the extra loss is not known. Suspected sources are resistance in the gate metal layer used for the capacitor and resistance in the via connections from bottom to top metal. Until the source of the extra loss is identified and eliminated, the increased thickness in top metallization may not have a significant impact on the Q of the series resonant circuit.

#### 3.4 CIRCUIT FABRICATION

The X-band amplifier, configured by eight low noise MESFET stages and their associated input and output matching network, is diagrammed in a composite layout in Figure 3-17. It includes eight interdigited 360  $\mu m$  MESFET with 1  $\mu m$  gate length; each finger is 90  $\mu m$  wide, twenty inductors and six bulk resistors and twenty-two capacitors. The amplifier size is 2.5 mm X 5.0 mm. In order to monitor the IC processing steps, a process evaluation cell has been developed and used in this program. The process evaluation devices include:

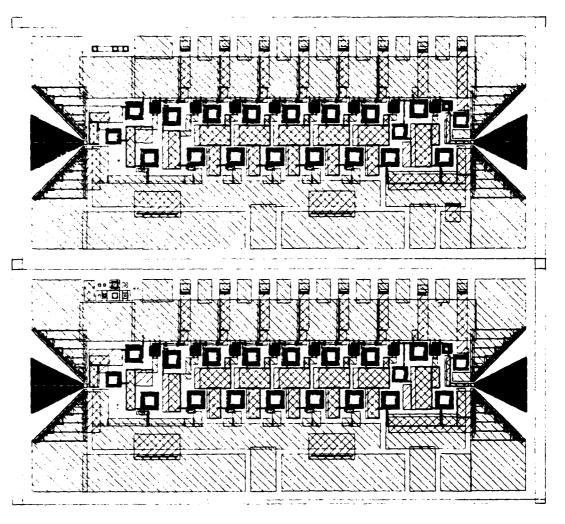


Figure 3-17. Complete 8-Stage MESFET Low Noise Preamplifier for 8 to 11 GHz Bandwidth

- 1) 100 μm x 1 μm FET
- 2) Twenty five 360 µm x 1 µm FET
- 3) Resistor bar (50  $\mu$ m x 50  $\mu$ m contact)
- 4) MOM capacitors
- 5) Ohmic contact string
- 6) Gate contact string
- 7) Gate/top metal serpentine
- 8) Ohmic/top metal serpentine
- 9) Mesa etch isolation pattern.

For circuit diagnosis purposes, a one-stage and two-stage preamplifier and L-C test patterns are included in the test area. A complete layout of the test area is shown in Figure 3-18.

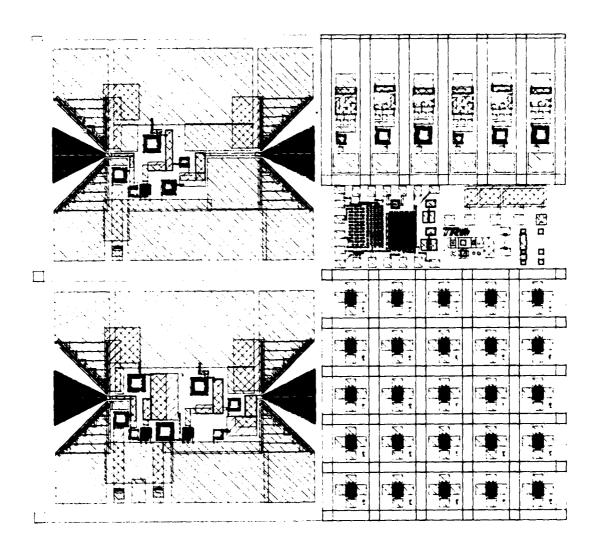


Figure 3-18. Test Cell Including (1) Test Pattern, Process Evaluation Devices, Discrete 360  $\mu m$  FET, One and Two-Stage Preamplifier

#### 3.5 INTERCONNECT AND ISOLATION TECHNIQUE

Most of the circuit elements are joined by the second level metal (or top metal); however, some connections through undercrossings are made with conductors which are deposited and defined along with the capacitor plates and gates.  $3000\text{\AA}$  of Silox formed by the oxidation of silane at  $390^{\circ}\text{C}$  is used as interlayer dielectric for isolation purposes as is the dielectric for the capacitors. After the silox is deposited, via holes are etched into it to permit contact to the top metal consisting of 500A titanium and 10,000A gold.

The Ti-Au metal system is chosen because gold is a good conductor, has low resistivity, and is easily bonded, while titanium makes low resistance contacts to the first level metal including bottom plates of capacitor, center feeds of inductor, gates, and ohmic contacts. The Ti-Au metal system is E-beam-deposited in a vacuum. Photoresist is then coated and patterned, followed by wet etch to refine the interconnect metal patterns.

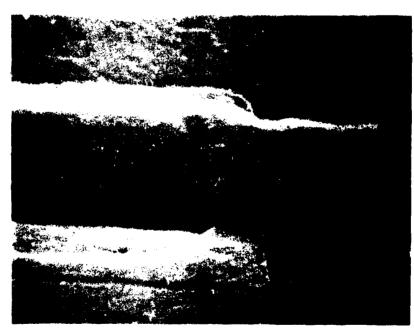
Two interconnection problems occured during the course of this program:

1) the step coverage problem over the sidewall of via holes and the gate metal steps and 2) the interconnect to the Al gate metal during the program's early stages due to the oxidation of Al surface. Replacing the Al gate by Cr-Pt-Au-Pt-Ti as discussed previously has resolved this problem. The step coverage problem over the via hole is shown in Figure 3-19 (a); break in the top metal occurs because of the sharp step of the via hole. An improved process has been developed to etch the via such that the via sidewall is gradual. The step coverage improved with oxide contour is shown in Figure 3-19(b).

The step coverage over gate metal is always a problem because the conventional CVD silox tends to create a inverted slope as shown in the drawing of Figure 3-20, which makes the good smooth step coverage almost impossible. Figure 3-21 shows a typical step coverage of top metal over first level metal, notice the continuity at the bottom of the step. It is believed that this poor step coverage causes serious yield problems. One possible solution is to sputter deposit silox to smooth out the sharp corner of the first level metal. A Perkin Elmer sputtering machine was purchased but because of delay in delivery and some mechanical problems the sputtering



(a) Break Due to Oxide Slope



(b) Step Coverage Improved with Oxide Contour

Figure 3-19. Step Coverage of Top Metal Crossing Over the Via Opening (a) Sharp Slope. (b) Gradual Slope

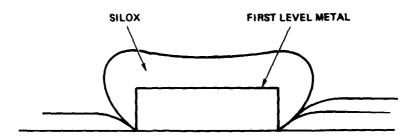


Figure 3-20. Simulating the Step Coverage of 4000 Å Silox over 4500 Å First Level Metal



Figure 3-21. Microphotograph of Top Metal Crossing Over First Level Metal

silox was not implemented into the IC process at the time this program completed. Since then we have developed a company proprietary process which completely eliminates the step coverage problem. Figure 3-22 illustrates the good smooth step coverage of top metal resulting from this new process.

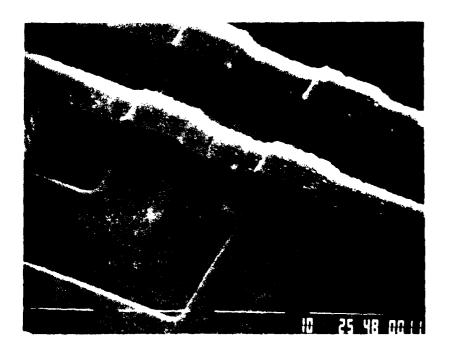


Figure 3-22. Microphotograph of 4  $\mu m$  Undercrossing Metal. (2000X)

#### 4. RF CHARACTERIZATION

#### 4.1 ACTIVE DEVICE CHARACTERIZATION

To evaluate process repeatability between wafers and FET computer model accuracy, the scattering parameters of several FET samples from different wafers were measured at various drain current levels.

A list of the working devices that were characterized is shown in Table 4-1.

14510 1 21 011	14516 1 21 3/14/4036/1254 564/665						
WAFER NUMBERS	DEVICE NUMBERS						
ONR-10	2,3,4,5						
ONR-20	1,2,3						
ONR-21	1,2,3						
ONR-28	3,5						
ONR-38	1,2,3,4						
PAC-2 No. 9	1,2,3,5,6,7,8,9						

Table 4-1. Characterized Devices

Automatic Network Analyzer (ANA) listings of measured scattering parameters for these devices are given in Appendix A. Wafer PAC-2, NO. 9 differs from wafers ONR-10 through ONR-38 in the planar process used in fabrication.

Existing discrepancies between the measured results and the FET computer model will be discussed in Section 6.

#### 4.2 PASSIVE COMPONENT CHARACTERIZATION

Several RLC samples from different wafers were characterized in two parts; associated parasitics were estimated from mechanical measurements and then subtracted by computer optimization routines. This characterization process permitted the accurate evaluation of TRW's microelectronic inductor computer model; further comments on this model as well as it's correlation with the measured values are included in Section 6.

A list of the characterized RLC circuits is shown in Table 4-2.

Table 4-2. Characterized RLC Samples

WAFER NUMBER	SAMPLE NUMBER
Experimenta?	1,2
ONR-38	3,4,5,7
L4-A	1,2

ANA listings of measured scattering parameters for these RLC circuits are given in Appendix B. Wafer L4-A was processed to achieve 3  $\mu m$  metal thicknesses on the inductors; the experimental wafer as well as ONR-38 have metallization thicknesses of 0.5 to 1.0  $\mu m$ .

#### 4.3 PREAMPLIFIER CHARACTERIZATION

The gain-frequency response characteristic was measured for several eight-stage amplifiers from different wafers. A list of these devices is shown in Table 4-3.

Table 4-3. Characterized Eight-Stage Amplifier

WAFER NUMBER	DEVICE NUMBER
ONR-10	1
ONR-21	1,2
ONR-28	1
ONR-37	2-1
ONR-38	1-5, 1-6, 1-7, 43-03

Automatic Network Analyzer listings of measured scattering parameters for these devices are provided in Appendix C. Analysis of discrepancies between predicted and actual performance will be discussed in Section 6. Test data of the deliverable units is given in Appendix D.

#### 5. COMPARISON OF PREAMPLIFIER PERFORMANCE GOALS AND ACTUAL PERFORMANCE

The original design goals for the preamplifiers were:

Gain

30 dB at 10 GHz

Frequency Response 8.0 to 11.0 GHz

Noise Figure

≤3.0 dB at 10 GHz

At the end of the evaluation phase of the preamplifier the measured performance characteristics for the best unit were:

Gain

20 dB at 6 GHz

Frequency Response 3.0 to 9.0 GHz

Noise Figure

8.0 dB at 6.0 GHz

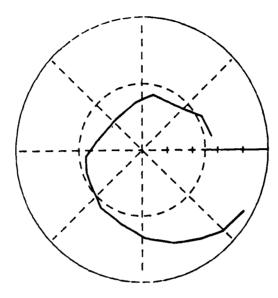
As shown, the measured gain was lower than the predicted gain. The frequency response was shifted to lower frequencies and the noise figure was higher than expected. Section 6 will include an analysis of these discrepancies.

#### 6. ANALYSIS OF DISCREPANCIES

During the evaluation phase of the Monolithic Microwave Preamplifier program, existing discrepancies between predicted performance and actual measurements were found to be originated by

- Discrepancies between theoretical and measured FET device S-parameters
- Discrepancies between theoretical and measured inductor values and their associated Q values

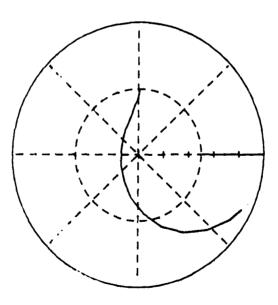
Discrepancies between theoretical and measured S-parameters for the FET used in the amplifier are shown in Figures 6-1 through 6-8. The greatest differences are exhibited by  $\mathbf{S}_{11}$  and  $\mathbf{S}_{21}$ . Consequently, it can be concluded that in the present design the devices are severely mismatched at the input and that their corresponding forward power transfer is considerably less than expected. The impact analysis of measured FET data on the amplifier frequency response is shown in Figure 6-9. The dashed line indicates the predicted performance of the preamplifier with theoretical FET S-parameters and inductor parameters, the solid line indicates the actual measured performance of the best unit, and the broken line is the theoretical performance with measured FET S-parameters and theoretical inductor parameters. Discrepancies between theoretical and measured values and associated parasitic ohmic resistances are shown in Table 6-1.



SII: POLAR FULL SCALE 1

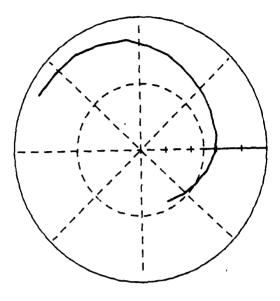
Figure 6-1. Measured  $S_{11}$ 

360uM DEVICE Vd=3 Id=30



S11: POLAR FULL SCALE 1

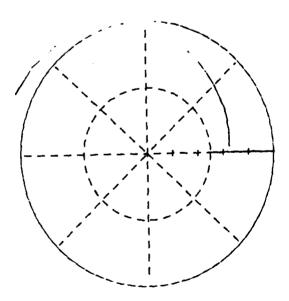
Figure 6-2. Theoretical  $S_{11}$ 



S21: POLAR FULL SCALE 2

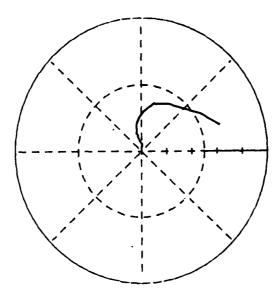
Figure 6-3. Measured S<sub>21</sub>

360uh DEVICE Vd=3 Id=30



S21: POLAR FULL SCALE 2

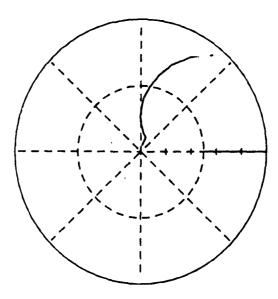
Figure 6-4. Theoretical  $S_{21}$ 



S12: POLAR FULL SCALE .5

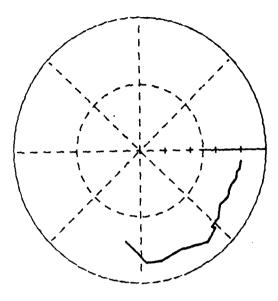
Figure 6-5. Measured S<sub>12</sub>

360uM DEVICE Vd=3 Id=30



S12: POLAR FULL SCALE .5

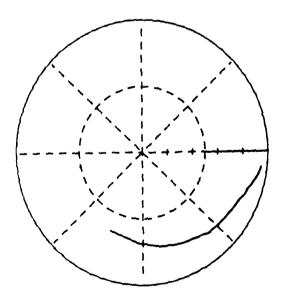
Figure 6-6. Theoretical  $S_{12}$ 



S22: POLAR FULL SCALE 1

Figure 6-7. Measured S<sub>22</sub>

360um DEVICE Vd=3 Id=30



S22: POLAR FULL SCALE 1

Figure 6-8. Theoretical S<sub>22</sub>

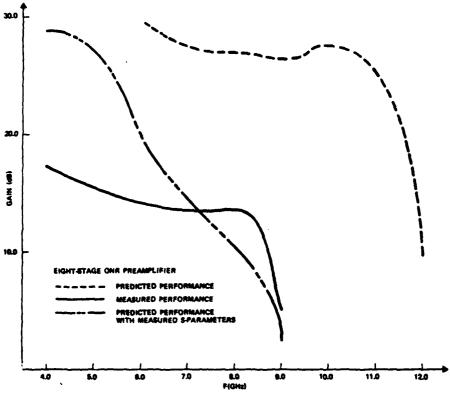


Figure 6-9. Eight-Stage ONR Amplifier Frequency Response

Table 6-1. Discrepancies in Inductor Values (Values are in Nanohenries, Ohms, and Picofarads)

SAMPLE NUMBER		CALCULATED	DELOACH MEASUREMENT	COMPUTER-FITTED DATA
Experimental No. 1	L R C	0.6 2.37 2.94	1.03 5.27 3.3	1.32 5.33 2.6
Experimental No. 2	L R C	2.34 6.21 0.55	3.7 14.25 0.42	3.09 14.78 0.50
ONR-38 No. 3 Run 1	L R C	1.34 4.17 1.14	2.03 8.92 0.92	1.8 8.26 0.92
ONR-38 No. 3 Run 2	L R C	1.34 4.17 0.19	1.88 11.82 0.21	1.76 12.36 0.21
ONR-38 No. 4 Run 1	L R C	1.34 4.17 0.57	1.93 7.89 0.56	1.6 7.49 0.60
ONR-38 No. 4 Run 2	L R C	1.34 4.17 0.19	2.08 9.15 0.23	1.75 10.15 0.23
ONR-38 No. 5 Run 1	L R C	2.34 6.21 0.11	3.02 17.09 0.15	2.84 18.95 0.14
ONR-38 No. 7 Run 1	L R C	0.6 2.48 0.42	1.31 5.98 0.38	1.1 5.3 0.38
L4-A No. 1	L R C	1.3 1.05 0.38	1.57 4.21 0.43	1.37 3.6 0.42
L4-A No. 2	R C	1.30 1.05 0.38	1.76 4.21 0.39	1.41 3.45 0.42

From these measurements it can be observed that all measured inductor values are higher than the theoretical values. One immediate consequence of this fact is a shift of the frequency response characteristic to a lower band than theoretically predicted; this agrees in principle with the measured results. The impact analysis of these discrepancies on the amplifier's frequency response is shown in Figure 6-10. The dashed line indicates the predicted performance of the preamplifier with theoretical FET S-parameters and inductor parameters; the solid line indicates the actual measured performance of the best unit, and the broken line indicates the theoretical performance with measured inductor parameters and theoretical FET S-parameters. The predicted gain-frequency characteristic using measured inductor data starts at 58.3 dB of gain at 4.0 GHz followed by a flat segment of 40 dB gain between 6.0 and 10.0 GHz, then dropping to 6.1 dB of gain at 12 GHz. Figure 6-10 shows a section of this curve for frequencies above 12 GHz.

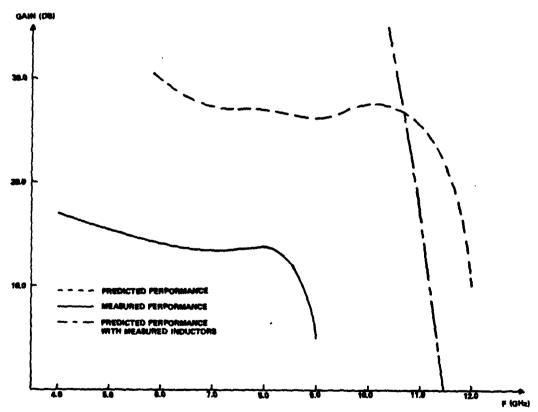


Figure 6-10. Eight-Stage ONR Amplifier Frequency Response

#### 7. CONCLUSIONS AND RECOMMENDATIONS

It has been concluded that the preamplifier design is highly dependent on the accuracy of the FET S-parameters and noise parameters, since the differences between the predicted and measured performances can be largely explained by the substantial discrepancies that exist within the theoretical and actual parameters of the FET's. To a lesser degree, the differences between predicted and measured values of the planar rectangular inductors contribute significantly to the inequalities of the preamplifier's performances. TRW's theoretical design capabilities for circuit analysis and synthesis appear to be adequate since a close correlation was established between the preamplifier performance data and the analyzed predicted circuit performance using measured FET S-parameters and inductor parameters.

In addition to these conclusions, a large data base for FET devices and inductors must be accumulated, the inductor computer model requires refinment to enhance it's accuracy at higher microwave frequencies, and GaAs integrated circuit processing must be improved to yield better FET device performance.

It is recommended that a second design iteration be made on this preamplifier using measured FET and inductor parameters drawn from a large data base. Significant processing improvements can also be made on channel profile optimization, controlled channel etching, better metal deposition techniques for gate metal formation, and improved dielectric deposition techniques to achieve good step coverage.

APPENDIX A

#### ONR FET CHARACTERIZATION

.00 VOLTS,	.00 MA (ME	(AS 1)	*2 VD	D=4V ID=31.0MA
FREQ	211	S 2 1	\$12	<b>S22</b>
	IAG ANG	MAG ANG	MAG ANG	MAG ANG
	928 -36	1.144 147	.037 74	.774 -5
	917 -40	1.141 143	.041 72	.771 -6
	909 -44	1.148 140	.044 71	.768 -7
	893 -48	1.145 136	.048 69	.764 -8
	885 -52	1.148 132	.051 67	.765 -9
	869 -57	1.144 129	.054 65	.759 -10
	849 -62	1.137 125	.057 63	.756 -11
	833 -66	1.125 121	.059 61	.752 -12
	814 -71	1.105 117	.060 59	.747 -14
	798 -76	1.091 113	.062 57	.741 -15
	773 -80	1.064 110	.063 55	.734 -16
	770 -84	1.030 107	.063 54	.730 -17
	.763 -88	1.014 104	.065 53	.725 -18
	.758 ~92	.993 .101	.066 52	.722 -19
	756 -96	.977 98	.067 51	.722 -20
	.753 -100	.957 95	.068 49	.724 -21
	750 -103	.947 92	.069 48	.728 -22
	.737 -107	.927 89	.070 46	.731 -23
5600.000 .	.722 -111	.910 86	.071 42	.731 -24
5800.000 .	.687 -114	.878 83	.071 38	.724 ~24
	.637 -117	.833 80	.063 28	.716 ~23
	.618 -116	.803 80	.048 37	.721 ~22
	.622 -118	.802 79	.049 49	.723 -23
	.625 -122	.802 77	.055 51	.719 -24
	.619 -125	.791 75	.058 51	.708 -25
	.615 -129	.778 73	.059 51	.696 -26
	.613 -133	.770 71	· .060 51 ·	.687 -26
	.617 ~136	.766 69	.061 51	.679 -28
	.617 ~139	.755 67	.061 51	.682 -29
	.613 ~142	.754 65	.061 51	.684 -30
	.611 -145	.751 63	.062 52	.685 -31
	.614 -149	.742 59	.064 51	.722 -31
	.600 -152	.733 57	.064 51	.729 -32
	.582 ~156	.718 54	.064 51	.727 -33
8800.000	.568 -160	.706 52	.064 50	.718 -33
	.567 -163	.690 50	.064 51	.708 -34
	.574 -166 .581 -169	.670 48 .661 46	.063 <b>5</b> 2 .063 <b>5</b> 3	.687 -35 .670 -36
	.587 -172	.652 45	.064 54	.662 -35
	.604 -176	.646 43	.066 54	.639 -36
10000.00	.628 -178	.640 41	.068 54	.624 -38
	.647 -179	.638 39	.069 54	.622 -42
	.658 180	.634 37	.070 53	.625 -45
	.661 -179	.636 35	.072 53	.644 -49
	.635 -179	.627 31	.072 52	.681 -52
	.601 -178	,618 28	.074 50	.719 -55
	.538 -176	.604 24	.074 49	.774 -57
	.441 -174	.577 20	.075 47	.830 -57
	.410 -167	.517 19	.071 46	.807 -59
	.395 -168	<b>.50</b> 0 23	.072 49	.762 -56
	.379 -173	.510 26	<b>4-1</b> .073 50	.743 -51
	.511 174	.591 22	.079 49	.778 -53

12400.00	.456	160	.586	18	.080	48	.755	-48
12600.00	.468	134	.550	15	.085	46	.705	-48
12800.00	.545	133	.541	12	.086	44	.641	~52
13000.00	.584	131	.538	9	.086	42	.610	-56
13200.00	.607	134	.531	6	.086	39	.599	-64
13400.00	.610	138	.521	3	.886	38	.620	-73
13600.00	.587	143	.504	0	.085	36	.675	-80
13800.00	.539	148	.486	-3	.085	35	.732	-84
14000.00	.528	151	.464	-3	.084	35	.720	-84
14200.00	.528	147	.463	-2	.087	37 .	.705	-80
14400.00	.486	138	.478	-4	.091	35	.711	-74
14600.00	.446	126	.474	~ 5	.094	34	.735	-69
14800.00	.421	114	.476	-8	.096	33	.754	-64
15000.00	.436	103	.475	-11	.099	31	.749	-62
15200.00	.470	97	.473	-14	.102	29	.738	-61
15400.00	.504	93	.465	-17	.196	27	.794	-62
15600.00	.534	91 -	.467	-19	.109	25	.666	-65
15800.00	.561	89 🔭	.452	-22	.113	22	.640	-68
16000.00	.571	88 *	.449	-25	.115	19	.617	-72
16200.00	.562	85	.443	-27	.118	17	.612	-76
16400.00	.555	82	.434	~30	.120	15	.618	-79
16600.00	.545	81	.428	-32	.124	12	.616	-82
16800.00	.548	77	.423	-33	.125	9	.613	-84
17000.00	.560	73	.414	36	.125	7	.616	~84
17200.00	.569	67	.412	-38	.128	5	.614	-84
17400.00	.583	63	.410	-41	.129	4	.604	-85
17600.00	.601	60	.401	-43	.132	2	.596	-86
17800.00	,613	59	.396	-44	.136	1	.568	-87
18000.00	.617	57	.393	-47	.142	~ 1	.554	-90

REF PLANE EXT(CM): IN= 5.48, OUT= 5.48

#### PAGE 1: 1

#### ONR FET CHARACTERIZATION

JUNE 9/80

.00 VOLTS,	.00 MA (M	EAS 1)	#3 VD1	D=4V ID=32.0MA
FREQ	S11	\$21	\$12	\$22
(MHZ)	MAG ANG	MAG ANG	MAG ANG.	MAG ANG
2000.000	.932 -35	1.170 147	.033 74	.783 ~6
2200.000	.923 -39	1.166 143	.036 72	.781 -7
2400.000	.916 -43	1.174 140	.040 71	.778 -8
2600.000	.902 -47	1.171 136	.042 69	.773 -9
2800.000	.898 -51	1.175 133	.045 68	.776 -10
3000.000	.884 -55	1.173 129	.048 65	.768 -11
3200.000	.867 -60	1.168 125	.050 63	.764 -13
3400.000	.852 -64	1.156 121	.052 62	.759 -14
3600.000	.834 -68	1.140 117	.053 59	.753 -16
3800.000	.820 -72	1.129 114	.055 58	.745 ~17 .
4000.000	.796 -76	1.106 110	.057 56	.738 -19
4200.000	.793 -79	1.072 108	.057 55	.732 -20
4400.000	.785 -83	1.061 104	.058 54	.727 -22
4600.000	.778 -87	1.044   102	.059 52	.724 -24
4800.000	.776 ~91	1.032 98	.061 51	.726 -25
5000.000	.773 ~95	1.017 95	.062 49	.728 -27
5200.000	.767 ~98	1.009 92	.063 47	.735 -29
5400.000	.753 -102	.990 89	.065 45	.738 -30
5600.000	.737 -106	.974 84	.066 40	.738 -32
5800.000	.698 -110	.935 81	.065 32	.729 -32
6000.000	.638 -112	.875 78	.053 18	.716 -31
6200.000	.632 -111	.847 79	.037 35	.726 -30
6400.000	.639 -114	.851 77	.041 50	.733 -31
6600.000	.641 -118	.848 75	.047 52	.730 -32
6800.000	.636 -122	.833 73	.049 51	.719 -33
7000.000	.632 -126	.817 71	.050 51	.709 -34
7200.000 7400.000	.632 -129 .638 -133	.808 69 .804 67	.051 51 .051 51	.701 -35 .695 -36
7600.000	.641 -135	.794 65	.051 52	.699 -38
7800.000	.638 -138	.794 63	.052 52	.702 -38
8000.000	.638 -141	.794 60	.052 53	.702 -39
8200.000	.642 -144	.789 57	.055 52	.739 -39
8400.000	.627 -147	.781 54	.055 52	.744 -41
8600.000	.608 -150	.767 52	.055 51	.738 -41
8800.000	.589 -153	.757 49	.055 51	.726 -42
9000.000	.582 -157	.741 46	.055 51	.710 -44
9200.000	.587 -159	.722 44	.055 52	.691 -46
9400.000	.589 -162	.715 42	.056 53	.674 -47
9600.000	.590 -166	.708 41	.057 54	.666 -48
9800.000	.604 -170	.707 39	.059 54	.647 -50
10000.00	.624 -173	.704 36	.061 53	.6 <b>38 -5</b> 3
10200.00	.642 -175	.702 33	.06 <b>½</b> 52	.646 -58
19409.00	.653 -177	.698 30	.063 50	.661 -62
19699.99	.657 -177	.697 27	.064 48	.694 -66
10800.00	.630 -177	.682 23	.065 47	.736 -68
11000.00	.599 -176	.665 19	.065 44	.776 -71
11200.00	.538 -175	.640 15	.064 42	.823 -72
11400.00	.443 -173	.600 11	.064 40	.859 -71
11600.00	.415 -167	.530 11	.060 39	.821 -71
11800.00	.403 -167	.519 16	.061 43	.775 -66
12000.00 12200.00	.389 -171 .522 176	.537 19 A-	3 .062 44 .070 43	.758 -60
12200.00	.522 176	1930 14	*818 42	.827 -62

12400.00	.462	163	.634	10	.071	41	.790	~58
12600.00	.467	136	.602	6	.077	38	.729	-60
12300.00	.540	135	.595	3	.077	35	.667	-66
13000.00	.575	133	.595	-0	.078	31	.640	-72
13200.00	.593	135	.588	-5	.078	27	.641	-81
13400.00	.593	138	.575	-8	.078	25	.672	-89
13600.00	.564	143	.553	-12	.076	22	.730	~95
13800.00	.511	147	.529	-15	.075	20	.778	-97
14000.00	.496	148	.505	-15	.074	21	.759	-96
14200.00	.489	143	.506	-15	.078	21	.753	-92
14400.00	.450	130	.518	-17	.082	19	.763	-86
14600.00	.419	116	.522	-20	.084	16	.787	-81
14800.00	.412	102	522	-23	.087	13	.803	-78
15000.00	.442	92	.516	-27	.089	11	.793	-77
15200.00	.486	87	.510	-29	.091	9	.774	-76
15400.00	.525	85	.496	-33	.094	6	.736	-78
15600.00	.558	84	.496	-35	.097	4	.700	-80
15300.00	.582	84	.480	-38	.099	1	.673	~83
16000.00	.596	82	.479	-40	.102	-2	.652	-86
16200.00	.581	80	.477	-42	.105	-4	.651	-88
16400.00	.570	78	.471	-45	.108	-7	.655	-90
16600.00	.556	76	.469	-48	.112	-9	.648	-92
16800.00	.558	72	.466	<b>5</b> 0	.115	-12	.639	-93
17000.00	.565	67	.466	-52	.116	-15	.634	-93
17200.00	.571	61	.464	-56	.120	-18	.624	-93
17400.00	.584	55	.468	-59	.122	-19	.605	-94
17600.00	.602	50	.460	-62	.127	-21	.586	-96
17800.00	.612	50	.453	-641	.130	-22	.550	-98
18000.00	.621	46	.456	-68	.138	-26	.532	-103

REF PLANE EXT(CM): IN= 5.48, OUT= 5.48

#### ONR FET CHARACTERIZATION

.00 VOLTS,	.00 MA (ME	(AS 1)	#4	VDD=4V ID=9.3MI
FREQ	S11	\$21	S12	\$22
(MHZ)	MAG ANG	MAG ANG	*****	. MAG ANG
2000.000	.945 -28	.980 149	.043 74	.801 -8
2200.000	.938 -31	.981 146	.047 73	.799 -9
2400.000	.932 -34	.991 143	.051 71	.796 -10
2600.000	.919 -37	.992 140	.055 69	.792 -12
2800.000	917 -41	.999 137	.059 68	.796 -13
3000.000	903 -44	1.002 133	.063 65	.789 -14
3200.000	.889 -48	1.001 129	.066 63	.785 <b>-16</b>
3400.000	.876 -52	.997 126	.069 61	.783 -17
3600.000	.861 -56	.987 122	.072 58	
3800.000	.844 -60	.980 118	.074 56	
4000.000	823 -63	.964 115	.076 55	
4200.000	.819 -66	.933 113	.077 53	
4400.000	.808 -70	.925 109	.079 52	
4600.000	.804 -73	.914 107	.081 50	
4800.000	802 -76	.906 104	.083 49	
5000.000	.798 -79	.896 101	.085 47	
5200.000	798 -82	.894 98	.087 46	
5400.000	.787 -85	.882 95	.090 44	
5600.000	.772 -88	.875 91	.093 40	
5800.000	740 -91	.849 88	.094 35	
6000.000	.693 -92	.809 85	.086 27	
6200.000	.683 -91	.789 85	.071 32	
6400.000	.679 -93	.790 84	.072 39	
6600.000	.669 -96	.792 81	.078 49	' TERE AA
6800.000	.655 -100	.784 79	.080 49	
7000.000	.643 -103	.774 77	.081 39	'
7200.000	.632 -106	.773 75	.083 38	• • • • • • • • • • • • • • • • • • • •
7400.000	.630 -109	.770 73	.084 37	
7600.000	.629 -113	.764 71	.085 37	
7800.000	.621 -116	.763 68	.086 3	
8000.000	.616 -119	.763 66	.086 35	J 11 V 1
8200.000	.618 -123	.763 62	•	• • • • • • • • • • • • • • • • • • • •
8400.090	.600 -127	.757 59	.089 3 .088 2	1100 [2
8600.000	.577 -131	.739 57	.087 2	
8800.000	.553 -136	.731 54	.085 2	
9000.000	.543 -140	.714 52 .693 50	.083 2	
9200.000	.546 -144		.083 2	
9400.000	.548 -148	.688 48 .681 47	.083 2	~ · · · · · · · · · · · · · · · · · · ·
9600.000	.550 -152	.682 45	.084 2	
9800.000	.567 -157	.681 43		5 .648 -51
10000.00	.591 -161	.682 40		4 .652 -55
10200.00	.617 -163	.681 37		3 .662 -58
10400.00	.637 -165	.684 35		2 .688 -61
10600.00	.651 -165 .637 -165	.675 31	.086 2	g .725 -63
10300.00		.661 26		7 .763 -66
11000.00		.641 22		6 .810 -67
11200.00	.560 -161 .472 -157	.603 18		3 .850 -66
11400.00	.450 -150	.529 18	.075 1	3 .812 -67
11600.00	.434 -148	.512 23	.074 1	7 .761 -63
11880.90	.418 -148	.524 27	075 2	737 -57
12000.00 12 <b>200.</b> 00	.556 -164	.635 23	A-5 085 2	780 -60
15700.00	,000	•	-	

12400.00	.473	-174	.632	19	.087	19	.745	-54
12600.00	.440	158	.604	14	.095	17	.690	-54
12800.00	.515	154	.595	12	.096	14	.634	-58
13000.00	.553	151	.593	8	.096	10	.610	-63
13200.00	.585	152	.583	4	.096	7	.607	-72
13400.00	.606	156	.569	2	.093	4	.635	-80
13600.00	.598	162	.545	-2	.091	2	.693	-87
13800.00	.566	169	.520	-4	.087	1.	.750	-90
14000.00	.570	174	.492	-3	.084	3	.731	-90
14200.00	.582	174	.499	-0	.088	7	.720	-85
14400.00	.550	169	.528	- 1	.094	7	.725	-80
14600.00	.501	160	.554	-3	.100	5	.744	-75
14800.00	.441	150	.570	-7	.104	2	.757	-71
15000.00	.415	138	.574	-11	.107	- 1	.748	-70
15200.00	.421	128	.574	-15	.109	-3	.728	-70
15400.00	.439	122	.562	-19	.111	-5	.689	-72
15600.00	.462	117	.562	-22	.114	-8	.649	-76
15800.00	.486	115	.543	-26	.115	-10	.622	-81
16000.00	.502	113	.542	-28	.119	-13	.604	-86
16200.00	.498	110	.540	-31	.121	-14	.605	-90
16400.00	.495	108	.532	-34	.122	-17	.614	-93
16600.00	.489	106	.523	-36	.124	-20	.617	-96
16800.00	.490	103	.522	· <b>-</b> 37	.127	-21	.617	-99
17000.00	.502	98	.518	-41	.126	-24	.622	-99
17200.00	.508	91	.521	-44	.130	-26	.618	-99
17400.00	.519	85	.520	-47	.130	-28	.610	-100
17600.00	.536	81	.508	-50	.131	-29	.601	-101
17800.00	.551	78	.496	~52	.133	-31	.578	-104
18000.00	.559	76	.494	-55	.137	-32	.569	-107

REF PLANE EXT(CM): IN= 5.48, OUT= 5.48

#### ONR FET CHARACTERIZATION

.00 VOLTS,	.00 MA (	MEAS 1)	*4 VD1	D=4V ID=31.0MA
FREQ	\$11	\$21	\$12	<b>522</b>
(MHZ)	MAG ANG	MAG ANG	MAG ANG	MAG ANG
2000.000	.930 -35	1.147 146	.034 73	.784 ~7
2200.000	.919 -39	1.142 143	.037 71	.782 ~9
2400.000	.912 -43	1.147 139	.040 70	.779 -10
2600.000	.898 -48	1.143 135	.043 68	.776 -11
2800.000	.891 -52	1.144 132	.046 66	.779 -12
3000.000	.876 -56	1.139 128	.048 64	.773 -13
3200.000	.857 -61	1.132 124	.050 62	.770 -15
3400.000	.842 -65	1.117 120	.052 60	.768 -16
3600.000	.823 -70	1.096 116	.053 58	.762 -17
3800.000	.809 -74	1.082 113	.055 56	.756 -18
4000.000	.785 -78	1.055 109	.056 54	.749 -20
4200.000	.783 -81	1.022 107	.056 53	.746 -21
4400.000	.776 -86	1.006 104	.057 52	.742 -22
4600.000	.770 -89	.988. 101	.058 51	.740 -23
4800.000	.768 -93	.974 98	.059 50	.741 -24
5000.000	.765 -96	.955 95	.061 48	.743 -25
5200.000	.762 -99	.947 93	.061 47	.748 -26
5400.000	.749 -102	.929 90	.063 45	.751 -27
5600.000 5800.000	.734 -106 .699 -109	.916 36 .886 83	.064 41	.750 -29
6000.000	.651 -111	.886 83 .840 80	.063 36	.742 -29
6200.000	.639 -111	.818 80	.055 25 .041 36	.731 -29 .735 -28
6400.000	.635 -113	.818 79	.044 49	.739 -29
6600.000	.629 -117	.816 76	.050 51	.735 -30
6800.000	.620 -121	.807 74	.051 50	.724 -31
7000.000	.611 -124	.795 72	.052 50	.713 -33
7200.000	.605 -128	.790 70	.054 49	.705 -34
7400.000	.606 -132	.786 68	.054 50	.699 -35
7600.000	.605 -136	.777 65	.054 50	.704 -37
7800.000	.598 -139	.777 63	.055 49	.707 -38
8000.000	.594 -143	.773 61	.055 .50	710 -39
8200.000	.595 -148	.766 57	.057 49	.750 -40
8400.000	.580 -152	.753 54	.057 48	.757 -41
8600.000	.563 -156	.736 51	.057 47	.753 -42
8800.000	.549 -161	.720 48	.056 47	.743 -42
9000.000	.550 -165	.700 46	.055 47	.731 -43
9200.000	.559 -169	.677 44	.054 48	.713 -45
9400.000	.570 -173	.665 42	.055 49	.697 -45
9600.000 9800.000	.578 -176 .599 180	.652 41 .644 39	.056 51 .057 50	.690 -45
10000.00	.625 177	.636 37	.058 50	.670 -46 .660 -48
10200.00	.646 176	.631 34	.059 49	.663 -52
10400.00	.658 175	.625 32	.060 49	.672 -54
10600.00	.660 176	.622 30	.060 48	.699 -58
10800.00	.634 176	.611 26	.061 47	.737 -60
11000.00	.600 177	.597 23	.062 46	.776 -62
11200.00	.538 179	.578 19	.061 44	.825 -64
11400.00	.444 -179	.547 16	.062 43	.870 -63
11600.00	.416 -173	.487 15	.058 42	.836 -64
11800.00	.408 -173	.473 20	.059 45	.736 -61
12000.00	.398 <b>-178</b>	.486 23 <b>A-</b> 3	7 .060 46	.765 -55
13200.00	.533 170	.565 13		.818 ~56

12400.00	.483	158	.569	15	.066	44	.789	-52
12600.00	.495	134	.524	12	.071	42	.738	-53
12800.00	.573	134	.517	9	.072	40	.674	-57
13000.00	.611	133	.515	6	.072	37	.646	-62
13200.00	.633	136	.509	3	.072	34	.638	-70
13400.00	.640	141	.498	1	.072	33	.661	-78
13600.00	.620	146	.482	-2	.071	31	.713	-85
13800.00	.576	152	.464	-5	.070	29	.766	-88
14000.00	.573	155	.443	-4	.069	31	.745	-88
14200.00	.582	153	.449	-3	.073	33	.730	-83
14400.00	.544	145	.466	-4	.077	31	.736	-78
14600.00	.498	134	.477	-7	.080	29	.759	-73
14800.00	.461	122	.484	-10	.083	27	.776	-69
15000.00	.464	112	.486	-13	.086	24	.769	-68
15200.00	.483	105	.485	-17	.089	22	.751	-68
15400.00	.518	101	.476	-20	.092	19	.713	-70
15600.00	.545	98	.477	-23	.095	16	.671	-73
15800.00	.573	97	.462	-27	.097	13	.642	-78
16000.00	.584	95	.460	-29	.100	10	.619	-82
16200.00	.578	92	.455	-32	.101	7	.618	-86
16400.00	.571	90	.446	-35	.103	4	.624	-90
16600.00	.562	88	.438	-38	.105	1	.622	-93
16800.00	.565	85	.435	·-38	.106	-2	.619	-95
17000.00	.577	80	.428	-42	.104	-5	.620	-95
17200.00	.585	74	.424	-46	.106	-7	.617	-95
17400.00	.597	70	.419	-48	.106	-8	.607	-95
17600.00	.615	67	.408	<b>-5</b> 1	.107	-9	.598	-96
17800.00	.628	65	.396	-52	.108	-11	.578	-98
18000.00	.632	63	.391	-55	.112	-12	.568	-100

REF PLANE EXT(CM): IN= 5.48, OUT= 5.48

. 19 MT LTD, .00 MA (MEAS t) #3 MTV-19 10∞15.0°F

	544	7/21	.*1	71	~ ~ ~	
. (원화 (1192)	311 Mas ans		·	:110		ans
্ন কৰিছেই তুলিকার হুবি তেখি	.943 -39					- 47
	.932 -33	1.0			.7%5	<b>-</b> 15
	.934 -37	1.131 (1)	4 . 453	1	.751	
	.912 -49	3 1 1 1 1 1 1	•		5	<del>-</del> .:
1. 1. 1. 1	.997 -44	-1 - 144 - 13		. •	.707	' 1
	.008 -48	$-1.1 \cdot 1 \cdot 1 = 10$		• •	• •	-1:0
i, .a., y	.871 -53	1.		<u>អូក</u>		- 1 A
79 M.S. T.	.064 -55	12.12		A 5		-13 -15
	.049 -33 .040 -63	1.115 10 1.116 12		6 t 90		-16 -16
00000.000 0000.000	.040 -63 .027 -66	1.193 11		57		-18
- 4079.303 - 4170.503	.313 -70	1.003 11		~ . 55		-14
4430.333	.005 -73	1.077 11		53		-20
4300.000	.791 -77	1.056 10		52		-21
4000.000	.731 -30	1.047 10	5 .007	50	.697	-23
5003.000	.765 -84	1.936 10	2 .008	40	.692	-34
5:20.033	.752 <b>-</b> 87	1.035		4.7		-34
5400.000	.737 -91	1.012 9		4.5	.604	-25 -25
ଅଟେବ୍ୟ ପ୍ରେମ୍ବ	.724 -94	.909 ე		4.2		-26 -27
5.0.00	.701 -98	• • • •	$\frac{9}{6}$ $\frac{1094}{67}$	97 39	.664 .653	-27
5.733.051 7.330	.665 -102 .648 -101		6 .473	34	.661	-27
13370.447 1437.57	.671 -104		5 .074	43	.673	-27
3,71.314	.669 -107		3 .00 <b>0</b>	4.1	.673	-29
	.667 -110		0 ,003	43	.672	-30
70 10 1	.664 -113		7 .004	42	.677	-31
7:13,203	.655 -116		5 ,706	11	.ផេខ3	+31
7430.510	.641 -119		3 .936	ୀରି ଓ	.679	-33
71.4.767 73.3.443	.628 -122		1 .086	411	• គ្នក់គ្ន	-33
73 0.00	.516 -135	• • • •	936	4.0	.6 5 .693	-33 -34
	.695 -129		5 ,896 .≰ ,637	319 × 3	.613	_
11. 1.451 14.0.011	.601 -102 .509 -106		OM (1994년) 2월 - 1943년	3 3	.607	
	.979 ~109		in 199	i a	5	- : :
	.917 -144	4	(7) (15)	3.7		- 1
4 4 4 4 1	597 -147		4	7,3	.617	- 1 1
95 mg. 1	.592 -151		. 5.19	3.5	.614	: :
2473.341	.501 -153		.000	35	.613	
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17:00.37		.561 -2	23 .112	2	.634	-34
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#### ONR PREAMP FET CHALACTONIZATION

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200 <b>0.</b> 000	.932 -35	4.4254	939 71	.753 -9
323 <b>3.</b> 333	.930 -39	1,355 141	.042 /3	.743 -6
3439,303	.909 -40	1.253 (41	.345 71	.741 -6
1130,940	1.838 -47	1 94 197	.949 69	.735 -7
. 3 <b>3.</b> 333	.882 -51	1.044 134	.932 67	.733 -0
300 <b>0.</b> 003	.063 -55	1.043 130	,85 <b>5</b> 65	.725 ~10
330 <b>0.</b> 800	.351 -60	1.31 127	.05 <b>8</b> 64	.715 -11
0:30 <b>.</b> 333	.843 -64	1.831 120	.040 62	.711 -12
339 <b>3.</b> 333	.828 <b>-</b> 68	1.293 120	.882 69	.797 -14
000 <b>0.</b> 000	.820 -72	1.203 116	.065 59	.704 -15
4) <b>89.</b> 000	.805 -76	1.102 113	.066 57	.701 -17
:200.001	.790 ~80	1.156 109	.063 55	.698 -18
4400.000	.779 -84	1.143 106	.069 54	.694 -19
46 <b>00.</b> 000	.76 <b>8 -</b> 83	1.116 193	.070 52	.694 -20
4330.887	.757 -91	1.104 100	.071 51	.691 -21
5000.000	.741 -95	1.087 97	.072 49	.686 -22
520 <b>3.</b> 031	.728 -99	1.071 94	.973 47	.683 -23
540 <b>0.</b> 433	.714 -103	1.052 92	.075 46	.678 -24
868 <b>0.</b> 070	.702 -107	1.025 33	.076 43	.676 -25
5300.000	.632 -111	1.002 35	.075 38	.661 -26
639 <b>0.</b> 333	.648 -115	.972 02	.067 30	.649 -25
619 <b>0.</b> 000	.628 -114	.917 92	.432 38	.660 -25
6430.231	.649 -117	.931 03	.957 50	.671 -26
66 <b>38.</b> 333	.649 -120	.927 79	.063 50	.673 -28
600 <b>0.</b> 000	.630 -124	.920 76	.065 49	.674 -28
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7200.300	.637 -130	.896 71	.067 49	.682 -2n
7400.000	.624 -133	.881 69	.068 48	.633 -30
7000.000	.613 -136	.868 67	.067 40	.679 -31
7 33.0 3	.607 -140	.835 65	.063 49	.660 -31
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233.3	.594 -147	.847 69	.370 49	.631 -33
340 <b>3.</b> 330	.595 -151	.839 50	.379 43	.642 -34
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3 30.333	.603 -158	.824 53	.971 49	.634 -35
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### ONR PREAMP FOR CHARACTERIZATION

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(882)	MAG ANG	Mae ans	Mag ang.	MAG ANG
1900.500	.945 -29	1.077 151	.045 75	.773 -6
0200.500	.935 -32	1.999 147	.849 73	.769 -6
2430.033	.927 -35	1.085 144	.053 72	.762 -7
.633.333	.916 -39	1.000 141	.057 78	.756 -0
შშიფ.კათე	.902 -42	1.33 133	.062 68	.749 -9
0000.000	.891 -46	1.091 135	.066 67	.746 -10
0290.033	.877 -50	1.797 131	.969 65	.737 -12
J490.000	.871 -53	1.034 128	.872 63	.733 -13
363 <b>8.</b> 333	.856 -57	1.077 124	.076 61	.728 -15
3838.003	.846 -60	1.030 121	.079 59	.723 -16 •
4000.000	.833 -64	1.068 113	.081 57	.729 -18
4200.000	.820 -67	1.052 114	.384 55	.719 -19
4403.000	.811 -71	1.043 111	.086 53	.715 -20
4600.000	.795 -74	1.025 103	.037 51	.713 -21
4030.000	.786 -78	1.016 105	.889 50	.708 -23
500 <b>3.</b> 30 <i>a</i> 524 <b>8.</b> 400	.771 -81 .758 -84	1.007 103 .996 103	.091 48	.703 -24 .701 -25
7430.070 7430.073	.738 -84 .744 -88	.935 97	.092 46 .094 45	
539 <b>0.</b> 833	.729 -91	.707 76 .965 93	.096 41	.694 -25 .690 -26
::30 <b>3.</b> 33 <b>3</b>	.706 -95	.543 90	.097 37	.675 -27
830 <b>3.</b> 333	.671 -93	.904 37	.092 30	.663 -27
3230.030	.656 -98	.871 37	.074 33	.672 -27
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363 <b>3.</b> 333	.672 -104	.391 34	.083 43	.682 -29
៩៤៦៧.៤៦៧	.671 -107	.806 81	.086 42	.682 -30
7830.330	.670 -110	.874 78	.037 41	.686 -31
1335.830	.660 -113	.871 76	.099 40	.693 ~31
2493.333	.645 -116	.862 74	.099 39 `	.638 ~32
7330.070	.631 -119	.848 72	.589 39	.676 -33
7740.000	.620 -122	.848 70	.008 39	.665 -33
7999.0.2	.612 -125	. 232 63	.009 38	.661 -34
30.00.000	.605 -123	.038 65	.000 37	.658 -35
3110.930 .100.330	.598 -132	.032 63	.091 37	.647 -35
333.343	.598 -136 .598 -140	.834 60 .827 58	.991 36 .892 86	.634 +36 .636 +38
3.3.773	.597 -143	.814 55	.092 35	.633 -40
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0000.000	.583 -150	.791 50	.092 33	.621 -44
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12380.33	.460	162	.665	12	.007	15	.633	-72
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10900.00	.481	145	.615	5 2	, 996	1.3	.430	-71
13700.50	.475	146	.5 15	3	.195	1.3	.596	-71
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15730.33	.512	115	.509	-15	.114	6	.635	-83
19200.00	.503	110	.533	-16	.117	5	. 556	-32
15:35.33	.502	109	.569	-13	.117	2	.621	-02
13900.00	.503	196	.563	-21	.116	1	.កញ្ជ	-32
15900.00	.512	102	.563	-23	.113	- 1	.592	-33
13000.33	.510	96	.558	-26	.113	-2	.506	-34
16209.03	.526	90	.584	-23	.121	-3	.590	-33
13433.33	.549	35	.5%4	-31	.133	- 5	.565	-34
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# PAGE 1: 1 ONR PREAMP FOT CHARACTERIZATION

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# PAGE 1: 1 ONR PA #21 FET CHARACTERIZATION

AUG 8 1980

.00 VOLTS,	.00 MA (M	IEAS 1)	#1 VD	D=4V ID=65.0MA
FREQ	Sii	S21	\$12	\$22
(MHZ)	MAG ANG	MAG ANG	MAG ANG	MAG ANG
2000.000	.928 -29	1.794 152	.019 83	.809 -6
2200.000	.922 -32	1.787 149	.021 82	.811 ~8
2400.000	.916 -35	1.789 146	.023 82	.809 ~8
2600.000	.904 -38	1.780 144	.024 81	.808 -9
2800.000	.897 -41	1.787 141	.026 81	.811 -9
30 <b>00.000</b>	.884 -44	1.783 138	.027 80	.805 -10
3200.000	.874 -47	1.791 135	.028 80	.807 ~10
3400.000	.863 -49	1.788 133	.029 80	.805 -11
3600.000	.848 -52	1.781 129	.030 79	.801 -11
3800.000 4000.000	.834 -54 .814 -57	1.793 126 1.787 123	.030 79 .031 79	.800 -11 .793 -11
4200.000	.803 -60	1.762 121	.032 80	.789 -12
4400.000	.785 -64	1.769 117	.032 80	.784 -12
4600.000	.772 -67	1.748 114	.033 81	.778 -12
4800.000	.761 -71	1.759 112	.035 81	.777 -13
5000.000	.746 -75	1.739 108	.035 81	.776 -14
5200.000	.731 -79	1.745 105	.037 81	.772 -15
5400.000	.714 -83	1.721 102	.037 80	.769 -16
5600.000	.696 -88	1.719 98	.038 76	.765 -17
5800.000	.670 -93	1.670 94	.037 69	.754 -19
6000.900	.616 -97	1.603 90	.027 55	.734 -19
6200.000	.588 -96	1.524 90	.015 97	.734 -18
6400.000	.602 -98	1.527 89	.028 120	.752 -19
6600.000	.609 -102	1.552 87	.036 114	.760 -21
6800.000	.604 -107	1.540 84	.039 111	.759 -23
7000.000	.593 -111	1.513 81	.042 111 .044 110	.755 -24 .754 -26
7200.000 7400.000	.584 -114 .577 -118	1.503 78 1.486 76		.754 -26 .752 -27
7600.000	.572 ~121	1.461 74	.046 111	754 -29
7800.000	.565 -125	1.447 71	.052 113	.758 -30
8000.000	.563 -128	1.432 70	.055 113	.762 -31
8200.000	.559 -131	1.420 66	.059 113	.770 -32
8400.000	.551 -134	1.414 65	.062 112	.778 -33
8600.000	.542 -138	1.398 62	.064 112	.776 -34
8800.00 <b>0</b>	.532 -142	1.388 60	.067 111	.773 -36
9000.000	.526 -145	1.375 57	.070 111	.778 -37
9200.000	.522 -149	1.359 54	.073 111	.771 -38
9400.000	.518 -152	1.337 52	.077 111	.772 -39
9600.000	.517 -156	1.332 49	.080 110	.774 -48
9800.000	.515 ~160	1.304 47	.084 109	.770 -41
1000 <b>0.00</b> 10200.00	.515 ~163 .515 ~167	1.288 44	.087 108 .091 107	.773 -42 .778 -44
10400.00	.515 -167 .515 -170	1.268 42 1.253 40	.095 106	.778 -44 .782 -46
10500.00	.512 -172	1.246 38	.098 104	.785 -48
10800.00	.503 -175	1.218 35	.101 103	.796 -50
	497 -178	1.221 33	.105 100	894 -51
11200.00	.489 189	1.183 31	.106 100	.800 -53
11490.00	.469 176	1.133 28	.110 97	.813 -54
11500.00	.468 174	1.173 26	.112 97	.813 -55
11300.3 <b>0</b>	.449 170	1.175 24	.116 95	.815 -56
12000.00	.441 166	1.159 21	.116 94	.814 -56
12200.00	.434 160	1.167 19 A	<b>-19</b> .120 92	.822 -57

12400.00	.420	155	1.162	16	.122	91	.815	-57
12600.00	.417	148	1.147	12	.125	90	.822	-56
12300.00	.415	142	1.154	9	.128	88	.826	-56
13000.00	.414	135	1.104	5	.133	87	.833	-56
13200.00	414	129	1.103	3	.138	85	.841	-57
13400.00	416	124	1.065	0	.142	83	.848	-58
13690.00	.424	118	1.054	-2	.145	80	.852	-60
13800.00	.435	113	1.038	-5	.149	77	.859	-62
14000.00	.448	109	1.025	-9	.151	75	.859	`-65
14200.00	.457	106	1.003	-11	.149	71	.846	-68
14400.00	.461	103	.975	-16	.146	69	.828	-72
14600.00	.461	100	.935	-19	.136	69	.801	-77
14800.00	.445	100	.830	-24	.122	78	.723	-84
15000.00	.484	105	.732	-12	.178	91	.562	-78
15200.00	.535	99	.890	-12	.217	75	.676	-68
15400.00	.528	93	.907	-18	.220	65	.744	-71
15600.00	.518	87	.934	-20	.212	59	.777	-75
15800.00	.508	83	.918	-26	.216	57	.809	-77
16000.00	.503	78	.921	-27	.215	52	.827	-79
16200.00	.500	72	.929	-32	.221	52	.846	-81
16400.00	.505	68	.906	-34	.224	47	.857	-82
16600.00	.516	63	.907	-38	.232	45	.852	-84
16800.00	.541	59	.903	~39	.239	41	.840	-86
17000.00	.569	55	.892	-43	.242	38	.820	-88
17200.00	.601	52	.878	-47	.252	34	.789	-90
17400.30	.630	50	.903	-48	.249	30	.734	-93
17600.00	.650	48	.890	-54	.254	29	.701	-96
17800.00	.646	45	.870	-55	.256	24,	.659	-100
13030.08	.642	44	.908	-61	.262	25	.636	-103

REF PLANE EXT(CM): IN= 5.48, OUT= 5.48

## S-PARAMETER FOR ONR-20 DEVICES DEVICE ONR-20-1

.00 VOLTS,	.00 MA (ME	EAS 1)	VD=4	ID=55 VG=-2.7
FREQ	S11	\$21	\$12	\$22
(MHZ)	MAG ANG	MAG ANG	MAG ANG.	MAG ANG
2000.000	.929 -29	1.835 151	.020 81	.813 -8
2200.000	.922 -33	1.823 149	.021 80	.815 <b>-</b> 9
2400.000	.916 -35	1.819 146	.023 80	.814 -10
2600.000	.906 -38	1.805 143	.024 79	.814 -11
2800.000	.898 -41	1.806 140	.026 79	.817 -11
3000.000	.885 -43	1.798 138	.027 79	811 -12
3200.000	.874 -46	1.797 135	.028 78	.813 -12
	.863 -48	1.790 133	.029 78	812 -12
3400.000	.849 -50	1.776 130	.029 78	.809 -12
3600.000	.835 -53	1.781 127	.030 78	.808 -12
3800.000	.815 -55	1.770 124	.031 78	.803 -12
4000.000	.802 -58	1.736 122	.031 79	.798 -12
4200.000		1.741 119	.032 80	.796 -12
4400.000		1.717 116	.032 81	791 -13
4600.000		1.727 114	.034 82	792 -13
4800.000	.760 -67		.034 83	793 -13
5000.000	.744 -70		.035 85	.791 -14
5200.000	.730 -74		.036 86	790 -15
5400.000	.711 -77			792 -15
5600.000	.695 -81	1.703 102		789 -16
5800.000	.678 -85	1.674 100	.038 88 .039 88	.791 -17
6100.000	.660 -88	1.675 97		.787 -18
6200.000	.641 -92	1.652 95	.040 89 .041 90	.780 -19
6400.000	.622 -96	1.624 92	.042 89	.776 -20
6600.000	.606 -100	1.622 89	.038 95	.769 -20
6800.000	.582 -105	1.589 85	.044 99	.773 -21
7000.000	.561 -106	1.544 85 1.559 82	047 98	.772 -22
7200.000	.559 -111		.049 99	.768 -23
7400.000	.552 -115			.769 -24
7600.000	.545 -119	1.532 77 1.524 74	.051 99 .053 99	.772 -25
7800.000	.536 -124		.055 99	.770 -26
8000.000	.531 -128		.057 98	775 -27
3200.000	.523 -133		.058 96	.778 -28
8400.000	.511 -138		.054 94	763 -30
8600.000	.487 -143	1.441 63 1.403 62	.047 105	749 -29
2300.000	.463 -145		.062 112	779 -29
9000.000	.472 -148		.069 108	777 -31
9200.000	.479 -153		.073 106	.774 -33
9400.000	.484 -158		.076 103	.773 -34
9600.000	.486 -162		.078 102	.765 -36
9800.000	.489 -167		.078 99	.758 -37
10000.00	.496 -171		.071 98	.740 -39
10200.00	.498 -175	1.313 44		.758 -38
_10400.00	.504 -179	1.293 41	.078 111 .091 107	.779 -40
10600.00	.502 179	1.274 48	.096 194	.792 -43
19800.00	.485 176	1.216 38 1.239 37	.099 100	.801 -45
11000.00	.486 175		.101 100	.793 -47
11200.00	.476 173		.104 96	.806 -49
11400.00	.476 169	1.209 32	.104 76	.806 -50
11600.00	.434 166	1.196 29	.110 93	.809 -51
11800.90	.472 162	1.193 27	.109 93	.803 -51
12980.80	.469 158	1.170 25		.814 -52
13200.00	.470 154	1.175 22	A-21.114 91	1017 WE

12400.00	.465	149	1.165	20	.116	91	.808	-52
12600.00	.470	143	1.148	17	.118	90	.812	-51
12800.00	.474	138	1.154	14	.121	89	.816	-51
13000.00	.478	133	1.106	10	.126	88	.820	-51
13200.00	.481	128	1.103	9	.131	86	.828	-51
13400.00	.486	124	1.067	6	.136	85	.832	~52
13600.00	.498	120	1.054	4	.139	83	.837	<b>-5</b> 3
13800.00	.511	117	1.041	3	.145	81	.838	-55
14000.00	.528	114	1.029	- 1	.150	79	.840	-57
14200.00	.540	112	1.009	-2	.153	76	.827	-59
14400.00	.552	109	.993	-6	.157	74	.812	-62
14600.00	.567	108	.979	-7	.160	72	.800	-64
14800.00	.578	106	.968	-11	.163	70	.786	-67
15000.00	.585	105	.943	-11	.167	67	.774	-70
15200.00	.587	103	.941	-14	.169	66	.778	-72
15400.00	.575	101	.904	-16	.177	64	.777	-73
15600.00	.569	98	.924	-16	.177	61	.785	-75
15800.00	.564	95	.904	-21	.184	60	.802	-77
16000.00	.552	92	.909	-21	.188	56	.812	-78
16200.00	.545	88	.916	-26	.194	57	.827	-80
16400.00	.544	84	.890	-28	.201	53	.834	-81
16600.00	.546	79	.883	-32	.209	52	.831	-83
16800.00	.559	75	.867	33	.219	49	.822	-84
17000.00	.582	72	.849	-36	.226	46	.805	-86
17200.00	.606	69	.820	-38	.239	43	.776	~88
17400.00	.633	66	.848	-39	.241	39	.731	-91
17600.00	.652	64	.826	-43	.250	38	.701	-94
17800.00	.654	61	.815	-43	.260	33	.669	-97
18000.00	.646	59	.855	-48	.269	33	.650	-100

REF PLANE EXT(CM): IN= 5.48, OUT= 5.48

## S-PARAMETER FOR ONR-20 DEVICES DEVICE ONR-20-2

.00 VOLTS,	1) AM 00.	IEAS 1)	V D = 4	ID=60 VG=-2.7
FREQ	<b>S11</b> .	\$21	\$12	\$22
(MHZ)	MAG ANG	MAG ANG	MAG ANG	MAG ANG
2000.000	.930 -30	1.806 152	.018 84	.804 -6
2200.000	.924 -33	1.794 149	.019 83	.804 -8
2400.000	.918 -36	1.792 147	.021 82	.804 -8
2600.000	.907 -39	1.779 144	.022 82	.804 -9 .807 -9
2800.000	.900 -41	1.781 141 1.771 139	.023 82 .024 82	.807 -9 .801 -10
3000.000	.886 -44 .877 -46	1.771 139 1.775 136	.026 82	.803 -10
3200.000 3400.000	.867 ~48	1.768 133	.026 82	.803 -11
3600.000	.852 ~50	1.758 130	.027 82	.800 -11
3800.000	.839 ~53	1.766 128	.028 83	799 -10
4000.000	.821 -55	1.761 125	.028 83	.795 -11
4200.000	.806 -57	1.727 123	.029 85	.792 -11
4400.000	.790 -60	1.735 120	.030 86	.789 -11
4600.000	.777 -63	1.713 117	.030 87	.785 -11
4800.000	.765 -67	1.725 115	.031 89	.786 -11
5000.000	.750 -70	1.707 112	.032 90	.786 -12
5200.000	.737 -73	1.716 109	.033 92	.784 -13
5400.000	.719 -77	1.696 106	.034 93	.784 -13
5600.000	.703 -81	1.701 103	.035 94 .037 96	.787 -14 .786 -15
5800.000	.685 - <b>84</b> .668 -88	1.669 100 1.671 97	.037 96 .038 97	.786 -16
6000.00 <b>0</b> 6200.000	.668 -88 .649 -91	1.647 95	.039 98	.782 -16
6400.000	.630 -95	1.621 92	.041 99	.777 -18
6600.000	.615 -99	1.619 90	.043 101	.775 ~18
6800.000	.600 -104	1.599 87	.044 102	.773 -19
7000.000	.582 -107	1.563 84	.046 102	.767 -20
7200.000	.570 -111	1.556 82	.048 103	765 -21
7400.000	.562 -115	1.545 79	.051 104	.761 -22
7600.000	.556 -119	1.520 77	.053 105	.763 -23
7800.000	.548 -123	1.510 74	.055 105	.767 -24
୧୭୭୭.ତ୭୭	.542 -127	1.492 72	.058 105	.767 -24
8200.000	.535 -130	1.476 69	.060 104	.776 -25
8400.000	.525 -135	1.467 67	.063 103	.780 -26
8600.000	.513 -139	1.450 64	.061 101	.768 -27 .760 -26
8899.999	.498 -144 .479 -149	1.428 62 1.392 59	.065 106 .062 103	.780 -27
9688.88 <b>0</b> 9288.88 <b>0</b>	.445 -152	1.332 57	.068 107	.775 -28
9400.000	.438 -151	1.318 57	.077 106	.772 -29
9600.000	.450 -153	1.349 56	.078 104	.772 -30
9000.000	.462 -157	1.348 53	.076 102	.763 -31
10000.00	.467 -161	1.341 50	.069 106	.754 -33
10200.90	.467 -164	1.325 48	.082 119	.754 -33
10400.00	.469 -167	1.316 45	.095 107	.757 -35
10600.00	.465 -169	1.311 44	.100 104	.784 -36
10800.00	.457 -172	1.289 41	.104 103	.794 -38
11900.00	.447 -174	1.299 39	.108 100	.803 -40
11200.00	.425 -176	1.258 36	.111 103	.797 -41
11400.00	.411 -130	1.266 34	.113 99	.312 ~43 .812 <b>~~~</b> 43
11399.00	.406 178	1.264 31 1.269 29	.118 98 .126 96	.812 -46
11989.30 13989.8 <b>0</b>	.382 174 .365 169	1.255 27	.125 95	.803 -46
12200.00	.352 163		·23 .131 93	.819 -47
12209.00	س ب تا سن س ب و			, ,

12400.00 12600.00 12600.00 12800.00 13000.00 13400.00 13600.00 14000.00 14200.00 14600.00 15200.00 15200.00 15200.00 15200.00 15600.00 15600.00 16600.00	.322 15 .314 16 .312 16 .312 17 .317 .329 16 .365 .382 .398 .411 .427 .427 .421 .427 .421 .427 .421 .419 .418 .423 .431 .450 .473 .507 .538	1.268 1.257 1.269 1.225 1.225 1.191 1.193 1.173 1.175 1.154 89 1.175 1.148 86 1.135 82 1.092 1.092 1.081 69 1.081 69 1.081 69 1.092 1.093 1.097 42 .983 .972 .983	21850963134915714490460159 	.134 .137 .142 .148 .156 .169 .177 .186 .199 .208 .219 .219 .229 .219 .229 .224 .259 .275	9988888777766655555444433332	359655205559 8823655205559 884552 884552 884273 884273 884567756 8848 8888 8888 8848 8848	74455478136925803579023579 
16400.00 16600.00	.450 .473 .507 .538	36 .982 32 .972 28 .953 25 .923	-40 -41 -45 -49	.259 .270 .275 .283	38 3 <b>5</b>	.875 .866	-83 -85 -87
17400.00 17600.00 17800.00	.586 .595 .575	22 .942 19 .907 14 .868 11 .887	-51 -56 -57 -62	.284 .296 .300 .324	22 19 18	.743 .707 .697	-94 -97 -100

REF PLANE EXT(CM): IN= 5.48, OUT= 5.48

### S-PARAMETER FOR ONR-20 DEVICES DEVICE ONR-20-3

.00 VOLTS,	.00 MA	(MEAS 1)		V D = 4	ID=60	VG=-2.7
FREQ	S11	\$21		\$12	52	22
(MHZ)	MAG ANG		ANG MAG		MAG	ANG
2000.000	.929 -27		154 .01		.804	~5
2200.000	.922 -31	1.847	151 .02	20 84	.805	~6
2400.000	.915 -34		148 .02		.804	-7
2600.000	.904 -37		146 .02		.804	-7
2800.000	.896 ~39		143 .03		.806	-8
3000.000	.881 -42		140 .03		.798	-8 -9
3200.000	.870 ~45		137 .02 134 .02		.801 .800	-9 -9
3400.090	.858 -48		131 .03		.797	- <del>9</del>
3600.000 3800.000	.828 -53		128 .03		.797	-ģ
4000.000	.808 ~57		125 .0		.791	- ģ
4200.000	.794 ~59		123 .0		.787	- 9 ·
4400.000	.775 ~63		119 .0:		.784	-9
4600.000	.762 -66		117 .03		.774	-10
4800.000	.750 -76		114 .0:	32 90	.779	-10
5000.000	.734 -74	1.763	111 .0		.780	-10
5200.000	.694 -77		108 .0		.778	-11
5400.000	.700 -80		106 .0		.779	-12
5600.000	.691 -8		103 .0		.782	-12
5800.000	.677 -89		100 .0		.781	-13 -14
6000.000	.661 -93		97 .0		.783	-14 -15
6200.000	.639 -96 .625 -98		95 .0 <sup>-</sup>		.773	-16
6400.000 6600.000	.616 -10		91 .0		.771	-16
6300.000	.604 -10		88 .0		.768	-17
7000.000	.588 -10		86 .0		.764	-18
7200.000	.576 -112		83 .0		.761	-19
7400.000	.570 -11		81 .0		.757	-20
7600.000	.564 -11		79 .0	54 108	.760	-21
7800.000	.555 -12		77 .0		.766	-21
8000.000	.548 -12		75 .0		.767	-22
8200.000	.539 -12		72 .0		.776	-23
8400.000	.528 -13		71 .0		.783 .779	-24 -25
8600.000	.515 -13: .502 -14:		68 .0		770	-25 -26
8800.000 9000.000	.494 -14		63 .0		759	
9200.000	.489 -14			69 118	.768	-25
9400.000	.480 -15		58 .0		.777	-26
9600.000	.474 -15			84 112	.779	
9800.000	.468 -16		53 .0		.773	-29
10000.00	.470 -16			92 109	.772	-30
10200.00	.466 -17			96 107	.776	-32
10400.00	.444 -17			99 105	.774	-34
10600.00	.439 -17			98 101	.764	-36
10800.00	.445 -17			89 109	.758	-35 -37
11000.00	.444 17			09 108 14 105	.805 .803	-40
11290.00 11400.30	.428 17 .421 17			14 105 19 101	.817	-41
11450.00	.422 16			21 100	.816	-43
11800.00	.408 16			27 97	.822	-44
12000.00	.401 15			25 96	.816	-44
12220.00	.397 15		26 <b>A-25</b> .1		.827	-45

THE RESERVE OF THE PROPERTY OF

12400.00	.389	147	1.219	23	.133	93	.819	-45
12600.00	.390	141	1.202	20	.135	93	.823	-44
12800.00	.391	134	1.203	17	.139	92	.828	-43
13000.00	.395	127	1.156	13	.144	91	.835	-43
13200.00	.398	122	1.149	12	.150	89	.842	-44
13400.00	.403	117	1.111	9	.157	88	.851	-44
13600.00	.414	112	1.099	7	.162	85	.859	-45
13800.00	.429	108	1.086	6	.169	83 -	.864	-47
14000.00	.445	104	1.087	2	.176	81	.869	-48
14200.00	.459	100	1.065	1	.180	78	.860	-50
14400.00	.472	97	1.064	-3	.186	75	.845	-53
14600.00	.485	95	1.049	-4	.190	72	.834	-56
14800.00	.492	91	1.045	-8	.194	70	.820	-58
15000.00	.496	88	1.017	-10	.199	67	.806	-61
15200.00	.495	85	1.009	-13	.202	65	.807	-62
15400.00	.483	80	.965	-16	.210	62	.805	-64
15600.00	.478	76	.970	-16	.210	60	.811	-66
15800.00	.473	71	.953	-21	.222	58	.829	-68
16000.00	.473	65	.940	-21	.225	54	.838	-69
16200.00	.476	59	.951	-25	.239	53	.844	-71
16400.00	.491	54	.918	-27	.228	47	.861	-71
16600.00	.508	49	.921	31	.240	48	.872	-73
16800.00	.541	45	.910	-32	.253	45	.869	-75
17000.00	.576	41	.896	-36	.262	42	.854	-77
17200.00	.611	38	.872	-39	.276	38	.823	-79
17400.00	.642	35	.884	-41	.273	34	.773	-82
17600.00	.653	32	.862	-45	.282	33	.740	-85
17800.00	.641	28	.823	-46	.285	29	.699	-89
18000.00	.620	26	.847	-51	.299	30	.675	-91

REF PLANE EXT(CM): IN= 5.48, OUT= 5.48

# PAGE 1: 1 ONR PA #21 FET CHARACTERIZATION

	•			
		9 <b>5</b> 1)	#2 VDD	=44 ID=55.0MA
.00 VOLTS,	.00 MA (ME	H2 1)		\$22
	211	221	S12 Mag ang	MAG ANG
FREQ (MHZ)	MAG ANG	MAG ANG	MAG ANG .022 83	<b>,</b> 800 ~5
2000.000	.932 -28	1.732 153 1.724 150	.024 81	.801 <sup>-7</sup>
2200.000	.926 -31	1.724 150 1.724 147	.026 81	.800 ~7 .798 ~8
2400.000	.920 -34 .910 -37	1.713 145	.027 81	.798 ~8 .803 ~9
2600.000	.910 -37 .904 -40	1.717 142	.029 80 .030 79	.797 ~9
2600.000 3000.000	.891 -42	1.709 140	.030 79 .032 79	. 797 -10
3200.000	.881 -45	1.711 137	.033 78	.797 -10
3400.000	.872 -47	1.705 134 1.693 131	.034 77	.794 -10 .792 -10
3600.000	.859 -49 .845 -52	1.699 128	.035 77	.792 -10 .787 -10
3800.000	.827 -54	1.687 125	.036 77 .037 77	784 -10
4000.000 4200.000	.818 -56	1.659 123	.037 77 .038 78	.781 -10
4400.000	.801 -59	1.664 120 1.639 118	.038 78	.776 -11
4600.000	.789 -62 : 778 -65	1.647 115	.040 78	.777 -11 .777 -11
4860.060	778 -65 763 -69	1.629 112	.041 78	.777 -11 .773 -12
5000.000 5200.000	.750 -72	1.637 110	.042 79 .043 77	771 -13
5400.000	.732 -75	1.618 107 1.620 103	.044 74	.770 -13
5600.000	.711 -80 .682 -84	1.620 103 1.578 100	.042 69	.759 -15 .746 -14
5800.000	.682 -84 .624 -86	1,516 97	.033 62 .026 88	750 -13
6000.000 6200.000	.613 -86	1.473 97	.026 88 .034 102	760 -14
6400.000	.620 -88	1.477 96 1.495 93	.040 101	.763 -15
6600.000	.618 -93 .607 -97	1.490 90	.043 100	761 -16 757 -17
6800.000	.607 -97 .593 -101	1.467 88	.045 101	.757 -17 .756 -17
7999.899 7299.999	.580 -105	1.467 86	.047 101 .049 103	752 -18
7400.000	.569 ~109	1.456 83	.051 105	.753 -18
7600.000	.563 -112	1.436 82 1.433 79	.054 105	.755 -19 .754 -20
7800.000	.553 -116 .549 -120	1.422 78	.057 106	.754 -20 .762 -21
8000.000 8200.000	.544 -124	1.416 74	.060 106 .063 107	768 -21
8200.000	.537 -128	1.415 73	.065 107	.763 -22
8690.999	.529 -132	1.406 79 1.400 68	.068 107	.759 -23 .762 -24
გგიც.000	.521 -137 .517 -141	1 391 65	.071 107	.762 -24 .753 -25
9000.000	.515 -145	1.381 62	.074 107 .077 107	750 -25
9200.000 9400.000	.514 -149	1.358 60 1.355 57	081 107	.749 -26
9600.000	.517 -153	1.355 57 1.326 55	.085 107	.742 -28 .740 -29
9800.000	.519 -157 .522 -160	1.309 52	.088 107	.740 -29 .742 -31
19999.99	.522 -160 .526 -164	1.288 50	.092 106 .096 105	742 -33
18288.09 18488.09	.531 -167	1.274 48	.096 105 .100 104	.741 -35
10600.90	.532 -169	1.268 46 1.240 43	.103 103	.749 -37 .757 -39
10800.00	.527 -171 .524 -173	1.244 41	.106 101	.757 -39 .752 -41
11000.00	.524 -173 .508 -175	1.203 39	.108 102 .112 99	.764 -42
11299.99 _11409.99	.501 -179	1.204 37	.112 99 .115 99	.765 -44
11600.00	.503 180	1.193 35 1.190 33		.770 -45
11800.00	.485. 176 .478 172	1 177 31	.121 96	.767 -45 .777 -47
12909.88	.478 172 .473 168	200	A-27 .125 95	*(()
12200.30				-

	404	162	1.174	26	.128	94	.772	-45
12400.00	.461	163	1.164	23	.131	94	.774	-45
12600.00	.459	157	1.171	20	.135	92	.779	-45
12800.00	.457	151		16	.140	92	.783	-45
13000.00	.458	145	1.131	14	.146	90	.789	-46
13200.00	.456	139	1.126		.152	89	.795	-47
13400.00	.462	133	1.094	11	.156	87	.798	-47
13600.00	.473	128	1.079	9	.162	84	.800	-49
13800.00	.487	123	1.064	7		83	.804	-51
14000.00	.507	119	1.059	4	.168	80	.794	-53
14200.00	.523	116	1.033	3	.172	78	.779	-55
14400.00	.538	113	1.023	-2	.176	75	.772	-58
14600.00	.559	110	1.007	-3	.180	74	.760	-61
14800.00	.573	108	.996	-6	.183		.745	-63
15000.00	.588	106	.969	-8	.188	70	750	-65
12000.00	.596	104	.960	-10	.190	69	.744	-67
15200.00	.590	102	.921	-13	.196	66		-69
15400.00	.588	99	.927	-14	.195	64	.752	-71
15600.00	.584	96	.908	-18	.201	63	.769	-73
15800.00		93	.898	-18	.203	60	.781	
16000.00	.579	90	.902	-22	.209	60	.794	-75
16200.00	.572	87	.873	-24	.214	57	.802	-76
16400.00	.573	84	.866	-27	.222	56	.800	-77
16600.90	.575		.853	-28	.231	53	.794	-79
16890.00	.588	81	.836	-31	.235	50	.780	-80
17000.00	.611	78		-33	.245	47	.756	-82
17200.00	.635	76	.819	-34	.247	43	.713	-85
17400.00	.665	74	.848	-3 <del>7</del>	.249	42	.681	-89
17699.00	.685	73	.826		.254	38	.652	-92
17800.00	.694	72	.817	-38	.253	39	.631	-95
12200.00	.684	70	.852	-43	.233	~ .		

REF PLANE EXT(CM): IN= 5.48, OUT= 5.48

## ONR PA #21 FET CHARACTERIZATION

.00 VOLTS,	.00 MA (ME	EAS 1)	•	*3 YDD=4V	ID=65.0MA
FREQ	\$11	\$21	\$12		\$22
(MHZ)	MAG ANG	MAG ANG	MAG	ANG MA	
2000.000	.930 -31	1.824 152	.019	82 .8	10 -6
2200.000	.923 -34	1.813 149	.021	81 .8	11 -8
<del>_</del>	.917 -37	1.812 146	.023		99 -8
2400.000		1.799 143	.024		09 -9
2600.000	.907 -40		.026		11 -10
2800.000	.900 -42	•	.027		05 -10
3000.000	.887 -45	1.793 138			07 -11
3200.000	.877 -48	1.796 135	.028		806 -11
3400.000	.867 -50	1.790 132	.028		
3600.000	.853 -52	1.776 129	.029		
3800.000	.841 -55	1.783 126	.030		
4000.000	.822 -58	1.772 123	.031	78 .7	
4200.000	.811 -60	1.742 121	.031		92 -12
4400.000	.795 -63	1.745 118	.032		89 -12
4600.000	.783 -67	1.719 115	.033		783 -12
4800.000	.773 -70	1.726 113	.034		783 -13
5000.000	759 -74	1.706 109	.034		783 -13
5200.000	747 -77	1.712 107	.036		779 -14
5400.000	.730 -81	1.688 104	.036		779 -15
	.712 -85	1.686 100	.037	75	776 -16
5600.000	.686 -90	1.640 96	.035	69	764 -17
5800.000	.636 -93	1,581 93	.027		750 -17
6007.000	.612 -92	1.514 93			751 -16
6209.000	.623 -94	1.515 92	.028		763 -17
6400.000	.626 -98	1.537 90	.035		767 -18
6600.000		1.525 87			766 -20
6800.000		1.498 84			761 -21
7000.000	.606 -105				759 -22
7200.000	.597 -109				754 -22
7400.000	.588 -112				757 -24
7600.000	.583 -115	1.463 78			760 -25
7800.000	.575 -119	1.454 75			761 -26
8000.000	.571 -122	1.446 74			769 -27
8200.000	,565 ~125	1.438 71			776 -28
8400.000	.557 -128	1.440 69			772 -29
8600.000	.548 -132	1.431 66			768 -30
8800.000	.538 -135	1.427 64			771 -31
9000.000	.530 -139	1.417 61			764 -33
9200.000	.525 -143	1.404 58			764 -34
9400.000	.520 -146	1.381 56			
9600.000	.517 -150	1.380 53			
9800.000	.516 -154	1.352 53			760 -36
10000.00	.515 -157	1.336 48			761 -38
10200.00	.515 -161	1.318 46			766 -40
10400.00	.516 -164	1.304 4			769 -42
10600.00	.514 -166	1.300 43			772 -44
10830.03	.507 -169	1.272 3			782 -46
11000.00	.502 -172	1.277 3	7 .103		793 -48
11200.00	.483 -174	1.231 3			787 -50
11400.00	.474 -177	1.233 3			899 -51
11500.00	.474 -179	1.220 3			802 -52
11800.00	.455 177	1.219 2		• '	.807 <b>-</b> 53
12090.99	.447 173	1.201 2			805 -53
12280.80	.440 168	1.209 2	3 A-29 .120		814 -54
12200.00	* 4 4 0 0 V				

.426	163	1.201	21	.123	94	.809	-53
.423	157	1.191	18	.125	93	.815	-52
.420	151	1.199	15		92	.818	-51
.420	145	1.156	1 1		91	.824	-51
.418	138	1.157	9		90		-51
.422	133	1.124	7				-52
.431	127	1.116	4				-53
		1.103					-54
		1.098					-56
	115						-58
	112	1.070	-7				-60
		1.059	-8		_		-63
	107	1.052	-12				-65
	104	1.030	-13				-68
.524	102	1.029	-16		66		-70
.518	99	.993	-18		64	.795	-72
.515	96	1.015	-19		60	.803	-74
.513	92	.999	-24	.205	59	.820	-76
.510	88	1.006	-24	.209		.834	-78
.507	84	1.018	-29			.847	-81
.513	79	.990	-31	.223			-83
.522	75	.990	35	.231	49	.846	-85
.544	71	.980	-37	.240		.835	-87
.572	68	.963	-41	.244	42	.813	-90
.603	65	.941	-44	.255	38	.782	-93
.635	62	.969	-45	.252	34	.732	-97
.659	61	.950	-50	.256	33	.702	-101
.664	59	.934	-52	.259	27	.669	-105
.659	58	.973	-58	.262	28	.655	-109
	.420 .420 .421 .421 .432 .432 .432 .432 .432 .432 .432 .532 .5313 .5312 .5313	.423 157 .420 145 .418 138 .422 133 .431 127 .442 123 .459 118 .473 115 .484 112 .502 109 .513 107 .521 104 .524 102 .518 99 .515 96 .513 92 .510 88 .507 84 .513 79 .522 75 .544 71 .572 68 .603 65 .635 62 .659 61 .664 59	.423 157 1.191 .420 151 1.199 .420 145 1.156 .418 138 1.157 .422 133 1.124 .431 127 1.116 .442 123 1.103 .459 118 1.098 .473 115 1.079 .484 112 1.070 .502 109 1.059 .513 107 1.052 .521 104 1.030 .524 102 1.029 .518 99 .993 .515 96 1.015 .513 92 .999 .515 96 1.015 .513 92 .999 .510 88 1.006 .507 84 1.018 .513 79 .990 .522 75 .990 .544 71 .980 .572 68 .963 .603 65 .941 .635 62 .969 .659 61 .950 .664 59 .934	.423 157 1.191 18 .420 151 1.199 15 .420 145 1.156 11 .418 138 1.157 9 .422 133 1.124 7 .431 127 1.116 4 .442 123 1.103 3 .459 118 1.098 -1 .473 115 1.079 -2 .484 112 1.070 -7 .502 109 1.059 -8 .513 107 1.052 -12 .521 104 1.030 -13 .524 102 1.029 -16 .518 99 .993 -18 .515 96 1.015 -19 .513 92 .999 -24 .510 88 1.006 -24 .507 84 1.018 -29 .513 79 .990 -31 .522 75 .990 -35 .544 71 .980 -37 .572 68 .963 -41 .603 65 .941 -44 .635 62 .969 -45 .659 61 .950 -50 .664 59 .934 -52	.423       157       1.191       18       .125         .420       151       1.199       15       .129         .420       145       1.156       11       .134         .418       138       1.157       9       .140         .422       133       1.124       7       .146         .431       127       1.116       4       .151         .442       123       1.103       3       .157         .459       118       1.098       -1       .163         .473       115       1.079       -2       .167         .484       112       1.070       -7       .172         .502       109       1.059       -8       .177         .513       107       1.052       -12       .180         .524       102       1.029       -16       .189         .513       99       .993       -18       .198         .513       92       .999       -24       .205         .510       88       1.006       -24       .209         .513       79       .990       -35       .231         .544       71	.423       157       1.191       18       .125       93         .420       151       1.199       15       .129       92         .420       145       1.156       11       .134       91         .418       138       1.157       9       .140       90         .422       133       1.124       7       .146       88         .431       127       1.116       4       .151       86         .442       123       1.103       3       .157       83         .459       118       1.098       -1       .163       81         .473       115       1.079       -2       .167       78         .484       112       1.070       -7       .172       76         .502       109       1.059       -8       .177       74         .513       107       1.052       -12       .180       72         .521       104       1.030       -13       .186       68         .524       102       1.029       -16       .189       66         .513       99       .93       -18       .198       64	.423       157       1.191       18       .125       93       .815         .420       151       1.199       15       .129       92       .818         .420       145       1.156       11       .134       91       .824         .418       138       1.157       9       .140       90       .833         .422       133       1.124       7       .146       88       .837         .431       127       1.116       4       .151       86       .844         .442       123       1.103       3       .157       83       .846         .459       118       1.098       -1       .163       81       .849         .473       115       1.079       -2       .167       78       .839         .484       112       1.070       -7       .172       76       .824         .502       109       1.059       -8       .177       74       .815         .513       107       1.052       -12       .180       .72       .803         .521       104       1.030       -13       .186       68       .791         .

REF PLANE EXT(CM): IN= 5.48, OUT= 5.48

## ONR28 FET CHARACTERIZATION

.00 VOLTS,	.00 MA (M	EAS 1)	#3 V	DD=3V ID=20.0MA
FREQ	S 1 1	S21	\$12	\$22
(MHZ)	MAG ANG	MAG ANG	MAG ANG	MAG ANG
2000.000	.927 -31	1.752 148	.067 72	.719 -12
2200.000	.914 -34	1.751 145	.073 71	.716 -13
2400.000	.897 -38	1.741 141	.079 69	.712 -15
2600.000	.888 -41	1.736 138	.085 67	.708 -16
2800.000	.865 -46	1.727 134	.090 65	.701 -17
3000.000	.849 -50	1.712 131	.095 64	.697 -18
3200.000	.835 -54	1.698 128	.099 62 .103 61	.691 -18 .686 -19
3400.000	.822 -58 .806 -63	1.674 125 1.664 122	.103 61 .107 59	.678 -19
3600.000	.806 -63 .791 -67	1.647 119	.111 57	671 -19
38 <b>00.</b> 000 4000.000	.780 -70	1.621 116	.113 56	.664 -19
4200.000	.762 -74	1.590 113	.116 55	.651 -20
4400.000	.748 -77	1.571 110	.119 54	647 -20
4600.000		1.555 107	.121 53	.638 -20
4300.000	.721 -84	1.546 105	.124 51	.628 -20
5000.000	.700 -87	1.533 102	.127 51	.620 -21
5200.000	.685 ~90	1.522 99	.130 49	.612 -21
5400.000	.669 -94	1.513 97	.133 48	.602 -22 .593 -23
5600.000	.648 -98	1.493 93	.136 46 .136 43	.573 -23
5800.000	.617 -103 .572 -106	1.468 90 1.410 87	.136 43 .126 40	.554 -22
6000.000	.572 -106 .561 -106	1.383 87	.120 45	.566 ~22
6200.000 6400.000	.569 -109	1.394 85	.126 47	.569 -23
6600.000	.570 -113	1.398 83	.131 47	.566 -24
6800.000	.555 -117	1.397 80	.135 46	.557 -25
7000.000	.543 -120	1.384 78	.136 46	·.551 ~25
7200.000	.527 -124	1.368 75	.138 45	.543 -26
7400.000	.513 -128	1.357 73	.139 45	.537 -26
7600.000	.499 -132	1.353 70	.141 45	.530 -27 .524 -28
7800.000	.485 -136	1.338 68	.142 44 .145 44	.517 -28
8000.000	.472 -141	1.331 66 1.312 63	.145 43	507 -29
8200.000 8400.000	.463 -146 .456 -151	1.307 61	.148 43	.498 -30
8600.000	.454 -157	1.293 58	.148 43	488 -30
8800.000	.454 -162	1.274 56	.149 42	· .478 -31
9000.000	.454 -166	1,258 53	.151 42	470 -32
9200.000	.460 -171	1.246 51	.152 42	.463 -33
9400.000	.461 -174	1.233 49	.154 41	456 -34
9600.000	.464 -178	1.222 47	.155 41	.450 -34 .441 -35
9800.000	.466 178	1.207 44	.157 41	.441 -35 .430 -36
10000.00	.462 175	1.197 42	.159 40 .162 40	.424 -38
10200.00	.461 171 .459 167	1.190 40 1.173 38	.164 40	.413 -39
10400.00 10600.00	.459 167 .455 163	1.159 35	.165 39	.401 -41
10300.00	.453 158	1.139 33	.166 38	.393 -43
11800.00	.458 154	1.141 30	.171 38	.387 -46
11200.00	.460 149	1.120 28	.172 37	.383 -49
11430.00	.464 145	1.101 25	.174 36	.382 -51
11600.30	.475 142	1.086 23	.174 36	.379 -51
11300.90	.475 138	1.064 21	.173 35	.378 -53 381 -53
12999.99	.488 135	1.049 19	.179 34	.381 -53 .376 -54
12300.00	.437 132	1.027 17 A	<b>-31 .</b> 181 34	.310 -34

	0.44	1.84	.07	-14.82	1.75	.05
12400.00	2.41	2.04	.15	-14.50	1.62	.05
12600.00	2.70		.11	-14.31	1.61	.05
12800.00	2.63	1.98	05	-14.16	1,63	.05
13000.00	2.40	1.78	07	-13.93	1.60	.05
13200.00	2.38	1.76	17	-13.72	1.59	.05
13400.00	2.26	1.65		-13.53	1.58	.04
13600.00	2.15	1.56	26	-13.42	1.57	.04
13800.00	2.07	1.50	37		1.57	.04
14000.00	1.94	1.38	52	-13.26	1.55	.04
14200.00	1.85	1.30	63	-13.11	1.51	.03
14400.00	1.87	1.29	74	-12.93	1.52	.03
14600.00	1.72	1.16	91	-12.87	1.48	.03
14800.00	1.71	1.12	-1.03	-12.67		.03
15000.00	1.65	1.06	-1.10	-12.55	1.47	.03
15200.00	1.46	.88	-1.27	-12.36	1.48	.03
15400.00	1.46	.85	-1.34	-12.14	1.44	.03
15600.00	1.24	.65	-1.54	-12.02	1.46	.03
15800.00	1.14	.56	-1.63	-11.81	1.44	
16000.00	1.09	.49	-1.78	-11.61	1.41	.03
16200.00	.86	.31	-1.98	-11.53	1.43	.03
16400.00	.67	.14	-2.20	-11.37	1.43	.03
16600.00	.76	.20	~2.30	-11.20	1.38	.03
16800.00	.58	.05	~2.58	-11.18	1.39	.03
17000.00	.56	.02	-2.74	-11.07	1.36	.04
17200.00	.45	09	-3.00	-10.96	1.35	.04
17400.00	.47	08	-3.06	-10.83	1.33	.04
17600.00	.41	15	-3.19	-10.58	1.30	.04
	.34	22	-3.32	-10.44	1.29	.05
17800.00 18000.00	~.03	51	-3.47	-10.26	1.33	.05
10000.00						

REF PLANE EXT(CM): IN= 5.48, OUT= 5.48

## ONR28 FET CHARACTERIZATION

	.00 VOLTS,	.00 MA (ME	AS 1)		#5 VDD:	=3V ID=25.0MA
_	FREQ	<b>S11</b>	\$21	51	2	\$22
	(MHZ)	MAG ANG	MAG AN	G MAG	ANG	MAG ANG
8	2000.000	.954 -16	.252 14			.538 -10
	2200.000	.951 -18	.260 14		78	.540 -11
1	240 <b>0.</b> 000	.949 -19	.265 14		77	.540 -13
1	2600.000	.947 -21	.269 13		76	.542 -14
•	2300.000	.938 -24	.273 13		75	.540 -15
•	3000.000	.934 -26	.278 13			.542 -16
I	3200.000	.933 -28	.281 13		73	.541 -16
4	3400.000 3600.000	.925 -31 .922 -34	.282 12 .285 12		72 70	.543 -17
	3800.000	.920 -36	.290 12		69	.541 -17 540 -18
1	4000.000	.917 -39	.293 11			.537 -18
1	4200.000	.908 -41	.301 11		67	.532 -18
	4400.000	.909 -43	.303 11		66	.532 -19
-	4600.000	.903 -45	.305 11			.526 -19
I	4800.000	.898 -46	.308 10			.521 -20
4	5000.090	.891 -48	.311 10		63	.516 -20
	5200.000	.888 -49	.316 10		61	.510 -21
7	5400.000	.878 -52	.324 10	1 .112	60	.504 -22
1	5600.000	.871 -54		7 .116		.499 -23
•	5800.000	.851 -57		4 .119	54	.485 -24
-	6000.000	.824 -59		1 .111		.473 -23
I	6200.000	.823 -59		3 .101	54	.482 -23
4	6400.000	.832 -61		2 .107	58	.483 -24
	6600.000	.839 -64		0 .115	58	481 -26
T	6890.000	.826 -66		7 .120	57	475 -27
I	7000.000 7200.000	.821 -69 .817 -70		5 .123	56 55	.470 -27 .463 -28
•	7400.000	.802 -72		3 .126	54	.456 -29
•	7600.000	.791 -75		9 .132	54	448 -29
ł	7800.000	.784 -77		7 .134	53	.440 -30
7	8000.000	.769 -80		5 .138	52	.434 -31
	8200.000	.750 -83		3 .141	50	.427 -32
T	8400.000	.737 -87		0 .145	49	.418 -34
1	8600.000	.725 -91		8 .147	48	.408 -35
•	8800.000	.714 -96		5 .149	47	.399 -36
-	9000.000	.708 -100		2 .153	45	.391 -38
I	9200.000	.702 -105		0 .155	44	.383 -39
•	9400.000	.702 -108		7 .157	43	.376 -40
	9600.000	.696 -112		5 .159	41	.371 -42
1	9800.600	.687 -116		.161	40	.360 -43
I	10000.00	.677 -119 .667 -123		9 .163	38	.350 -45 .344 -47
_	10200.00	.667 -123 .651 -127		.166	37 35	.344 -47 .333 -50
•	10400.99 10600.99	.635 -131		2 .168	34	.323 -52
I	10000.00	.620 -136		9 .168	33	.317 -54
-	11000.00	.620 -141		6 .173	31	.316 -57
	11200.30	.609 -146		13 .174	29	.315 -60
1	11400.00	.603 -151		9 .176	27	.315 -62
Į	11600.00	.610 -156		7 .176	26 2.	.317 -62
-	11998 0	.599 -160		5 .180	24	.318 -63
•	12000.00	.698 -165		.180	23	.322 -62
I	12200.30	.602 -169		9 A-33 .181	22	.318 -61
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12400.00	.561 -172	.419	17	.173	20	.307	-59
12600.00	.590 -178	3 .445	14	.187	18	.309	-57
12800.00	.585 177	7 .454	12	.190	17	.297	-54
13000.00	.574 171	.452	9	.192	16	.279	-51
13200.00	.571 165	.453	. 6	.197	13	.258	-48
13400.00	.573 159	.451	3	.201	12	.235	-46
13600.00	.572 153		-0	.204	10	.210	-44
13800.00	.579 148	3 .444	~3	.206	8	.186	-42
14000.00	.581 143		-6	.208	6	.159	-40
14200.00	.584 139		-9	.212	3	.133	-40
14400.00	.592 135	.437	-11	.216	2	.113	-40
14600.00	.592 136	3 .437	-14	.217	-0	.094	-41
14800.00	.594 126	.436	-17	.221	-2	.079	-40
15080.00	.595 122	2 .439	-19	.226	-4	.066	-39
15200.00	.587 116	.438	-23	.229	-6	.054	-36
15400.00	.586 110	3 .437	-26	.236	-8	.046	-26
15600.00	.588 104	4 .429	-29	.238	-10	.046	-10
15800.00	.589 98	3 .427	-32	.244	-13	.042	14
16000.00	.600 92	2 .420	-35	.248	-15	.049	38
16200.00	.608 87	7 .411	-38	.251	-18	.065	53
16400.00	.615 83	2 .403	-41	.254	-21	.081	62
16600.00	630 78	3 .401	-42	.259	-22	.099	67
16800.00	.639 7	4 .393	-45	.259	-25	.116	70
17000.00	.649 71	3 .398	-47	.262	-28	.133	71
17200.00	.656 6	5 .387	-50	.265	-30	.148	7.1
17400.00	.662 6	1.385	-52	.267	-32	.164	71
17600.00	.666 57	7 .383	-55	.274	-33	.176	70
17300.00	.673 50	3 .377	-57	.277	-35	.187	69
18000.00	.659 41	∍ .368	~60	.282	-38	.197	67

REF PLANE EXT(CM): IN= 5.48, OUT= 5.48

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#1 VB=4V ID=35.689 .ee Me IMEEC 1 1 , 10 " .TC; ភព។ ្យាម ខ 811 四十三日 ANG MAG MOS กมอ BMG AMG MAG .043 1 1121 **~** ⊗ 77 ાં શકે ઉ 1 -1 + .007 2000 -99 ្រាក់ក្សាស្រា .340 -8 76 . @ ? **5** .a.H SS A.D M SS A.D M 2.101 141 .087  $- \in \mathbb{S}$ .807 76 .026 137 2.168 2.189 .872 -47 .8:2 -1.0.023 7.5 104 -- 5- 1 .854 -1.0.829 , 139 74 2.149 131 .032 -55 .923 -12 .031 7.3 127 0.116 -59 .013 .321 7.3 -13 .332 123 2.103 51343.9 3 34.93.0 5.03.0 .797 .775 -64 .830 -14 72 . 933 1.33 2.062 -€6 -72 -14 72 .015 . 533 .758 .739 .733 117 មួន។ ខេត្ .813 -1672 . 436 2.002 -76 110 33. · · · · -16 72 .012 .006 1.969 119  $- \in \mathfrak{g}$ .810 -17 72 .037 1.927 197 -04 .810 72 -18 .037 104 1.607 -00 1.894 30.000 -18 .810 72 .038 191 1.868 -92 -18 72 .039. .808 1.808 . 93 .652 -96 5.54 (4.6) -19.804 .939 72 1.808 95 1, 19, 19, 19 1, 19, 19, 19 -160 .629 .802 -19 1.772 .039 72 93 .608 -365 .800 -20 1.755 71 . 441 33 54 (8.20) 5358.000 -109 .592 .794 -20 67 1.216 .041 36 .566 -114 **5**7.3 .777 .000 -104 .031 -108 .050 -102 .477 -100 -21 .037 1.674 82 .763 -19. 116 65 1.535 30 5 / 10 · .794 -19 .031 111 1.541 32 .005 -20 .041 104 1.55 79 .494 -175 44 M.S. -21 .894 101 77 .045 1.571 . 204 -101 10 **10 .** 12 13 -22 .805 9.2 .047 73 .405 -136 1.559 9.7 -23 .801 .349 93 71 1.542 19 3 . · · · · .798 -24 .751 93 ,866 -147 68 1.519 -35 .797 94 .953 1,493 65 .657 -155 .793 100 -26 2.074 6.3្អក្ភ -150 .702 .703 .703 .701 3.000 ,35<u>0</u> -27 190 -6.35.0 - 1 A B 79. OK. 4.15 -: C 150  $\underline{1} \supseteq 1$ 5 ) -113 1000 1). , 10.5 1 - 1 .449 -172 .454 -177 .458 -179 1.400 5.53 - 5 1 . 7 . . 1111 1.000 1.000 1.000 1.000  $\mathbf{g}_{i,k}^{\mathrm{out}} = \mathbf{g}_{i,k}^{\mathrm{out}}$ 5 1 .703 .703 .704 .704 77 7. 4.0 i . 4.5 .465 . Ç-3 1.090 1.090 1.7 4.3 . O. 9 . . . 43 ..... • 1, 12 . 7 . 3 -46 1.047 3.3 3.3 1000 - 41 3 5 . 30 771

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TRW DEFENSE AND SPACE SYSTEMS GROUP REDONDO BEACH CA MONOLITHIC MICROWAVE PREAMPLIFIER.(U) JUL 81 A BENAVIDES, R KAELBERER, T S LIN NOODI TRW-S/N-32153.000 AD-A104 857 F/G 9/5 N00014-77-C-0645 UNCLASSIFIED NI 2 ...; 4.04677 END DATE 18 O

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-		4.5	-100	1 . i	58	7.4		.072	92	.7		- 2 -	
· · · · · · · · · · · · · · · · · · ·		4 4 in 13		1.1		7.3		.074	24	.7		-20	
				1.1		8.0		.179	9.5	.7		2:	
		4400		1.1		5.7		. 17 34	27			~22	
			~1.47	1.1		6.5		. 108	9.9			2.1	
			-152	1.0		5 -2		14	1.34	.7		<b>~</b> ⊕	
				1.0		ال ق		.193	1/1/		. 3	<del>-</del> 25	
		. 41144	~ 1 E 1	1.0		53		.137	100			<b>~</b> ,₹1	
* 1 * * * * * * * * * * * * * * * * * *		, a. ; ;	-165	1.0		55		. 1.15	1 3 2		1.3	-25	
		. · · . · · ·	~ 1 C 9	1.0		<b>9</b> 0		<b>CLD4</b>	1 13		} 1	$- \lesssim i$	
1			+173	1.0		'5 1,		. 133	1.33		2.4	~ 3 C	
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			113	1 . :		4.77		. 13	! ! :	. 7	1. 7.	<b>-</b> 0€	
			3 In	1 .		1 :				• 1	. ;	• • •	
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13 32.77	.206	155	.947	1.6	.297	? l	.533	-50
	.359	148	9.25	10	. 206	1 3	.507	-54
: 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	.410	1.4.	.907	1.0	1336	0.5	.615	-53
	.417		.091	.3	. 101	1 1	.633	-53
		20 <del>1</del>	.878	•	. ( 3 5	(1)	. 5 3 4	-53
	.407		175	٠,	1171	, ,	.3.29	-50 -50 -50
	.415.			- 3 - 2	1.3	13	.311	-54
	.∻ପୁପ୍	115	(1 . ()	_ 3	. 1	2.1	. 5 14	-85
	. 466	110	.ស្នប	- ÷	1.155		3.13	-50
1 · · · · · · ·	,476	5.5	. 61.9			1 1	6 17	- 5
7	, A 11 (1)	1.6.1	.១១។	- 7	, 1 5 3		. 5 - 7	-59
	.501	5.7	114	- 7	. 1 5 3		.613	-61
	. 5 / 3	C) (	- 7° ''	-11	. 1 3 13	2.2		-64 -64
	.500	5.41	4 4 4 7	- 1 -1	. 1 7 7	-3.3	. 6 ; ;	
	. 55 %	6.6	.748	-13	. 150	/ 3	.642	-66
	🔩 🖫 គឺម៉ា	5.73	.743	-19	3.15	* 3	.641	-67 -67
	15	7.5	.736	-21	.169	2.9	.୫33	-69
	.500 .550	7.5	.717	-23	.173	. 9	. 3 3 5	-71
	.ទី៤៦	7.2	.730	-26	.177	29	.630	-72
	.ຮັຕສິ	់ 8	.691	-23	.104	2.0	.6%3	-73
	1351	4. 15	.680	3:0	.100	. 3	.633	-75
	in the second	6.0	.634	312	.133	- (1) - (1) - (1) - (1)	.310	-77
		1.1		15 3	1	9.5	. 15 i A	-7:
•		1 2						+ 5.1 - 5.1
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			}	• •				-162
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4			. •			1	,	

PAGE 1: 5

SEP 9,1980

#### ONR PA PAC-2 #9 FET CHARACTERIZATION

.00 VOLTS	, .00 MA (I	1EAS 1)		#3	V D = 5 V	ID=35MA
FREQ	S11	\$21		\$12	\$ 2	2
(MHZ)	MAG ANG	NAG	ANG J	MAG ANG	MAG	ANG
2000.000	.943 ~30	1.830	151	.025 77	.859	-6
2290.300	.933 -33	1.832	149	.027 76 ·	.857	-6
2400.000	.924 -37			.029 75	.854	-7
2600.000	.913 -41			.032 73	.853	-7
2800.000	.901 -44			.933 72	.845	~8
3000.000	.887 -49			.035 71	.840	~ 9
3200.000	.877 -53			.037 69	.841	- ġ
3400.000	.861 -57			.039 68	.833	-10
3600.000	.852 -61			.040 66	.829	-12
3800.000	.840 -65	1.818		.041 65	.829	-12
4000.000	.826 -69			.042 64	.825	-13
4200.000	.817 -72			.043 63	.823	-13
4400.000	3.805 -76			.044 62	.820	-14
4500.000	1.792 -80			.045 61	.817	-14
4899.999	.779 -84			.046 59	.813	-15
5000.000	.768 -88			.047 58	.812	-16
5200.000	.754 -92			.047 55	.805	-16
5400.000	.736 -96			.048 54	.805	-17
5600.000	.717 -101	1.689		.050 49	.791	-17
5800.000	.678 -107	1.632		.050 36	.773	-18
6000.000	.593 -107	1.505		.032 14	.753	-16
6239.300	.624 -106	1.520		.020 66	.782	-15
6409.900	.645 -109	1.549		.030 74	.787	-17
6600.000	.651 -114	1.563		.035 72	.791	-18
6800.000	.647 -119	1.557		.037 71	.789	-19
7000.000	.635 -122	1.535		.038 71	.734	-20
7200.000	.627 -127	1.521		.039 71	.784	-21
7400.000	.622 -130	1.509		.039 72	.780	-21
7600.000	.615 -134	1.495		.040 74	.782	-23
7800.000	.608 -138	1.489		.041 75	.781	-23
8a0 <b>0.</b> 000	.601 -141	1.467		.042 75	.775	-25
8200.000	.596 -146	1.443		.043 76	.779	-25
8400.000	.591 -150	1.431		.044 77	.771	-27
8639.000 •	.587 -154	1.423		.045 78	.766	-28
883 <b>0.0</b> 00	.584 -158	1.407		.046 78	.779	-30
9000.000	.583 -162	1.383		.047 78	.767	-31
9200.000	.581 -165	1.370		.049 78	.768	-33
9400.000	.579 -169	1.355		.050 78	768	-34
9600.000	.581 -173	1.340		.051 78	.769	-36
989 <b>0.</b> 000	.579 -176	1.316		.053 78	.771	-38
10000.00	.582 -180	1.295		.054 77	.775	-39
10200.00	.578 177	1.275		.055 76	.773	-40
19499.40	.577 174	1.264		.057 76	.772	-42
10 00.00	.579 171	1.243		.057 75	.772	-44
າດນວິດີາ	.576 168	1.226		.958 73	.769	-45
ំខ្លុំ	.577 165	1.210		.959 73	.774	-46
	.571 (62	1.194		.000 71	.770	-43
the state of the s	.539 :58	1.134	25	.981 79	1771	- 4
	.567 194	1.154	20	.932 69	.777	-50
	564 771	1.114		.955 37	1775	-4
	.509 147	1.1.0	iJ	.331 33	i ir i	-62
	554 144	1.112	15 A-51		.737	-53
	TOWNS CO		V-71	a will select		~ · ·

	E 47	140	1.095	13	.066	64	. 107	- 53
12400.00	.547		1.076	11	.066	62	.789	-53
12600.00	.539	136		. 8	.068	60	.794	-53
12800.00	.537	131	1.059		.069	59	.797	-53
13000.00	.535	126	1.051	6	.007	5 Ź	.798	-54
10200.00	.535	121	1.042	4	.070		.800	-54
13400.00	.536	117	1.035	1	.072	54		-55
13800.00	.540	112	1.027	- 1	.073	52	.802	-56
13800.00	.550	108	1.023	-4	.075	50	. 801	
	.556	104	1.017	-7	.076	47	.802	-57
14388.00	.561	้ออ	1.003	~10	.078	44	.798	-59
14:00.00		96	.997	-13	.ଡଃଡ	41	.799	-61
14400.00	.566	92	.978	-16	.031	38	.796	-62
14300.00	.571		.979	-19	.083	35	.791	-64
14300.00	.580	87	.972	-22	.085	31	.790	-66
15000.00	.586	83		-25	.086	28	.782	-67
15200.00	.583	78	.956		.087	25	.782	-68
15400.00	.583	73	.945	-29	.088	22	.780	-70
15600.00	.587	67	.928	-31		18	.775	-71
15300.00	.596	62	.919	-35	.089		.764	-72
16000.00	.607	57	.898	-38	.091	16	.763	-73
16200.00	.617	53	.887	-41	.091	13		-75
16400.00	1.632	48	.865	-44	.094	10	.761	-77
16600.00	÷.656	45	.859	-47	.095	6	.757	
16399.93	.675	42	.850	-50	.096	4	.753	-79
10000.00	.694	39	.830	-53	.098	1	.747	~80
17000.00	.716	36	.804	-56	.099	-2	.743	~83
17000.00		34	.797	-59	.100	-4	.724	85
17 00.00	.724	31	790	-62	.102	-7	.713	~87
17300.00	.742		.775	-65	.103	-9	.693	-91
17900.00	.749	29		-69	.106	-11	.693	-93
។១១៦៨ ១៨	.744	26	.764	-02				

REF FLAME EXT(CM): IN= 5.48, OUT= 5.48

PAGE 1: 5

## ONR PA PAC-2 #9 FET CHARACTERIZATION

SEP 9,1980

		r L i C	HERECIEKTER	110
.aa volts.	. AA MA	IMEAS	1.)	

#1 VD=5V ID=35MA

FREQ	211	\$21	\$12	•	523	2		
(MHZ)	MAG ANG	MAG ANG	MAG	ANG '	MAG	ANG		
2000.000	.939 -33		.028					
				74	.828	-8		
2200.000	.930 -36	1.849 147	.031	74	.825	-8		
2400.000	.922 -39	1.848 144	.033	72	.822	-9		
2600.000	.909 -43	1.846 141	.035	71	.820	-10		
2890.000	.898 -46	1.838 138	.037	70	.812	-11		
3000.000	.884 -50	1.842 135	.040	68	.807	-12		
3200.000	.872 -54	1.833 132	.041	67	.807	-12		
3400.990	.858 -58	1.822 129	.043	65	.799	-13		
3699.808	.850 -61	1.803 125	.044	64	.796	-15		
3800.000	.839 -65	1.794 123	.046					
4000.000				63	.797	-15		
	823 -69	1.768 120	.047	62	.793	-16		
4200.000	.814 -71	1.768 117	.048	61	.796	-17		
4400.000	.801 -74	1.739 115	.049	59	.793	-17		
4600.000	<b></b> 788 <b>-</b> 77	1.727 1.12	.050	59	.791	-18		
4890.000	.775 -80	1.715 109	.051	58	.790	-18		
5000.000	.760 -84	1.710 107	.052	57	.789	-18		
5200.000	.744 -87	1.700 104	.053	56	.784	-19		
5400.000	.724 -91	1.687 102	.055	54	.784	-19		
5600.000	.704 -96	1.691 98	.057	51	.772	-20		
5890.000	.677 -102	1.668 95	.058	45	.760	-20		
6000.000	.621 -107	1.605 91						
			.051	30	.734	-20		
6200.000	.594 -106	1.538 91	.029	48	.745	-17		
6400.000	.611 -109	1.567 90	.040	63	.757	-19		
6600.000	.618 -114	1.589 87	.044	62	.758	-20		
6830.0 <b>00</b>	.613 -119	1.589 84	.046	62	.755	-21		
7000.000	.601 -123	1.572 82	.047	62	.749	-52		
7200.000	.591 -128	1.564 79	.048	62	747	-22		
7400.000	.583 -132	1.555 76	.049	62	.742	-23		
7600.000	.572 -137	1.543 73	.050	62	.740	-24		
7800.000	.565 -142	1.539 71	.051	63	.736	-25		
8000.000	.558 -147	1.514 68	.852	62	.730	-27		
3200.000	.556 -153	1.495 65	.052	63	.733	-27		
8400.000	.556 -158	1.478 62	.053	64	.724	-29		
3600.000	.559 -163	1.464 59	.053	64	.717	-30		
3800.000	.564 -168	1.439 56						
			.054	64	.716	-32		
9030.000	.571 -172	1.407 53	.054	64	.711	-34		
9230.000	.578 -176	1.386 51	.055	65	.708	-35		
9400.000	.581 -179	1.364 49	.056	66	.707	-37		
9630.000	.589 178	1.346 46	.957	66	.706	-39		
9800.000	.589 175	1.323 44	.058	66	.708	-40		
10000.00	.593 173	1.298 41	.059	66	.711	-42		
10299.00	.590 170	1.280 39	.061	66	.708	-43		
18400.00	.589 167	1.269 36	.062	66	.706	-45		
16000.00	.591 163	1.250 34	.063	65	.795	-47		
(0.10.0)	.591 150	1.236 31	.០៩៩	61	.702	-49		
11 10.90	.595 :57	1.215 29	.ପଠର .ପ୍ରଶ	61	.703	-50		
	.597 179							
		1.200 26	.បាន់តិ	63	.700	-52		
	.601 150	1.183 24	.000 0:0	62	.703	-54		
1: 1.1	. မေΩ်းကို သည် မ	1.153 21	.069	54	.79	-56		
		1.193 19	.070	1.3	. 73	+50		
	.615 101	1.110 18	.071	59	.703	-59		
11.000.00	.618 198	1.051 14 A-	<b>.53 .</b> 072	53	.711	-60		

Salar Salar

	417	136	1.071	12	.073	58	.712	-01
12430.00	.617		1.051	10	.074	57	.714	-62
12600.00	.616	133		7	.075	56	.715	-62
12800.00	.616	130	1.033			55	.715	-63
13000.00	.615	127	1.023	6	.077		.714	-64
13200.00	.615	124	1.010	3	.078	53		
13400.00	.616	120	1.001	1	.080	52	.709	-65
13500.00	.619	117	.988	-2	.081	50	.707	-66
	.627	113	.978	-4	.083	43	.704	-68
13809.00		1 1 1	.968	-6	.085	46	702	-69
14000.00	.633		.950	-8	.036	44	.695	-71
14290.00	.640	108		-11	.088	43	.693	-73
14400.00	.647	105	.941		.089	41	.696	-75
14600.00	.654	103	.920	-13	.091	39	.693	-77
14300.00	.664	101	.919	-16		37 37	.691	-79
15000.00	.672	99	.911	-18	.092		.687	-80
15200.00	.668	96	.895	-20	.094	35	.688	-82
15400.00	.657	93	.883	-24	.097	33		-83
15600.00	.660	90	.875	-25	.098	31	.685	
15300.00	.659	87	.871	-28	.100	28	.683	-84
	.660	84	.859	-31	.104	27	.675	-86
16999.00	.662	80	.854	-34	.104	25	.677	-87
16200.00		77	.839	-36	.103	21	.672	-89
:6430.00	.665	74	.834	-39	.110	19	.669	-92
16300.00	`.682		.824	-42	.112	17	.663	-94
16393.99	: 694	71		-44	.115	14	.657	-97
17900.00	.706	69	.815	-47	.117	12	.654	-100
17/100.00	.720	67	.790			9	.639	-103
17<30.00	.728	65	.786	-49	.118		.631	-107
17430.80	.742	64	.776	-52	.121	8		-111
17:00.00	.757	63	.773	-55	.122	6	.624	-114
10010	748	61	.763	~58	.126	4	.629	-114

POF PLANE EXT(CM): IN= 5.48, OUT= 5.48

PAGE 1: 5

#### ONR PA PAC-2 #9 FET CHARACTERIZATION

SEP 9,1980

12430.33	.493	171	.927	22	.067	78	.811	-61
12600.00	.475	167	.918	19	.068	77	.815	-62
12800.00	.463	161	.905	16	.070	76	.321	-62
13000.33	.457	155	.902	14	.072	74	.825	-63
10200.00	.456	149	.890	11	.073	73	.832	-63
13499.83	.469	143	.802	9	.075	71	.834	-64
10000.00	.467	138	.873	6	.077	68	.833	-65
13300.00	.476	133	.863	3	.079	66	.839	-67
14000.00	.487	130	.856	1	.081	64	.843	-68
14200.00	.494	127	.841	-2	.032	61	.837	-70
14400.00	.498	123	.834	-5	.034	58	.840	-72
14600.00	.503	120	.816	-7	.084	55	.839	-73
14000.00	.505	116	.316	-10	.086	52	.837	-76
15000.00	.509	113	.804	-12	.087	49	.839	-77
15200.00	.504	109	.792	-15	.089	47	.832	-78
15490.00	.495	104	.784	-19	.090	44	.838	-80
15600.00	.496	99	.772	-21	.090	42	.836	-31
15300.00	.497	94	.766	-24	.092	39	.835	-81
16000.00	.502	90	.751	-26	.094	36	.833	-82
16200.00	.507	85	.748	-29	.095	34	.834	-82
16490.00	512	ଓଡ	.733	-31	.097	31	.837	-83
16000.00	7.528	7,6	.732	÷34	.099	28	.839	-84
16930.93	.542	7.1	.725	-37	.191	26	.839	-85
17:30:33	.557	6.7	.723	- 4 0	.104	23	.834	-86
17773	.575	63	.795	-42	.197	29	.333	-87
17130.00	.590	59	.706	-45	.199	17	.314	-90
17000.00	.611	56	.792	-49	.111	14	.797	-92
177	.626	51	.699	-52	.113	1 1	.779	-95
18773.47	.636	43	.683	-56	.117	9	.787	-97

REF PLANT ENTION): IN= 5.48, OUT= 5.48

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#### SEPT. 19, 1980

#### ONR PA PAC-2 #9 FET CHARACTERIZATION

.00	VOLTS,		MA	(MEAS	1)			<b>#</b> 5	$\forall D = 4 \forall$	I D =	30.	. ØM
FREG	Q	S 1	. 1		S 2		S 1	2		\$22		
(MHZ		MAG	ANG			ANG	MAG	ANG	MAG		ANG	
2000.		.949	-27			154	.033	75	.83		~ 6	
2200.		.940	-30			152	.037	75	.83		- 7	
2400.		.932	-33			149	.040	73	.82		- 7	
2680.		.919	-36		21	146	.043	72	.82		~ 8	
2800.		.909	-39 -43			143 140	.045	70 68	.81		- 9	
3000. 3200.		.895 .886	-43 -47		49	137	.048 .051	67	.80 .80		-11 -12	
3400.		.870	-50			134	.053	65	.79		-14	
3600.		.860	-54			131	.055	63	.79		-15	
3800		.846	-57			128	.057	62	.78		-16	
4000		.829	-61			124	.059	60	.78		-18	
4200		.819	-65			122	.060	59	.78		-18	
4400		805	-68			118	.061	57	.78		-13	
4600		:.791	-72			115	.063	56	.77		-26	
4800.	. 999	.775	-76	1.8	376	112	.065	55	.77		-21	Ĺ
5000.	. ១១១	.760	-80		358	110	.066	53	.76	8	-22	2
5200.		.747	-83			107	.067	50	.76		-23	š
5490.		.727	-88			103	.068	48	.76		-24	
5600.		.704	-93			100	.071	44	.74		-25	
5309.		.668	-98			96	.071	35	.72		-26	
6990.		.599	-100		347	94	.053	24	.70		-24	
6200		.613	-99		38	95 60	.043	48	.73		-23	
6400		.627 .630	-102		60	93 89	.051	52 52	.74		-25 -25	
6600 6800		.625	-112			87	.055 .056	52 52	.74 .73		-26	
7880		.617	-116		550	3.4 3.4	.057	51	.73		-27	
7200		.609	-121		529	81.	.058	50	.73		-27	
7499		.602	-125		513	79	.059	50	.72		-28	
7600		.595	-126		594	76	.059	50	. 72		-36	
7800		.589	-132			74	.059	50	.7		-31	
8000		.583	-136			72	.059	50	.7		-33	
8299		.579	-146			69	.058	50	.73		-33	
8400	.000	.575	-144		510	66	.058	51	.73		-34	4
8699		.572	-148		196	64	.058	51	.73		-36	
8899		.569	-152		179	62	.058	51	.7		-36	
9000		.567	-156		158	59	.058	52	.73		-36	
9200		.566	-159			57	.059	52	.73		-37	
9400		.563	-163			55 50	.868	52	.70		-37	
9600		.570	-167		407	52 53	.061	52	.65		-39	
_ 939 <b>0</b>		.571	-178		38 <b>6</b>	50 47	.062	52	.63		-41	
- 1999) - 1939)		.572 .563	-173 -176		349 349	47 45	.062 .063	51 50	.69 .69		-42	
1949		.ანა .ნგნ	-179		342	43	.053	50 50	.61		-45	-
1000		.5,0	1 77		321	43	.364	49	.6	70 30	-47	
1000		.570	175		110	ဒုတ်		49	.6:		-49	
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	J. J	.553	156	· 1	233	24	.071	1.1	. 6.		-5.	
11 0	$z \cdot 12$	.501	152	1.	222	21 <b>A-5</b> 7	,070	4.3	. 63	34	-55	5

12400.00	.549	148	1.207	19	.074	42	.678	-57
12600.00	.551	145	1.199	17	.074	42	.679	-58
12800.00	.543	141	1.182	14	.075	40	.683	-60
13000.00	.536	136	1.173	11	.076	38	.683	-61
13200.09	.533	131	1.166	9	.077	36	.691	-62
13400.09	.538	126	1.160	7	.078	35	.637	-62
13800.90	.549	121	1.146	3	.080	33	.687	-63
13300.00	.561	118	1.142	1	.081	31	.693	-64
14006.00	.570	114	1.136	-2	.084	29	.635	-65
14700.30	.571	110	1.122	-5	.086	27	.673	-67
14400.09	.578	107	1.112	-8	.089	25	.663	-69
14600.00	.579	103	1.093	<b>~11</b>	.090	23	.662	-71
14300.00	.588	99	1.038	-14	.093	19	.659	-74
15000.00	.598	96	1.071	-17	.095	17	.655	-75
15200.00	.599	91	1.058	-20	.097	13	.642	-78
15400.90	.601	87	1.050	~24	.098	10	.640	-81
15600.00	.595	82	1.031	-27	.099	8	.640	-83
15300.00	.596	76	1.008	-31	.102	5	.€38	-84
16000.00	.615	7.1	.994	~34	.103	2	.633	-85
16200.00	.635	67	.968	-33	.104	- 1	.614	-86
16400.00	1.652	63	.943	<b>-41</b>	.106	- 4	.601	~88
16699.99	₹.669	58	.919	-44	.103	-6	.5∋3	~90
16300.00	.681	56	.883	-45	.109	-9	.575	-91
17000.70	.697	53	.870	-49	.109	-12	.531	-94
17/00/.00	.791	51	.336	-52	. 1 1 1	-13	.529	-97
177300.00	.709	49	.822	-55	.111	= 1 7	.510	-191
17.90.30	.711	46	.301	-57	. 1 1 1	-19	.503	-105
17733.33	.726	46	.782	-59	.112	-29	.494	-107
10000.00	.730	÷ 4	.763	-62	.113	-22	.476	-110

REF PLANT ENT(CM): IN= 5.48, 09T= 5.48

.00 VOLTS, .00	MA (MEAS	1)	#5	VD=4V ID=10.0MA
FREQ S:	1 1	321	812	322
HHZ) MAG	ANG MA		MAG ANG	MAG ANG
2000.000 .953	-24 1.5		.043 75	.837 -7
2200.000 .945	-27 1.5		.047 74	.834 -8
2400.000 .938	-29 1.5		.051 73	.829 -8
2600.000 .925	-32 1.5		.055 71	.824 -9
200 <b>0.000 .916</b> 300 <b>0.000 .902</b>	-35 1.5 -39 1.5		.059 69 .063 68	.315 -11
3200.000 .896	-42 1.6		.063 68 .067 66	.807 -12 .807 -14
3400.000 .880	-45 1.6		.070 64	.797 -15
3600.000 .871	-49 1.6		.070 62	793 -17
ରଚ୍ଚ .857	-52 1.6		.076 61	.789 -18
4000.000 .843	-55 1.6		.079 59	.783 -20
4200.000 .834	-59 1.6		.081 57	.783 -21
4400.000 .818	-62 1.5		.083 55	.776 -22
4630.000 \.804 4990.000 \.788	-65 1.5 -69 1.5		.086 54	.772 -22
5000.000 .774	-73 1.5		.039 52 .091 50	.767 -23 .759 -25
5200.000 .762	-77 1.5		.093 48	.752 -26
5499.000 .742	_80 î.5		.095 45	.750 -27
5800.000 .719	-85 1.5		.099 42	.736 -28
<b>5</b> 83 <b>3.</b> 333 .681	-90 1.5		.100 35	.716 ~29
- 6439.949     .626	-90 1.4		.082 26	.695 -27
୍ରେମ୍ପ	-90 1.4		.072 40	.721 -27
6400.000 .649	-94 1.4		.080 43	.724 -28
- 6600.000 .643 - 6800.000 .636	-98 1.4 -103 1.4		.034 42 .036 42	.723 -29 .717 -30
7000.000 .625	-107 1.4		.087 41	.712 -31
7200.000 .615	-112 1		.089 39	.705 -32
7400.000 .609	-116 1.4		.090 38	.696 +32
7600.990 .603	-120 1.4		.090 37	.693 -34
7999.309 .597	-124 1.3		.090 36	.605 <b>-</b> 35
୍ଷ୍ଟ୍ରପ୍ରପ୍ତ କୃତ୍ୟ			.090 05	.679 -37
.584 .576 .576	-100 1.0		.089 35	.685 -38
0600.000 .571	-134 1.3 -138 1.3		.089 34 .088 33	.678 -39 .672 -40
8890.000 .563	~142 1.0		.088 33	.671 -41
9000.000 .559	-146 1.3		.008 32	.678 -41
9399.000 <b>.</b> 552	-150 1.0	90 56	.009 32	.663 -42
	-155 1.3		.090 31	.659 -42
9674.000 .557	-159 1.7		.ଶ୍ୟନ ଓଡ଼	.650 -44
			.090 29	.646 -46
	-165 1.3 -168 1.3	223 47 213 44	.091 28 .091 27	.647 -47
		113 44 108 42	.001 26	.643 -49 .639 -50
10300.53		(9) 40	.001 :3	.634 -52
្រុះមិន ខុស្មិនទ	-176 1.	101 37 TO	. 1 1	.031 -54
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16500.00
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777 06301 ZMT78H): IM= 5.48, 887= 5.48

.00 VOLTS	, .00 MA (M	EAS 1)	# 6	9 VD=4V ID=25.0M
FREQ	\$11	\$21	\$12	S22 Mag ang
(MHZ) 2000.000	MAG ANG .937 -32	MAG ANG 1.795 150	MAG ANG .033 72	
2293.889	.927 -35	1.782 147	.035 71	.838 -10
2400.000	.916 -39	1.775 144	.038 69 .040 67	
2679.000 2870.000	.902 -42 .890 -46	1.761 140 1.744 138	.040 67 .042 66	
3003.000	.878 -50	1.734 134	.044 55	.824 -13
3203.000	.867 -53	1.718 132 1.697 129	.046 64 .048 63	
3400.000 3600.000	.852 -57 .844 -60	1.686 126	.070 0:	
3800.000	.832 -63	1.684 124	.051 60	
4090.000	.817 -67 .807 -70	1.673 121 1.672 119	.053 59 .053 59	
4200.000 4430.000	.807 -70 .793 -73	1.658 116	.055 57	
4630.000	·.776 -77	1.654 113	.056 50	
4890.000	~.762 -81 .747 -85	1.659 110 1.646 108	.058 59 .059 54	
5000.000 5200.000	.747 -8 <b>5</b> .736 -89	1.637 104	.060 5:	2 .794 -17
5400.000	.718 -93	1.613 101	.061 50	
5609.000	.699 -97 .680 -102	1.605 98 1.578 95	.063 41 .065 41	
<b>5</b> 800.000 6000.000	.637 -105	1.525 91	.062 31	a .751 -21
6299.000	.607 -104	1.452 91	.042 3	
6490.000 6690.000	.612 -105 .615 -109	1.460 90 1.497 88	.040 4: .047 5:	<del>-</del>
68J0.000	.602 -113	1.503 85	.050 5	3 .772 -22
7000.000	.585 -118	1.498 82	.051 5 .052 5	
7200.000 7400.000	.570 -123 .555 -128	1.491 79 1.482 76	.052 5 .052 5	
7600.000	.544 -134	1.467 73	.052 5	2 .762 -26
7809.000	.539 -139	1.450 70	.052 5 .052 5	
8039.888 8290.888	.537 -144 .535 -149	1.422 63 1.392 64	.052 5	
8400.000	.535 -154	1.372 62	.052 5	3 .757 -31
8600.000	.538 -158	1.353 59 1.336 57	.052 5 .052 5	
8800.888 9800.888	.536 -162 .534 -166	1.336 57 1.310 54	.052 5	
9200.000	.532 -170	1.297 52	.052 5	5 .756 -34
9400.000	.530 -174	1.274 50 1.262 47	.052 3 .054 5	
9660.300 9830.300	.538 -178 .540 178	1.262 47 1.237 45	.055 5	
1010 <b>0.</b> 00	.543 176	1.215 42	.056 5	
10200.99	.540 173	1.197 39 1.183 37		5 .753 -42 5 .754 -44
10410.00 13-30.01	.546 17 <b>0</b> .954 168	1.183 37 1.134 35		4 .753 -46
10 00 00	,551 FAT	1,110 30	. 1:3	3 .754 -41
		1,130		1
	.g. 242 .g.: 242	1 · 1 · 1 · 2 / 2 / 3 · 3 · 3 · 3 · 3 · 3 · 3 · 3 · 3 · 3	1.13	
	.51.7	1 1133 115	1	1 -1 -1
	1968 122 1968 112	1 1.7 11 1.048 10	• •	.71) -1 0 - <b>.</b> 700 -52
	.490 107 .480 142	1.048 10 1.001 18 <b>A</b>		0 .785 -52
to the limit of the second				

12400.00	.491	138	1.011	15	.066	49	.786	-52
12500.00	.494	134	.999	13	.066	48	.786	-51
12800.90	.486	131	.983	11	.067	47	.790	-51
13000.00	.477	126	.981	9	.069	45	.793	-51
13200.00	.476	121	.983	7	.071	43	.791	-51
13400.00	.476	117	.935	5	.072	42	.791	-51
13600.00	.477	111	.984	2	.074	40	.794	-51
13300.00	.476	106	.989	- 1	.076	38	.795	-52
14000.00	.489	98	.937	- 5	.077	35	.782	-52
14200.00	.487	93	.962	-7	.079	34	.763	-53
14400.00	.501	89	.956	-10	.031	31	.747	-54
14600.00	.518	85	.934	-13	.083	29	.753	-56
14300.00	.526	81	.926	-16	.086	26	.753	-58
15000.00	.543	78	.907	-13	.088	24	.753	-59
15200.00	.552	76	.899	-21	.090	21	.742	-62
15430.00	.552	73	.889	-24	.091	18	.735	-64
15600.00	.540	69	.832	-26	.092	16	.742	-66
15800.00	.538	63	.872	-30	.094	13	.746	-66
16000.00	.549	59	.867	-32	.097	11	.748	-67
16700.00	.557	54	.853	-36	.098	3	.749	-67
16400.00	1.564	49	.339	-38	.101	7	.747	-68
16690.00	:.577	44	.829	-41	.104	5	.740	-69
16390.00	.596	4 1	.811	-43	.107	3	.727	-69
17000.00	.619	40	.811	-46	.111	0	.694	-71
17230.00	.626	38	.731	-40	.113	- 1	.690	-72
17-39.63	.637	37	.793	-50	.117	- 4	.681	-75
17300.00	.649	35	.709	~53	.119	-6	.671	-77
17030.00	.659	3 <b>3</b>	.788	~55	.122	-9	.659	-79
16900.60	.656	31	.789	-60	.126	-12	.647	-83

rss Plant EXT(CM): IH= 5.48, OUT= 5.48

	FET	CHARACTERIZAT	IUN	
			#7 VB=	:47 ID=25.0NA
.00 VOLTS,	.00 MA (MEA	13 1)	•	
.00 70613,		S21	\$12	S22 Mag Ang
FREQ	\$11	MAG ANG	MAG ANG	.860 -8 Mag and
(MHZ)	MAG ANG	1.641 153	.038 72	.858 -9
2609.808		1.642 150	.841 71	.853 -9
2200.000	.742	1 651 147	944 70 947 68	849 -10
2499.000	701	1.656 144		.340 -11
2699.000	.917 -39 .904 -42	1.654 140	.05 <b>0</b> 66 .053 65	.832 -12
2800.000	891 -46	1.658 137	.055 63	.834 -13
3000.000	.879 -50	1.654 134	.057 62	824 ~14 820 ~15
3383.889	.863 -53	1.633 131	_059 60	
3490.000 3600.000	.853 -55		.061 59	.818 -16 .813 -17
ეგცი.00° ეგცი.000	.୫୫୫ - <sup>69</sup>	1.625 125	.063 57	.815 -17
4000.000	822 -63	1.602 120	.064 57	809 -18
4200.000	.812 -66 .798 -68	1.583 117	.065 55 067 54	.806 -19
4499.999		1.578 114		.799 -20
46ଗ୍ରୁ.ଗ୍ରିଗ		1.581 111	.069 53 .070 52	.795 -21
4880.000	764 -75 747 -78	1.571 189	.072 50	790 -22
5000.000	702 -82	1.565 105	.073 43	.789 -23
5200.000	.710 -86	1.549 102	.076 45	773 -24 764 -25
5400.000 5600.000	.685 -90	1	.077 40	.764 -25 .742 -25
5800.000	.656 -95	1.519 95 1.457 91	.071 30	746 -23
6939.999	.601 -99	1.398 92	.053 35	.759 -24
6399.993	.576 -99 .581 -101	1.407 90	.054 46 060 48	.765 -25
គួនឡូញ ស្គ្រាថ	.581 -101 .583 -106	1.437 38	.060 48 .063 48	.759 -26
8600.00U	.575 -11 <u>1</u>	1.437 85	.063 47	.756 -28
6000.000	.567 -115	1.431 82	.064 46	752 -29 745 -30
7000.000 7200.000	559 -121		.064 46	1 1 -
7290.000 7490.000	.550 -125	1.405 76 1.381 73	.054 46	.745 -31 .740 -32
7690.000	540 -129	1.358 71	.064 46	737 -34
7800.000	.532 -133	1.327 69	.064 46 .063 47	748 -35
2000.000	.524 -136 517 -140	1.396 66		.741 -36
ឧទ្ធមា្សាសិមិ		1.294 64	.063 47 .063 47	.734 -37
8498.000	.512 -144 .509 -148	1.289 62	.033 17	.734 -38
8600.000	507 -153	1.283 59	.063 43	.734 -38
ឧទ្ធម.១៣៦	567 -157	1.266 56 1.256 53	. n 54 49	.733 -39 225 -40
9000.000 9200.000	509 -162	1	. 49	
9400.000	.509 -167	1.236 51 1.223 48	.965 49	.719 -43 .719 -45
9633.000	.521 -171	1.200 46	.066 43	.723 -47
, 9800.000	.044	1.179 44	.967 48 968 47	.221 -49
16330.87	. 32	1.162 41		.724 -50
_ ເຄາສອເປັນ		1.156 <sup>39</sup>	.009 47 .009 49	.723 -5%
រក្សាស្វាល	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1,140 36	1 1	
10110.4	1913	<u>. 1.1</u> 33	, , <u>, , , , , , , , , , , , , , , , , </u>	
• (* 1914 - 1) • (* )				No. of the control of
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5	*		, , ,	
<b>.</b>				
1	• •		A 63	•
l.			A-63	

	504	144	1.015	15	.080	40	.720	-64
12490.00	.506		1.002	13	.030	40	.722	-65
12600.00	.505	142	1.002	10	.082	38	.727	-67
12800.00	.493	139	.991		.084	37	.735	-67
13990.00	.478	134	.985	8		3 <b>5</b>	.736	-68
13200.00	.471	128	.982	5	.08 <b>5</b>	34	.729	-68
13400.00	.470	123	.977	3	.087		.723	-69
13600.00	.477	116	.964	- 1	.689	32		-71
13300.00	.491	111	.955	-3	.091	30	731	-72
13000.00	.513	105	.944	-7	.093	27	.718	
14000.00	.515	101	.915	-9	.094	26	.703	-75
14200.00		99	.901	-12	.096	24	.702	-77
14400.00	.528	97	.832	-14	.097	21	.701	-80
14600.00	.534	94	.873	-17	.099	19	.706	-81
14000.80	.541		.861	-19	.101	17	.709	-83
15600.00	.549	92		-21	.102	15	.701	-84
15380.00	.547	89	.850	-24	.104	13	.705	-85
15490.00	.542	85	.843		.105	ii	.711	-86
15600.00	.534	79	.831	-27		• •	.716	-85
15300.00	.538	73	.813	-30	.108	8	.715	-84
16000.00	.559	69	.801	-32	.111		.696	-85
16200.00	.579	65	.788	-35	.112	હ	.020	-87
15430.00	.600	62	.772	-37	.116	4	.686	-88
	2.619	60	.765	-39	.120	2	.682	
16400.00	.635	59	.756	-41	.123	Ø	.672	-89
16000.00	.649	57	.757	-43	.125	-2	.635	-92
17390.00		57	.740	-45	.130	-3	.633	-93
17700.00	.643		.753	-48	.132	- 5	.625	-97
17486.83	.644	55 50	.749	-51	.136	-7	.627	-99
17790.00	.644	52		-54	.1.11	-9	.621	-100
17300,00	.648	49	.749		.145	-12	.602	-102
4 (5 (5 (4 (5 ) ) (7 ) (7 )	649	46	.745	-58	* 1 4 7			

REF PLANT EXT(CM): IN= 5.48, OUT= 5.48

.00 VOLTS,	.00 MA (M	IEAS 1)	#8	VD=4V ID=25.0MA
FREQ (MHZ) 2000.000 2200.000 2400.000 2600.000	\$11 MAG ANG .940 -30 .931 -33 .923 -35 .911 -38	\$21 MAG ANG 1.603 150 1.585 147 1.577 145 1.565 142	\$12 MAG ANG .036 69 .038 68 .041 67 .043 65	S22 MAG ANG .846 -12 .842 -13 .839 -14 .835 -15
2000.000 3000.000 3200.000 3400.000 3600.000 3800.000	.903 -41 .890 -43 .883 -45 .868 -47 .860 -50 .844 -52 .828 -55	1.552 139 1.548 136 1.544 134 1.531 131 1.531 129 1.538 126 1.537 124	.045 64 .048 63 .050 62 .051 61 .053 60 .056 59	.819 -20 .816 -21 .814 -22
4200.000 4400.000 4600.000 4890.000	.818 -57 .800 -60	1.547 121 1.537 118 1.545 115 1.552 112 1.551 109 1.548 106 1.534 102	.058 57 .060 56 .062 55 .064 53 .066 52 .068 49	.808 -24 .803 -24 .800 -25 .793 -26 .787 -28 .785 -29
5430.000 5830.000 6030.000 6730.000 6433.000 6630.000	.687 -84 .666 -89 .622 -94 .581 -94 .597 -95 .600 -100 .595 -104	1.528 99 1.504 95 1.451 91 1.365 90 1.378 90 1.396 87 1.394 85	.071 44 .072 39 .070 28 .050 27 .046 41 .052 46	.741 -34 .740 -32 .756 -32 .765 -33 .761 -33
7000.000 7200.000 7400.000 7600.000 7000.000 8000.000 8200.000	.586 -109 .577 -113 .571 -117 .563 -122 .560 -126 .558 -129 .554 -133	1.382 82 1.373 79 1.365 76 1.356 74 1.351 72 1.331 69 1.315 66	.055 46 .057 46 .057 46 .057 46 .057 46 .057 46	.753 -34 .743 -34 .738 -36 .726 -37 .719 -40
8400.000 8600.000 8000.000 9000.000 9200.000 9400.000	.550 -137 .546 -140 .542 -144 .540 -147 .535 -150 .520 -154 .532 -158	1.299 63 1.293 61 1.282 58 1.270 55 1.258 52 1.246 50 1.231 47	.057 47 .058 46 .058 46 .058 46 .058 47 .059 47	.707 -46 .703 -43 .710 -50 .711 -51 .705 -53 .701 -55
9809.000 10000.00 10200.00 10400.00 10300.10	.531 -162 .533 -165 .527 -168 .531 -171 .533 -173 .537 -175	1.210 44 1.190 41 1.170 38 1.156 36 1.130 34 1.117 32 1.007 00	.061 46 .061 45 .062 44 .062 44 .062 45	701 -58 .701 -60 .694 -63 .692 -66 .691 -70 .697 -72
	.010 000 .010 000 .01	1.000 1.20 1.200 1.20 1.000 1.20 1.000 1.20 1.000 1.20		7777 -775 .7777 -777 .7777 -777 .7737 -777 .7737 -77

12400.00	.474.	160	1.024	13	.072	36	.706	-80
12600.00	.472	155	1.014	10	.073	34	.702	-82
12000.00	.465	150	.999	7	.074	32	.696	-84
13000.00	.460	144	.995	4	.075	29	.689	-86
13200.00	.463	138	.988	1	.075	27	.679	-88
13400.00	.474	133	.978	- 1	.076	25	.674	-90
13603.00	.485	128	.959	-4	.076	23	.684	-92
13300.00	.500	124	.953	-7	.076	22	698	-91
14000.00	.514	119	.941	-10	.079	20	.695	-91
14200.00	.516	116	.916	-13	.ଡଃଡ	18	.672	-92
14400.00	.529	114	.909	~15	.082	17	.662	-92
14600.00	.534	112	.892	-18	.085	14	.667	-94
14800.00	.542	109	.889	-20	.087	11	.646	-96
15000.00	.552	107	.800	-23	.033	7	.601	-99
15200.00	.553	105	.873	-25	.088	5	.548	-102
15400.00	.552	102	.876	-29	.୬ବ୍ଞ	3 3	.526	-106
15600.03	.541	98	.848	-31	.088	3	.520	-107
15800.00	.537	93	.866	-35	.092	2	.528	-107
16000.00	.545	88	.841	-37	.097	1	.539	-108
18200.00	.557	84	.845	-40	.100	-2	.559	-112
16490.00	.567	80	.828	- 44	.105	-5	.601	-115
16600.00	្ញ.581	75	.821	-47	.110	-8	.643	-116
16300.00	.596	72	.810	-50	.112	-12	.642	-116
17000.81	.611	68	.806	-53	.112	-15	.694	-117
17300.00	.614	66	.770	-56	.114	-16	.531	-117
17400.00	.625	64	.776	-59	.116	-18	.576	-119
17300.00	.636	60	.768	-62	.120	-19	.573	-120
17300,03	.650	58	.753	-64	.124	-22	.550	-120
18530,05	.661	56	.758	-68	.129	-24	.517	-124

REF PLANE EXT(CM): IN= 5.48, OUT= 5.48.

.00 VOLTS,	.00 MA (1	MEAS 1)	#9	VD=4V ID=35.0MA
FREQ	S 1 1	321	\$12	\$22
(MHZ)	MAG ANG	MAG ANG	MAG ANG	MAG ANG
2000.000	.937 -33	2.095 130	.031 74	· .836 -8
2200.000	.927 -36	2.094 147	.034 73	.834 -9
2400.000	.914 -40	2.095 144	.036 72	.830 -10
2600.000 2800.000	.897 -44 .885 -48	2.097 140 2.088 137	.039 70 .041 68	.827 -11 .819 -12
:300.000 :300.000	.871 ~53	2.035 134	.043 67	
3200.000	.858 -57	2.074 131	.045 65	.814 -14
348 <b>0.</b> 000	.841 -61	2.049 127	.047 64	.806 -15
349 <b>0.</b> 999	.830 -65	2.025 124	.049 62	.802 -16
3000.000	.818 -69	2.014 121	.050 61	.799 -17
4990.000 4200.000	.802 -73 .792 -77	1.987 118 1.944 115	.052 59 .052 58	
	.777 -80	1.912 112	.053 57	.792 -20
	.763 -84	1.894 109	.054 55	.789 -21
4890.900	7.746 -88	1.879 106	.055 54	.788 -22
	.732 -92	1.860 103	.056 53	.782 -22
53A9.999	.716 -96	1.834 100	.057 51	.779 -23
549 <b>0.</b> 000 560 <b>0.</b> 000	.699 -101 .678 -106	1.806 97 1.792 93	.057 49 .059 46	
5000.000	.656 -111	1.750 90	.050 40	.755 <del>-</del> 26
6000.000	.610 -117	1.677 36	.054 30	.735 -26
6200.000	.571 -115	1.581 86	.035 30	.732 -24
6400.800	.593 -118	1.614 85	.035 52	.753 -25
6500.000 6830.099	.596 -123 .594 -128	1.627 82 1.622 80	.041 57 .04 <b>5</b> 56	.761 -26 .758 -27
7000.000	.508 -133		.046 56	.756 -28
7290.000	.581 -138	1.577 74	.046 56	.754 -29
7400.000	.577 -143	1.557 71	.047 56	749 -30
760 <b>0.</b> 900	.575 -148	1.527 63	.047 56	.750 -31
7830.000 0000.000	.579 -152 .579 -156	1.509 66 1.469 63	.047 57 .047 58	.745 -31 .743 -33
8200.000	.584 -160	1.436 60	.047 58 .047 59	.753 -33
8499.089	.584 -164	1.410 58	.047 60	.747 -34
8600.000	.587 -16 <b>7</b>	1.396 56	.04 <b>8</b> 60	.741 -36
239 <b>0.</b> 090	.586 -170	1.377 54	.048 61	.739 -37
9000.300 9200.000	.586 -173 .583 -177	1.354 51 1.343 49	.049 61 .050 62	.737 -37 .738 -38
9400.000	.585 17 <b>9</b>	1.321 46	.951 63	
9600.000	.590 176	1.306 44	.052 63	.729 -41
28 <b>00.</b> 000	.592 173	1.283 41	.054 62	.729 ~43
10000.00	.594 170	1.298 39	.054 62	.735 -45
14200.00	.590 16 <b>7</b> .597 164	1.238 37 1.224 35	.056 62 .057 31	.733 -46 .734 -48
19400.98 2018.89	.597 164 .604 162	1.206 32	.053 00	.734 -40 .735 -50
<u> </u>	.600 161	1.191 30	.359 39	.733 -52
	.U// 159	1.1.17	, () (i)	.737 <b>-5</b> 0
	196	1 . NH 25	14	. 7 1 2 - 5 .
•	.733 16 <b>2</b> .97 739	1 - 1 - 1 - 1 - 2 - 1		.733 -553 .733 -557
	.5 (49) 575 (46)	1	A PAGE TO A STATE OF THE STATE	.7.) -57 .7.3 -50
		1.10		.733 -83
	.565 137	1.002 13 A	-67 (930 31	.709 -66

12400.00	.568	133	1.074	1 1	.069	51	.736	-61
12600.00	.571	131	1.067	. 8	.070	49	.737	-61
12800.00	.560	127	1.057	6	.071	47	.742	-63
13000.00	.548	122	1.046	3	.073	45	.747	-63
13200.00	.549	118	1.040	1	.075	43	.747	-64
13400.00	.553	113	1.034	-2	.076	4 1	.739	-64
13800.00	.554	108	1.029	-5	.078	38	.739	-66
13300.00	.554	103	1.016	-8	.079	35	. 746	-67
14000.00	.562	96	1.012	-12	.082	32	.735	-69
14200.00	.561	90	.971	-14	.032	30	.717	-70
14400.00	.578	87	.968	-13	.084	27	.715	-72
14680.00	.586	84	.941	-21	.085	24	.713	-74
14500.00	.599	80	.929	-23	.087	21	.716	-76
15888.00	.618	77	.908	-26	.089	18	.719	-77
15200.00	.629	75	.894	-28	.090	16	.797	-79
15400.00	.631	72	.881	-32	.091	13	.706	-81
15600.00	.613	67	.860	-34	.092	11	.714	-82
15800.00	.606	62	.848	-38	.094	8	.716	-82
16000.00	.626	58	.829	-40	.096	6	.714	-82
16200.00	-636	54	.819	-44	.097	2	.694	-83
16400.00	.639	51	.786	-46	.099	1	.684	-85
16600.00	∴.639	47	.768	-,49	.101	-2	.631	-86
16.06.00	.655	45	.748	-50	.103	-3	.674	-87
18600,30	.686	43	.754	-52	.196	-6	.644	-89
17335.00	.704	4.4	.717	-34	.108	-7	.619	-91
17430,88	.713	44	.729	-56	.111	-10	.615	-94
17.000.00	.718	43	.731	-59	.114	-11	.613	-97
17583.88	.733	42	.728	-61	.117	-13	.608	-99
13000.00	.735	40	.737	-63	.120	-16	.538	-102

PER PLANE EXT(CM): IN= 5.48, OUT= 5.48

APPENDIX B

3

## ONR FET CHARACTERIZATION

.90 VOLTS,	.00 MA (M	EAS 1)		LC CKT #10 X
.90 VOLTS, FREQ (MHZ) 2000.000 2300.000 2400.000 2600.000 2800.000 3200.000 3400.000	.00 MA (M S11 MAG ANG .774 -166 .801 -174 .820 178 .817 171 .810 164 .796 157 .776 152 .756 146 .734 142	S21  MAG ANG .366 -47 .268 -42 .194 -26 .174 1 .210 23 .272 34 .337 37 .398 38	S12 MAG ANG .366 -47 .269 -42 .194 -27 .173 1 .210 23 .272 34 .337 37 .398 38	\$22 MAG ANG .774 -166 .801 -174 .820 178 .818 171 .811 164 .796 157 .776 152
3399.999 4099.999 4299.999 4499.999 4699.999 5099.999 5299.999 5499.999 5499.999	.711 137 .690 134 .686 131 .675 128 .661 126 .645 124 .624 122 .602 121 .580 120 .561 118	.494 36 .537 35 .579 33 .613 32 .644 30 .671 28 .696 26 .716 24 .731 23 .748 21	.494 36 .537 35 .579 33 .613 32 .643 30 .670 28 .696 26 .716 24 .732 23 .748 21	.711 137 .690 134 .686 131 .675 128 .661 126 .645 124 .624 122 .602 121 .580 120 .561 118
6000.000 6200.000 6400.000 6600.000 7600.000 7400.000 7600.000 7600.000 8600.000	.521 116 .501 114 .482 111 .468 108 .458 106 .448 103 .442 101 .441 99 .438 99 .435 98 .438 99	.769 18 .778 17 .787 16 .795 15 .808 14 .813 13 .828 12 .838 11 .846 10 .852 8 .855 7	.769 18 .778 17 .786 16 .796 15 .807 14 .813 13 .827 12 .838 11 .845 10 .852 8 .856 7	.521 116 .501 114 .483 111 .468 108 .458 106 .448 103 .442 101 .441 99 .438 99 .435 98 .438 99
\$400.000 \$400.000 \$600.000 \$000.000 \$200.000 \$400.000 \$600.000 1000.00 10400.00	.453 99 .453 99 .455 98 .455 97 .426 97 .427 88 .421 83 .421 79 .421 79 .421 79 .421 79 .379 76	.853 .833 .833 .829 .822 .822 .821 .821 .821 .821 .821 .821	.050 .853 .833 .833 .829 .822 .822 .822 .822 .824 .842 .842 .842	.453 99 .453 99 .455 98 .455 97 .422 95 .423 88 .423 88 .422 79 .391 77 .379 75
19303.43 19313.60 11397.3 1913.60 1913.60 10203.00 10203.00	.084 78 .392 81 .407 85 .434 89 .410 92 .471 98 .461 93 .463 92	.895 -4 .096 -5 .000 -7 .000 -3 .067 +10 .0411 B .000 -8	.896 -4 .896 -5 .900 -7 .800 -9 .848 -10 -1 .811 -11 .807 -11 .797 -8	.334 78 .391 81 .437 85 .434 89 .430 32 .471 33 .462 93 .434 92

12400.00	.376	91	.792	-6	.784	-7	.371	91
12600.00	.345	81	.898	-4	.399	- 4	.344	81
12800.00	.248	82	.921	-7	.923	-7	.248	82
13000.00	.197	88	.931	-9	.931	-9	.197	88
13200.00	.185	90	.927	-12	.927	-12	.185	90
13400.00	.186	84	.924	-12	.924	-12	.186	84
13600.00	.197	75	.910	-14	.908	-14	.198	75
13800.00	.218	68	.922	-15	.923	-15.	.218	68
14000.00	.250	64	.906	-15	.906	-15	.249	64
14200.00	.277	65	.914	-17	.914	-17	.276	65
14400.00	.312	66	.891	-18	.891	-18	.312	67
14600.00	.377	71	.886	-19	.886	-19	.377	71
14800.00	.419	71	.845	-19	.844	-19	.418	71
15000.00	.418	70	.857	-18	.857	-18	.418	70
15200.00	.382	70	.868	-17	.868	-17	.382	70
15400.00	.321	68	.903	-17	.903	-17	.321	68
15600.00	.222	67	.941	-19	.941	-19	.222	67
15800.00	.138	79	.943	-22	.941	-22	.138	80
16999.99	.115	109	.951	-23	.950	-23	.115	109
16200.00	.148	122	.970	-25	.969	-25	.148	123
16400.00	.181	107	.945	-28	.945	-28	.181	107
16500.00	.212	91	.937	-31	.938	-31	.212	91
16800.90	.227	70	.900	-30	.901	-31	.227	70
17000.09	.273	60	.884	-32	.882	-32	.273	60
17200.39	.309	15.2	.065	-32	.866	-32	.309	52
17490.00	.344	47	.873	-33	.874	-33	.344	47
17600.00	.370	45	.847	-34	.848	-33	.371	45
17300.00	.394	44	.378	-34	.379	-34	.395	44
18988.18	.397	45	.851	-36	.845	-36	.392	45

REF PLANE EXT(CM): IN= 4.74, OUT= 4.74

### ONR FET CHARACTERIZATION

FREQ
11 00 0 13

12400.00	.173	70	.911	-17	.908	-17	.172	7.0
12600.00	.090	4.0	.970	-18	.970	-18	.090	40
12800.00	.013	-84	.957	-20	.957	-20	.013	-85
13999,00		-148	.956	-20	.956	-20	.056	-148
13280.00		-164	.957	-22	.956	-22	.062	-164
13400.00		-175	.958	-22	.958	-22	.042	-175
13690.00	.018	140	.948	-23	.949	-23	.018	140
13800.00	.035	72	.956	-24	.956	-24	.034	72
14000.00	.069	65	955	-25	.954	-25	.069	65
14200.00	.101	71	.950	-26	.950	-26	.101	71
14400.00	.147	76	.945	-27	.946	-27	.147	76
14600.00	.223	81	.943	-28	.943	-28	.223	81
14800.00	.267	79	.920	-29	.919	-29	.267	79
15000.00	.249	77	.916	-29	.915	-29	.249	77
15200.00	.198	ઇ2	.919	-29	.919	-29	.198	82
15400.00	.120	97	.925	-30	.924	-30	.120	97
19600.00	.102	146	.908	-30	.907	-30	.102	147
15800.00	.161	179	.929	-31	.930	-31	.161	179
16000.00	.217	178	.904	-30	.903	-30	.217	178
16200.00	.263	176	.976	-30	.975	-30	.263	176
15400.00	.246	162	.953	-33	.954	-33	.246	162
16600.00	.219	147	.981	-35	.981	-35	.219	147
16890.00	ં .153	130	.945	-36	.944	-36	.153	130
17000.00	.145	105	.937	-38	.937	-38	.145	105
17399.00	.144	81	.932	-40	.932	-40	.144	81
17460,00	.154	68	.911	-39	.912	-39	.154	68
17609.89	.173	60	.916	-49	.916	-39	.173	60
17300.00	.189	56	.908	-42	.907	-42	.180	56
10000.00	.188	57	.911	-42	.907	-42	.186	57

REF FLANE EXT(CM): IN= 4.74, OUT= 4.74

ONR-38 2.5 TURN #1

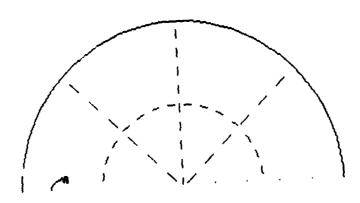
19:55:49 3 OCT 80

FREQUENCY	REFL COEFF	-IN	LOSS-FOR		LOSS-REV		REFL COEF	F -0UT
	S11		\$21		MAG	ANG	MAG	ANG
MHZ	MAG	ang	MAG	ANG	ring	11114	,	
• • • • • • • • • • • • • • • • • • • •					401	-12.5	.716 -	174.4
2000.0000	.7:6 -1	174.4	.491	-12.5	.491	-14.8	713	172.8
2100.0000		172.8	.461	-14.8	.461	-11.9	729 -	172.5
2200.0000		172.3	.481	-12.0	.481	-15.3	751 -	-171.8
2300.0000			.522	-15.3	.522		765 .	-174.7
2400.0000		174.8	. 475	-23.3	.474	-23.3	767	-173.5
2500.0000			.427	-22.3	.428	-22.2		-176.1
2600.0000		176.2	.437	-23.9	.437	-24.0		-174.3
2700.0000		174.3	.397	-31.6	.397	-31.5		
2800.0000		177.7	.338	-27.8	.338	-27.8		-177.6
		177.4	.326	-21.5	.326	-21.7		-177.5
2900.0000	,	179.4	.286	-25.2	.28€	-25.1	.825	179.4
3000.0000	, , , , , , ,	178.0	.219	-15.7	.219	-15.8		177.9
3100.0000		176.3	. 255	-1.0	. 255	-1.0		176.3
3200.000		174.3	.280	-3.9	.280	-4.0		174.4
3300.000	,	.73.7	,250	5.0	.250	5.0		173.6
3400.000		171.1	,285	14.6	. 285	14.5		171.1
3500.000	a .779	172.2	.334	9.5	.334	9.4		172.1
3600.000	0 .756	170.1	.301	6.5	.301	6.5	.758	170.1
3700.000			.315	14.9	.315	15.6		170.9
3 <b>800.000</b>		170.9	.400	10.7	.400	10.6	. 774	169.3
3900.000		169.3	.348	6.1	.349	6.1	. 757	169.1
4000.000		169.2	,323	12.7	.323	12.7	7 .730	168.6
4100.000	0 .730	168.5		10.8	.394	10.	7 .710	168.2
4200.000		168.2		4.3	.379	4.		167.9
4300.000		168.0		12.5	•	12.		169.5
4400.000	.752	169.5				14.		172.7
4500.000	.768	172.8		14.3	· <del>-</del>			171.7
4600.000		171.7		1.4				
4700.000		169.7						
4800.000		170.8	4		-		·	
4900.000		172.0				_		
5000.00		175.3	. 390	7.3	. 390			<u> </u>

FREQUENCY	REFL COEFF -1	361		OSS-REVE S12 Mag	RSE RE	FL COEFF \$22 MAG	-OUT ANG
MHZ	MAG AND	MAG	HITG	****			
11114		7 .469	-9.6	. 489	-9.8	.716 -1	74.8
2000.0000	.7:5 -174		-13.3		-13.4	.722 -1	.72.0
2100.0000	7:7 -171		-11.1	. 466	-11.3	.723 -	175.5
2200.0000	7:8 -175	.4 .466	-13.3	. 492	-13.5		170.9
2300.0000	.731 -171	.1 .492	-20.0		-20.1	.746 -	175.0
2400.0000	.746 -175	.1 .453	-19.3	.428	-19.4	.753 -	171.5
2500.0000	.753 -171	.6 .420	-17.3 -21.7	.440	-21.8	.763 -	175.4
2600.0000	.763 -175	,4 ,440		. 401	-29.8	.785 -	172.1
2700.0000	.784 -172	.0 .403	-29.7	.337	-27.0	.807 -	176.7
2800.0000		.8 .337	-26.9	.319	-21.1	.821 -	176.1
2800.0000		. 8 . 317	-21.0	.280	-24.4	.825 -	178.8
2900.0000		3.8 .280	-24.3	.216	-15.1	.826	179.4
3000.0000		3.5 ,216	-15.1	.251	. 1	.817	177.9
3100.0000	,	250,			-2.7	.886	176.2
3200.000		6.2 .275	-2.4	.275	6.7	.797	175.3
3300.000		5.4 .248		.247	16.9	.786	174.8
3400.000	4 3	4.8 .286		. 286	11.9	.772	174.2
3500.000		4.3 .341		.342	9.1	.764	174.5
3600.000		4.4 .302	9.1	,302	17.0	.759	172.8
3700.000		2.9 .309	17.2	.309		.750	175.0
3800 <b>.000</b>	• • • • • • • • • • • • • • • • • • • •	4.9 .385		.385	13.7	.746	172.3
3900.0 <b>00</b>		2.4 .356		. 351	9.4	.741	175.4
4000.000		5.4 .33		. 335	16.6	.736	172.3
4100.000		2.3 .41		.418	13.8	.730	174.7
4200.000	736			.386	7.8		172.4
4300.000	10 .730		٠	. 351	14.6	.731 .725	174.9
4400.000	30 .731 1		•	.413	15.6		173.1
4500.000	aa .724 L			. 404	3.9	.723	174.2
4600.000	ag ,723 1	,	`			.722	173.9
4700.00	99 ,7:8 1				15.6	.725	
4800.00	aa .721 1		' ·		4.8	.719	
4900.00	00 .7:9 1			·		.718	174.9
5000.00	99 .7:7 1	74.9 .37	2				
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B-6

0NR-38 2.5 TURNS +1

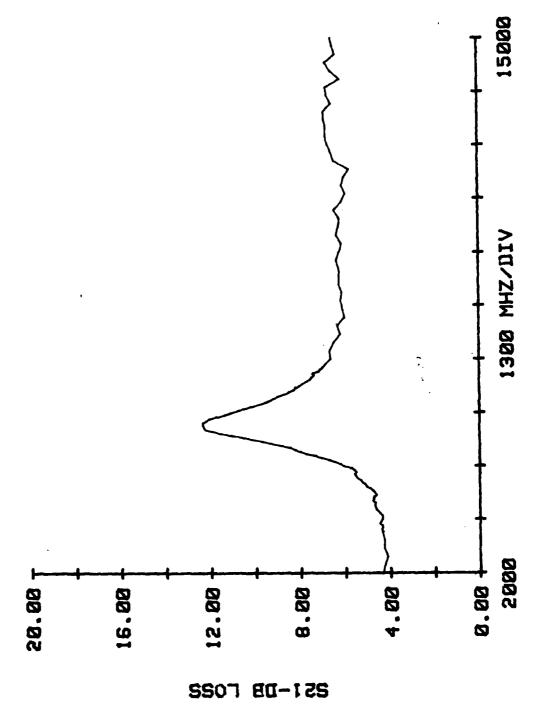


S11 S21 S12 S22  MHz MAG ANG MAG ANG MAG ANG MAG ANG  2000.0000 .575 -147.5 1.013 -37.6 1.011 -37.7 .575 -147.6  2100.0000 .600 -152.1 .936 -42.2 .936 -42.3 .600 -152.1
2100,0000 .600 -152.1 .936 -42.2 .936 -42.3 .600 -152.1
2100,0000 .600 -152.1 .936 -42.2 .936 -42.3 .600 -152.1
2200,0000 .634 -154.3 .851 -38.8 .850 -38.9 .638 -154.4
2300,0000 .680 -159.4 .827 -38.4 .827 -38.5 .683 -159.3
2400,0000 .709 -165.9 .705 -45.0 .703 -45.0 .712 -165.8
2500.0000 .7:3 -170.3 .550 -39.8 .550 -40.2 .717 -170.3
2600,0000 .707 -177.7 .505 -31.8 .504 -31.9 .711 -177.9
2700.0000 .708 179.8 .442 -27.9 .442 -28.1 .712 179.8
2800.0000 .7:9 172.6 .384 -10.9 .384 -11.0 .723 172.6
2900,0000 .734 169.2 .428 7.0 .427 6.9 .734 169.1
3000,0000 .735 163.6 .470 9.8 .470 9.7 .735 163.6
3100,0000 .725 159.4 .450 19.0 .450 18.9 .725 159.4
3200.0000 .717 155.3 .594 27.9 .594 27.8 .717 155.4
3300.0000 .707 150.6 .680 21.0 .680 20.9 .712 150.6
3400.0000 .699 147.0 .655 26.9 .655 26.8 .699 147.1
3500.0000 .673 143.3 .769 33.2 .768 33.1 .674 143.4
3600.0000 .643 139.8 .879 27.0 .879 26.9 .644 139.8
3700.0000 .645 138.4 .814 25.1 .814 24.9 .646 138.5
3800.0000 .658 133.8 .882 30.8 .882 30.6 .658 133.9
·
3900.0000 .666 132.6 1.000 24.0 1.000 23.8 .666 132.6
3900.0000 .666 132.6 1.000 24.0 1.000 23.8 .666 132.6 4000.0000 .639 125.9 .956 22.3 .956 22.4 .641 125.9
4100.0000 .6:4 127.0 .937 28.1 .937 28.0 .615 126.9
4200.0000 .584 123.8 1.016 24.2 1.016 24.2 .586 123.8
4300.0000 .569 125.6 1.016 19.3 1.016 19.3 .569 125.6
4400,0000 .599 124.3 1.024 24.9 1.024 24.8 .599 124.3
4500.0000 .593 128.7 1.042 21.2 1.042 21.1 .593 128.5
4600.0000 .605 125.8 1.026 13.8 1.026 13.7 .608 125.8
4700,0000 .559 123.0 1.013 19.0 1.013 19.0 .561 123.0
4800.0000 .525 124.7 1.010 21.0 1.010 21.0 .525 124.7
4900.0000 .5:9 126.0 1.013 13.1 1.013 13.1 .519 125.9
5000.0000 .541 127.2 1.040 16.7 1.040 16.7 .541 127.2

FREQUENCY	REFL COEFF -IN	LOSS-FOR	_	LOSS-REV		REFL COE	
MHz	S11 Mag ang	MAG	ANG	WAC	ANG	S2: MAG	ANG
2000.0000	.397 -166.9	.606	-9.6	. 606	-9.6	. 397	-166.9
2200.0000	.392 -165.0	.613	-9.3	.611	-9.3		-165.2
2400.0000	.395 -166.9	.622	-10.8	.620	-10.7		-166.7
2600.0000	.387 -168.4	.611	-12.8	.611	-12.9		-168.5
2800.0000	.387 -168.5	.612	-13.2	.612	-13.3		-168.3
3000.0000	.397 -168.0	.606	-15.0	.606	-15.0		-168.1
3000.0000	.398 -167.9	.607	-15.0	.607	-15.0	. 400	-168.1
3050.0000	.400 -167.7	.603	-15.4	.603	-15.3	.402	-167.9
3100.0000	.403 -166.6	.606	-16.2	.606	-16.3	.403	-166.9
3150.0000	.406 -166.5	.606	-17.4	.606	-17.4	.406	-166.7
3200.0000	.4:0 -166.8	.598	-17.8	.598	-17.9	.411	-166.9
3200.0000	.4:0 -166.9	.598	-17.8	. 598	-17.7		-166.9
3250.0000	.4:4 -167.2	.601	-18.2	.601	-18.2		-167.2
3300.0000	.4:8 -166.8	.605	-18.4	. 605	-18.4		-166.9
3350.0000	.421 -166.6	.606	-18.7	. 604	-18.7		-166.9
3400.0000	.426 -166.5	.605	-19.4	. 605	-19.3		-166.7
3400.0000	.426 -166.5	.605	-19.4	.605	-19.3		-166.8
3450.0000	.426 -167.2	.598	-19.3	.598	-19.9		-167.4
3500.0000	.429 -168.1	.593	-20.2	.591	-20.1		-168.3
3550.0000	.431 -167.8	.587	-20.5	.586	-20.5		-168.0
3600.0000 3600.0000	.434 -166.7 .434 -166.7	.584 .584	-20.7 -20.7	.584	-20.7		-166.9
3650.0000	.437 -167.1	.583	-21.2	.584 .583	-20.7 -21.1		-166.9 -167.1
3700.0000	.443 -168.0	.586	-21.9	.584	-21.8		-167.1 -168.1
3750.0000	.447 -167.9	.578	-22.1	.578	-22.1		-168.1 -168.1
3800.0000	.455 -166.7	.581	-22.2	.581	-22.1		-167.0
3800.0000	.456 -166.7	.581	-22.2	.581	-22.1		-167.1
3850.0000	.460 -167.0	.579	-22.0	.579	-22.1		-167.3
3900.0000	.468 -169.0	.588	-22.5	.586	-22.6		-169.2
3950.0000	.472 -169.3	.584	-23.2	.584	-23.1		-169.5
4000.0000	477 -168.2	.578	-24.6	.577	-24.5		-168.5
4000.0000	.477 -163.4	.579	-24.6	.578	-24.6		-168.6
4050.0000	.482 -167.5	.571	-24.9	.570	-24.8		-167.7
4100.0000	.482 -169.3	.560	-26.3	.560	-26.2		-169.4
4150.0000	.490 -170.9	.555	-27.1	. 555	-27.0		-171.0
4200.0000	.495 -169.7	.548	-27.9	.548	-27.9		-169.8
4200.0000	.494 -169.8	.548	-27.8	.548	-27.8	. 494	-169.9
4250.0000	.507 -169.8	. 544	-29.1	. 544	-29.1	.507	-170.1
4300.0000	.5:8 -170.5	.534	-30.2	.534	-30.2	.518	-170.6
4350.0000	.532 -170.9	.531	-30.4	.530	-30.4	.532	-171.1
4400.0000	.547 -169.5	.526	-30.8	.526	-30.8		-169.6
4400.0000	.548 -169.6	.527	-30.9	.526	-30.9		-169.8
4450.0000	.565 -167.4	.530	-31.0	.530	-31.0		-167.6
4500.0000	.574 -166.4	.526	-32.5	.523	-32.5		-166.4
4550.0000	.593 -168.1	.519	-34.1	.519	-34.0		-168.2
4600.0000	.599 -168.2	.499	-35.5	.499	-35.5		-168.3
4600.0000	.599 -168.3	.499	-35.5	.499	-35.5		-168.3
4650.0000		.490	-36.7	.490	-36.7		-169.2
4700.0000	.6:9 -170.6	.475	-38.2	. 475	-38.1		-170.7
4750.0000	.625 -171.6	.463	-39.9	463	-39.9		-171.8
4800.0000	.635 -172.1	.445	-40.7	.445	-40.6		-172.3
4300.0000	.635 -172.1	.445	-40.7 -41.6	.445	-40.7		-172.2 -171.7
4850.0000 4900.0000	.647 -171.6 .657 -170.5	.431	-41.8	.430 .411	-41.6 -41.7		-171.7 -170.7
4950.0000	.678 -169.2	.411 .399	-40.3	.399	-40.2		-170.7 -169.4
5000.0000		.399		.397 B_8.387	-39.9		-169.4 -169.8
5000.0000	.693 -169.6	.389	-39.9	.388	-39.9		-169.8 -169.7
2660.6688	1073 -107.0	. 307	- J / . J	. 300	37.7	. 673	1031

5050.0000	.707 ~170.5	.379	-39.7	•	-39.6	.707 -	
5100.0000	.726 -171.5	.362	-39.7	.362	-39.7	.726 -	171.7
	.733 -171.8		-39.8		-39.7	.733 -	172.1
5150.0000	•					.739 -	
5200.0000	.739 -172.8	•	-38.2		-38.2		
5200.0000	.739 -172.8	.328	-38.1	.328	-38.2	.739 -	
5250.0000	.735 -175.5	.312	-38.2	.312	~38.3	.738 -	175.7
	.734 -178.3		-37.7	.299	-37.7	.734 -	
<b>5</b> 30 <b>0.</b> 0000	-						
5350.0000	.730 -178.2		-36.0	.280	-36.0	.730 -	
5400.0000	.723 -178.7	.265	-34.1	. 265	-34.1	.723 -	178.9
5400.0000	.724 -178.7		-34.3	.265	-34.2	.723 -	178.9
			-30.5	.253	-30.6	.720	178.1
5450.0000	.720 178.2						
5500.0000	.7:4 175.0	.244	-26.2	.244	-26.1	.713	174.9
5550.0000	.7:3 175.1	.243	-21.9	.242	-21.8	.711	174.9
5600.0000	.7:6 176.0		-17.0	.242	-16.8	.716	175.8
		•	-16.9	.242	-16.8	.716	175.7
5600.0000	.7:6 175.9		-				
5650.0000	.708 174.4		-13.8	.241	-13.8	.708	174.2
5700.0000	.7:1 172.2	.245	~9.4	. 246	~9.3	.709	172.0
5750.0000	.703 171.2	.249	-6.1	.249	~6.0	.699	171.0
				.259	-3.1	.698	172.0
5800.0000	.691 172.3	.259	-3.2				
5800.0000	.691 172.3	. 259	-3.2	. 259	-3.2	.690	172.0
5850.0000	.686 170.3	.271	-1.9	.271	-1.7	. 683	170.1
	.671 167.0	.278	-1.0	.280	-1.1	.667	166.8
5900.0000				.289	.5	.659	165.5
5950.0000	.659 165.8	.289	.5				
6000.0000	.651 166.4	.298	2.5	.298	2.5	.650	166.1
6000.0000	.653 166.3	.298	2.3	.298	2.5	.651	166.1
		.310	3.2	.310	3.2	.638	164.8
6050.0000			-			.630	163.7
6100.0000	.633 164.0	.323	4.2	.323	4.1		
6150.0000	.624 163.8	.333	5.2	.333	5.0	.624	163.4
6200.0000	.6:7 164.7	.342	4.9	.342	4.9	.614	164.4
		.342	5.0	.342	5.1	.614	164.3
6200.0000	.6:7 164.6						163.8
6250.0000	.609 164.1	.349	5.1	.349	5.0	.607	
6300.0000	.601 163.5	.356	4.9	.357	4.9	.598	163.3
6350.0000	.595 164.0	.368	4.8	.368	4.8	.592	163.7
		.376	4.7	.376	4.6	.583	163.3
6400.0000	.583 163.6						
6400.0000	.583 163.5	.376	4.5	.376	4.5	.583	163.2
6450.0000	.575 162.7	.386	3.6	.386	3.6	. 575	162.4
6500.0000	.568 162.9	.389	3.7	.389	3.7	.566	162.5
			3.5	.397	3.4	.561	163.4
6550.0000	.562 163.8	. 397					
6600.0000	.554 164.1	.403	3.8	.403	3.7	. 554	163.8
6600.0000	.553 164.1	.403	3.8	.403	3.8	.553	163.8
6650.0000	.545 162.0	.411	3.3	.411	3.2	.544	161.7
				.418	2.8	.537	162.6
6700.0000	.537 162.8	.418	2.8				
6750.0000	.530 165.3 ·	.423	2.3	.423	2.2	.530	165.0
6800.0000	.525 164.7	.428	2.3	.428	2.3	.525	164.5
6800.0000	.525 164.8	.428	2.4	.428	2.3	.525	164.5
					1.4	.516	162.1
6850.0000	.5:6 162.4	. 425	1.4	. 425			
6900.0000	.5:6 162.9	.438	2.0	.438	2.1	.510	163.1
6950.0000	.5:0 164.2	.442	1.3	. 442	1.3	. 504	164.6
	.507 163.8	.447	. 4	.447	. 4	.502	164.1
7000.0000				.447	.3	.503	164.2
7000.0000	.507 163.8	.447	.3				
7200.0000	.496 167.2	.467	.5	.467	. 4	. 490	167.4
7400.0000	.479 167.0	.465	9	. 465	-1.8	. 476	166.9
	.476 168.0	.475	-3.3	.475	-3.4	.474	167.7
7600.0000					-5.3	.471	168.7
7800.0000	.471 168.9	. 491	-5.2	. 491			
8000.0000	.443 170.6	.484	-6.1	.484	-6.1	. 445	170.5
8200.0000	.446 169.7	.502	-9.2	. 502	-9.3	.451	169.9
		.498	-11.4	.498	-11.6	.430	168.8
8400.0000						.410	169.2
3600.0000	.405 168.1	. 493	-11.1	.493	-11.2		
9800.0000	.398 166.3	. 495	-11.7	. 495	-11.7	.403	168.0
9000.0000	.398 167.3	.489	-12.2	.489	-12.2	.401	169.3
			-13.7	.491	-13.7	.396	169.9
9200.0000	.397 167.3	.489					170.8
9400.0000	.480 168.1	. 488	-14.0	. 489	-14.0	.396	
9600.0000	.401 168.8	.482	-14.4	.483	-14.5	. 394	171.4
9830.0000	.406 169.3	.490	-15.7	.491	-15.8	.397	171.5
					-16.0	.397	172.6
10000.0000	.408 170.9	. 495		-4			172.2
10200.0000	.4:2 171.3	.483	-15.7	.483	-15.8	. 401	116.6

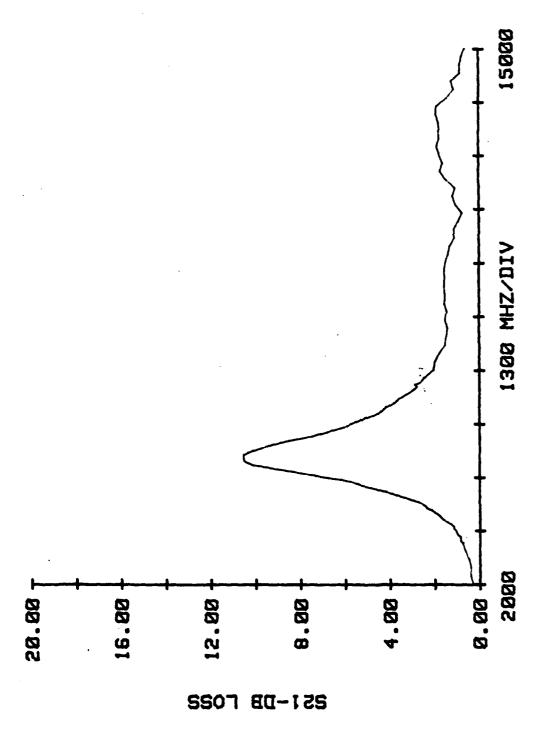
10400.0000 . 425 .488 .488 176.0 ~15.2 -15.2.415 176.5 19600.0000 .426 178.1 .490 -16.5 . 492 -16.6 .418 178.0 10800.0000 .409 -174.5 .477 -16.6 .477 -16.6 .405 -174.9 .420 -170.0 11900.0000 . 496 -16.2. 497 -16.2.420 -170.8 11200.0000 .4:0 -167.3 .506 -20.4 .506 -20.5 .411 -168.1 11400.0000 .373 -168.6 .497 -22.9 .497 -22.0 .380 -169.0 11600.0000 .357 -166.0 .504 -21.0.504 -21.1 .368 -165.7 11800.0000 .364 - 172.4.516 -23.4 .379 -170.9 .518 -23.3 12000.0000 .386 -175.6 .477 -24.9.478 -24.8 .399 -173.0 12200.0000 .423 - 175.5.472 -23.9.472 -23.9 .426 -174.5 12400.0000 .427 -174.6 .464 .462 -24.4-24.4 .430 -174.8 . 458 12600.0000 .420 -173.6 -25.5.459 -25.5 .422 -173.6 12800.0000 .422 -173.2 . 459 -26.2 .459 -26.2 .424 -173.2 .426 -173.7 . 455 13000.0000 -27.0 . 455 -27.1 .427 -173.7 13200.0000 .440 -174.8 . 454 -26.2 . 454 -26.3 .443 -174.8 .447 -176.8 13409.0000 .472 -26.1 .472 -26.2 .449 -176.9 13600.0000 .455 -176.1 -26.5 .461 . 462 -26.6 .455 -176.2 13300.0000 .461 -171.6 .459 -25.0 .459 -25.0 .463 -171.7 .494 14000.0000 .491 -170.0 -27.5 . 494 -27.7 .494 -170.2 -31.3 14200.0000 .460 -169.3 .471 -31.2 .471 .461 -169.6 14400.0000 .431 -165.8 . 459 -30.2 -30.3 .432 -165.9 .460 14600.0060 .433 -164.2 .483 -31.1 .483 -31.2 .433 -164.3 .476 14800.0000 .4:4 -164.6 -33.2 .476 -33.4 .414 -164.5 15000.0000 .4:4 -163.5 .472 -32.6 .472 -32.6 .412 -163.6



Α.					
<b>\</b>	and cores ath t	_OSS-FORWAR	RD LOSS-RE		L COEFF -OUT
FREQUENCY	KELF COTL	\$21	\$1		\$22
	\$11		NG MAG	ANG	MAG ANG
MHz	MAG ANG	11114			
		.968 -1	3.7 .962	-13.6	.172 -112.9
2000.0000	.171 -112.5		4.3 .953	-14.3	.186 -111.0
2200.0000	.185 -110.7		5.5 .954	-15.5	.197 -114.6
2400.0000	.197 -114.4	_	7.8 .948	-17.8	.202 -118.6
2600.0000	.202 -118.2	• • · ·		-19.4	.209 -121.7
2800.0000	.208 -121.8			-21.9	.232 ~123.8
3000.0000		* '		-21.9	.232 -123.9
	ANA -172 2		1.9 .912	_	.240 -124.3
3000.0000		.907 -2	2.6 .904		.248 -122.4
3053.0000		.907 -2	23.4 .903	-23.4	.257 -123.5
3100.0000			24.3 .901	-24.3	.267 -126.0
3150.0000	A . C . 100 0		25.3 .895	-25.4	.267 -125.0
3200.0000			25.3 .895		.267 -126.1
3200.0000	.266 -126.3		26.0 .890	-26.0	.275 -126.7
3250.0000	, 274 -126./		26.4 .884		.287 -125.6
3380.0006	. 287 ~125.6		26.8 .877		.295 -127.8
3350.0000	295 ~126.7				.307 -129.8
3400.000					.307 -129.7
3400,000			27.3 .87	-	.316 -131.3
	0.6 (01.2		28.2 .866	-	.328 -131.1
3450.000			29.0 .850		.338 -131.2
3500.000		.835 -	29.9 .83		.348 -133.7
3550.000			39.3 .82		.348 -133.1
3600.000			30.2 .82	2 -30.3	.348 -133.7
3699.909	0 .348 -133.8		.30.8 .81	1 -30.8	359 -135.8
3650.000	18 .359 ~135.9		31.5 .80		.372 -136.1
3700.000	19 .372 -136.0			-	.383 ~137.1
3750.000	183 -136.9	•			.396 -139.2
3800.000					.397 -139.2
3890.000		•			.412 -141.2
3850.00			-32.6 .76		.423 -143.6
3879.000		• • •	-32.9 .75		.438 -144.2
3904.00			-33.7 .74		447 -145.7
3950.000		.731	-35.3 .72		447 -145.8
4000.00			-35.4 .72		464 -148.1
4600.00			-36.1 .76		471 -151.1
4050.00		•	-37.9 .68		.4/1 -151.1
4100.00			-38.5 .6	58 -38.6	.488 -154.5
4150.00	00 .488 -154.5	·	-39.5 .6	37 -39.5	.497 -155.3
4200.00	197 ~155.4		-39.4 .6	37 -39.5	.496 -155.3
4200.00	A96 -155.3	.637	<b>~~~</b>	18 -40.5	.514 -157.8
4250.00	199 .5:4 -15(+4	.618	,	93 -41.5	.534 -159.8
4300.00	.534 -159.	7 .593		68 -41.3	.551 -161.9
4350.00		3 .5/1		47 -41.0	.572 -162.2
4370.00	4 7 4	9 .548		_	.571 -162.2
4499.99		g .548		· · · ·	.593 -162.1
4400.00		g .533		33 -40.2	.606 -162.8
4450.00		_		511 -40.7	.627 -166.5
4500.0				198 -41.2	
4550.0			-41.3	455 -41.3	
4600.0	000 .634 -168.		-41.2	455 -41.3	
4600.0	ú00 .634 −168.	· ·		432 -40.5	.644 -171.3
4650.0	aaa .644 -1/1.	1 .432		402 -39.8	.651 -174.6
4700.0	aaa .651 ~1/4.	5 .402	• • •	379 -38.9	.654 -177.4
4750.0	aga .655 -177.	3 .380	•••	355 -36.7	.656 -179.1
4890.0	1000 .659 -179	1 .355		355 -36.7	
4500.0		.355			5 6 4 4 7 0 A
4800.0		, 5 , 333	•		
4859.6	,000			313 -30.3	130 7
4900.6	400 470		-24.5	304 -24.5	
4950.6	, , , , ,		-19.7B-12.	297 -19.	177 6
5000.0	409 477			298 -19.	6 ,694 177.6
5000.0					

5050.0000	.706 175.1	.298	-14.9	.298	-14.9	.705	175.0
5100.0000	.7:4 172.0		-10.5		-10.4	.713	172.0
5150.0000	.7:3 170.3	.298	-6.2	. 298	-6.3		170.1
	.7:0 169.2	.304	-1.0	.304	-1.1	.706	169.1
5200.0000		.304	9	.304	-1.0	.706	169.1
5200.0000	.7:0 169.2		1.9	.312	1.8	.695	165.7
5250.0000	.695 165.8	.312		.324	4.4	.682	161.1
5300.0000	.682 161.2	.325	4.3				160.1
5350.0000	.672 160.2	.334	7.4	.334	7.3	.669	
5400.0000	.661 160.3	.346	9.3	. 345	9.3	.661	160.1
5400.0000	.661 160.2	.345	9.3	. 345	9.2	.661	160.1
5450.0000	.654 157.6	.361	12.2	. 361	12.1	.654	157.5
5500.0000	.646 152.8	.377	14.9	.376	14.8	.643	152.8
5550.0000	.645 150.8	. 400	16.5	.400	16.5	.645	150.7
5600.0000	.651 151.5	.423	18.6	.423	18.4	.650	151.4
5600.0000	.650 151.4	.423	18.4	.423	18.4	.650	151.4
5650.0000	.648 149.6	.436	18.8	.434	18.7	.645	149.5
5700.0000	.649 146.1	.457	20.0	.457	20.0	.649	145.9
5750.0000	.646 143.5	.470	20.7	.470	20.8	.644	143.4
5800.0000	.639 144.0	.491	21.0	.490	20.9	.638	143.9
5800.0000	.639 144.1	. 491	21.0	.490	21.0	.639	143.9
5850.0000	.634 142.2	.507	20.3	.507	20.3	.630	142.1
5900.0000	.6:9 138.7	.516	19.5	.516	19.5	.619	138.6
	.6:4 136.1	.531	19.5	.530	19.4	.613	136.0
5950.0000		.545	20.1	.543	20.1	.605	135.8
6000.0000			20.1	.543	20.0	.606	135.7
6000.0000	.609 135.8	.546		,555	19.9	.597	134.0
6050.0000	.599 134.0	.557	19.8	.579	19.8	.594	131.8
6100.0000	.594 131.9	.579	19.8		19.9	.592	130.7
6150.0000	.592 130.8	.594	20.0	.592			
6200.0000	.589 131.5	. 684	19.4	.601	19.3	.586	131.5
6200.0000	.589 131.4	. 604	19.4	.602	19.4	.586	131.4
6250.0000	.583 129.1	.613	19.3	.611	19.3	.579	129.0
6300.0000	.573 127.0	.619	18.9	.618	18.8	.573	126.9
6350.0000	.571 127.3	.633	18.5	.633	18.5	.571	127.3
6400.0000	.564 127.5	.647	18.2	. 645	18.2	.561	127.5
6400.0000	.564 127.5	.646	18.0	.643	18.0	.561	127.5
6450.0000	.557 124.5	.655	17.0	. 655	17.0	.554	124.5
6500.0000	.551 122.4	.662	17.0	.662	17.0	.549	122.3
6550.0000	.547 122.9	.674	16.5	.670	16.5	. 544.	122.9
6600.0000	.544 123.8	.686	16.5	.686	16.4	.541	123.8
6600.0000	.542 123.8	.685	16.6	.685	16.5	.540	123.8
6650.0000	.534 120.8	.698	15.8	.698	15.8	.534	120.7
6700.0000	.523 117.0	.709	15.1	.784	15.1	.520	116.9
6750.0000	.526 118.7	.717	14.6	.717	14.6	.523	118.6
6800.0000	.507 120.1	.726	14.4	.724	14.3	. 506	120.1
		.727	14.4	.723	14.3	.507	120.1
6800.0000	.508 120.1 .502 116.8	.719	14.1	.719	14.1	.500	116.8
6850.0000		.739	14.1	.739	14.0	.489	114.2
6900.0000	.492 114.2		13.3	.745	13.3	.485	114.0
6950.0000	.485 114.1	.746		.748	12.5	.476	116.0
7000.0000	.478 116.0	.752	12.5		12.5	.477	116.0
7000.0000	.479 116.0	.751	12.5	.748			113.4
7200.0000	.457 113.5	.791	11.8	.786	11.7	. 454	112.9
7400.0000	.441 113.0	.799	11.2	.795	11.1	.441	
7600 <b>.0000</b>	.4:6 106.6	.814	8.8	.814	8.7	.416	106.6
7800.0000	.401 105.9	.840	6.0	.835	6.0	.400	105.9
8000.0000	.372 102.6	.847	5.0	.842	5.0	.372	192.5
8200.0000	.354 102.5	.852	. 5	. 851	. 4	. 354	102.4
8400.0000	.368 98.5	.841	9	.837	-1.0	.366	98.4
8600.0000	.383 97.6	.848	8	.845	9	. 381	97.6
8880.0000	.398 92.4	.838	-1.8	.837	-1.9	.398	92.3
9000.0000	.405 90.9	.841	-2.0	. 837	-2.1	. 405	90.9
9200.0000	.4:6 89.6	.837	-2.8	.835	-2.9	.415	89.5
9400.0000	.4:9 87.6	.840	-3.5	.837	-3.5	.419	87.6
9600.0000	.4:6 86.1	.839	-3.7	.835	-3.7	.416	86.1
9800.0000	.406 84.9	.842	-5.0	.837	-5.0	.405	84.7
10000.0000	.390 86.7	.854		-13.854	-5.6		86.5
10200.0000	.376 89.8	.863	-4.2	.862	-4.3	.374	89.7
10500.000	1010 0710			•			

10400.0000	.362	89.1	.883	-5.4	.878	-5.5	.360	89.0
10600.0000	.3:2	90.7	.880	-6.0	.880	-6.1	.310	90.8
10800.0000	.280	93.1	.899	-6.4	.899	-6.4	.280	93.1
11000.2000	.243	94.6	.919	-9.7	.919	-9.8	.242	94.6
11200.0000	.248	92.6	.889	-13.1	.888	-13.2	.248	92.4
11400.0000	.249	89.5	.875	-13.8	.875	-13.9	.249	89.6
11600.0000	.302	85.3	.888	~15.8	.883	-15.8	.302	85.3
11800.0000	.3:2	84.7	.849	-17.5	.849	-17.5	.311	84.7
12000.0000	.345	93.6	.822	-14.3	.820	-14.4	.345	93.6
12200.0000	.375	95.9	.832	-14.1	.831	-14.2	.375	95.9
12400.0000	.385	91.9	.819	-13,2	.819	-13.2	.385	91.7
12600.0000	.368	86.4	.808	-13.0	.808	-13.0	.367	86.3
12800.0000	.328	79.5	.818	-13.5	.818	-13.5	.326	79.5
13000.0000	.261	76.3	.818	-13.7	.818	-13.7	. 259	76.1
13200.0000	.180	93.7	.815	-15.0	.815	-15.0	.180	93.9
13400.0000	.232	123.7	.804	-14.6	.803	-14.7	. 232	123.8
13600.0000	.308	129.0	.808	-12.0	.803	-12.1	.308	129.1
13800.0000	.341	125.2	.852	-10.4	.852	-10.4	.340	125.3
14000.0000	.330	117.6	.881	-14.6	.878	-14.6	.330	117.5
14200.0000	. 295	109.6	.869	-14.6	.869	~14.7	. 295	109.4
14400.0000	.280	98.6	.909	-16.0	.906	-16.1	.280	98.8
14600.0000	.246	82.9	.910	-19.9	.906	-19.9	. 245	82.9
14800.0000	.221	77.8	.917	-20.0	.913	-20.1	. 221	77.5
15000.0000	.203	76.7	.933	-21.6	. 929	-21.6	.203	76.8



FREQUENCY	REFL COEFF -		ORWARD 21	LOSS-RE		REFL COE	
MHz	MAG AN		ANG	MAG	ANG	MAG	ANG
2000.0000	.369 -121	.3 .879	-21.2	.879	-21.2	. 372	-121.5
2200.0000	.406 -126	• - • - • •	-24.4	.840	-24.4		-126.9
2400.0000	.451 -132		-28.4	.791	-28.3		-133.2
2600.0000	.501 -140		-33.0	.737	-33.0		-140.4
2800.0000	.556 -148		-36.2	.654	-36.2		-147.9
3000.0000	.6:1 -155		-39.4	.545	-39.4		-155.7
3000.0000	.6:1 -155		-39.5	.546	-39.5	.615	
3050.0000			-39.4	.516	-39.4	.631	-158.7
3100.0000	.637 -159		-39.8	.494	-39.8		-159.7
3150.0000	.649 -161		-40.4	.468	-40.4		-162.1
3200.0000	.662 -165		-40.2	.431	-40.1	.667	
3200.0000	.662 -165	.4 .432	-40.0	.432	-40.1	.667	
3250.0000	.670 -168	.2 .405	-38.8	.405	-38.8	.677	-168.2
3300.0000	.682 -170	.5 .381	~36.9	.381	-37.0	.687	~170.6
3350.0000	89 -173	.5 .357	-34.3	.357	-34.3	.693	-173.7
400.0000	.700 -175	.7 .337	-31.9	.337	-32.0	.705	-175.8
3400.0000	.701 -175	.8 .337	-31.9	.337	-31.9	.705	-175.9
3450.0000	.705 -177	.2 .314	-28.3	.313	-28.3	.710	-177.3
3500.0000	.7:0 179	.8 .291	-23.5	. 291	-23.5	.714	179.8
3550.0000	.7,5 175		-18.1	.276	-18.1	.720	175.6
- 3600.0000	.7:8 173		-12.1	.267	-12.2	.722	173.6
3600.0000	.7:8 173		-12.1	.267	-12.1	.722	173.6
3650.0000	.723 173		-6.7	.266	-6.6	.727	173.0
3700.0000	.722 170		-1.8	. 264	-1.9	.726	170.3
3750.0000	.723 165		3,5	. 265	3.5	.727	165.8
3800.0000	.728 163		7.9	. 274	8.0	.730	163.2
3800.0000	.729 163		8.0	.274	7.9	.730	163.1
3850.0000	.727 162		13.0	.288	13.1	.730	162.7
3900.0000	.725 161		16.3	.304	16.2	.726	161.1
3950.0000 4000.0000	.7:9 157		18.9 21.3	.323 .336	18.8	.721 .719	157.8 154.5
4000.0000	.7:6 154		21.3	.336	21.3	.719	154.5
4050.0000	.7:6 154		23.5	.354	23.5	.719	154.0
4100.0000	.7:2 153		26.0	.372	26.0	.712	153.5
4150.0000	.7:0 150		27.8	.393	27.8	.710	150.5
4200.0000	.705 147		28.1	.414	28.1	.709	147.2
4200.0000	.794 147		28.1	.414	28.1	.707	147.0
4250.0000	.782 146		28.7	.431	28.7	.703	146.6
4300.0000	.696 145		29.7	.440	29.6	. 698	145.5
4350.0000	.691 143	3.8 .455	30.4	.456	30.5	.692	143.7
4400.0000	.687 142	.3 .473	30.8	.473	30.9	.689	142.2
4400.0000				.474	31.0	.690	142.2
4450.0000	.684 146			.493	30.4	. 685	140.6
4500.0000				.510	29.6	.679	139.4
4550.0000				.519	29.0	.676	137.7
4600.0000				. 531	28.3	.672	136.8
4600.0000			28.4	. 531	28.3	.671	136.9
4650.0000				. 548	28.5	. 666	135.6
4700.0000				.569	28.7	. 662	133.5
4750.0000				.584	27.9	. 659	131.8
4800.0000				.595 .594	27.2 27.0	.650 .649	131.9 131.9
4800.0000 4850.0000				.604	27.0	.646	131.9
4900.0000			27.0	.611	27.0	.642	129.4
4950.0000				.620	27.2	.634	127.0
5000.0000				B-16.635	26.1	.632	127.3
5000.0000		2.5 .634	26.2	B-16.634	26.2	.631	127.4
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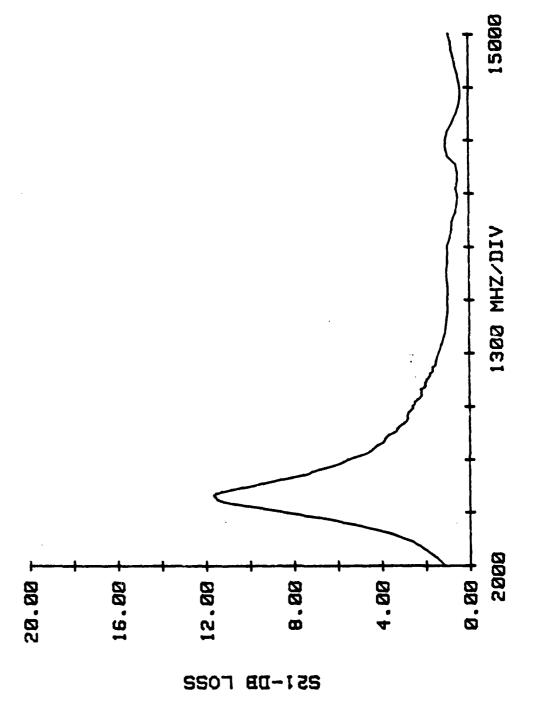
					05 0	.626	28.0
5050.0000	.624 128.0	.642	25.3	.641	25.3		
5100.0000	.622 125.3	. 644	24.7	.644	24.7		25.1
5150.0000	.6:7 122.7	.649	24.5	.650	24.5		22.7
5200.0000	.609 123.0	.657	24.8	.657	24.8		122.9
	.609 123.0	. 657	24.7	.658	24.7	.609	122.9
5200.0000		.673	24.2	.673	24.2	.608	123.9
5250.0000	.608 124.0		23.5	.685	23.5		122.2
<b>5</b> 300.0000	.602 122.2	.684		.686	23.2		119.9
5350.0000	.596 119.9	.686	23.2				119.2
5400.0000	.592 119.3	.695	23.2	,695	23.2		-
5400.0000	.592 119.3	.694	23.2	. 694	23.2		119.2
5450.0000	.590 120.3	.704	23.5	.704	23.6		120.2
5500.0000	.584 119.1	.714	23.7	.715	23.8		119.1
5550.0000	.579 116.8	.723	23.4	.724	23.4		116.8
	.574 116.5	.726	23.6	.726	23.6		116.4
5600.0000	574 116.5	.727	23.6	.727	23.6	.574	116.4
5600.0000		.725	22.8	.727	22.8	.571	116.6
5650.0000	.570 116.7	.727	22.7	.727	22.7		115.7
5700.0000	.564 115.8			729	22.8		114.9
5750.0000	.560 114.9	.729	22.8		22.6		114.7
5800.0000	.554 114.8	.738	22.6	.738		.555	114.8
5800.0000	.554 114.8	.737	22.5	.738	22.5		113.4
5850.0000	.550 113.6	.746	21.7	.747	21.8	.552	
5900.0000	.545 112.9	.745	20.8	.746	20.8	.545	112.7
5950.0000	.542 113.2	.753	20.5	.753	20.5	.542	113.1
	.536 112.9	. 755	20.8	.756	20.8	.537	112.9
6000.0000	_	.756	20.8	.756	20.8	.539	112.8
6000.0000		.764	20.2	.764	20.2	.529	111.5
6050.0000		.775	19.7	.775	19.8	.525	110.3
6100.0000	.525 110.3		19.7	.781	19.7	.521	110.6
6150.0000	.521 110.7	.782		.780	19.1	.516	111.7
6200.0000	.5.6 111.8	.780	19.1		19.2	.517	111.6
6200.0000	.5:5 111.6	.780	19.2	.780		.509	110.1
6250.0000	.509 110.2	.781	19.1	.782	19.1		107.7
6300.0000	.502 107.8	.778	18.7	.778	19.7	.502	
6350.0000	.501 108.7	.791	18.6	.791	18.6	.502	108.5
6400.0000	.496 110.0	.799	18.4	.799	18.4	.497	110.0
6400.0000	.496 110.0		18.2	.796	18.2	.496	109.9
6450.0000	490 108.2		17.5	.797	17.5	.490	108.2
	.485 106.0		17.4	.800	17.4	. 485	105.9
6500.0000			17.1	.804	17.1	.482	106.1
6550.0000	- ·		16.8	.811	16.8	.480	107.7
6600.0000	- · · · · · · · · · · · · · · · · · · ·		16.9	.812	16.9	.479	107.7
6600.0000	.480 107.8		16.6	.817	16.6	.473	106.9
6650.0000	.473 107.0			817	16.0	.466	194.5
6700.0000	.466 104.7		16.0	.828	15.6	.465	104.1
5750.0000	.464 104.2		15.6		16.0	.458	195.7
6800.0000	.458 105.8		15.9	.828	15.9	.459	105.7
6800.0000	.459 105.8		15.8	.829		.452	105.7
6850.0000	.451 105.8		16.1	.829	16.1		103.2
6900.0000	.448 103.3	.841	16.2	.840	16.2	.448	
6950.0000	.444 102.2	.843	15.7	.843	15.8	.444	102.2
7000.0000	.439 103.4	.844	15.7	.843	15.7	.439	103.4
7000.0000	.439 103.5		15.6	.844	15.6	.439	103.4
	.421 101.3		15.8	.854	15.8	.421	101.2
7200.0000	408 99.		14.7	.871	14.7	.408	99.4
7400.0000			13.4	.881	13.4	.393	98.3
7600.0000			11.5	.886	11.5	.382	97.4
7800.0090	.382 97.4		9.7	.893	9.7	.376	97.1
3000.0000	.376 97.3			.894	8.4	.372	96.0
8200.0000	.373 96.		8.4		7.9	.371	94.7
8400.0000	.371 94.		7.8	.894		.369	93.5
8600.0000	.369 93.		7.8	.897	7.8		92.8
8800.0000	.368 92.		7.0	.897	7.1	.368	
9000.0000	.367 92.		6.8		6.9	. 366	92.1
9200.0000	.362 91.		5.3		5.4	.362	91.3
9400.0000	.355 91.		4.6		4.6	.355	90.9
9600.0000	.346 90.		4.1	.898	4.2	.345	90.8
9800.0000	.336 91.		3.6	. 897	3.7	. 336	91.1
	.324 91.		3.1	n 909	3.2	.324	90.9
10000.0000	3:1 90.		4.1	B-1/.917	4.1	.311	90.7
10200.0300							

XE

7.20

	A // T	00.7	.920	3.9	.921	4.0	. 297	90.6
10400.0000	.297	90.7		3.3	.934	3.4	.279	91.2
10600.0000	.279	91.4	.934		.943	1.3	.267	91.9
10800.0000	. 267	92.0	.942	1.2			.267	93.2
11000.0000	.267	93.4	.948	1	.948	.0		94.1
11200.0000	.282	94.3	.938	-2.0	. 938	-2.0	.282	
11400.0000	.290	97.5	.947	-2.7	.946	-2.7	. 289	97.3
11600.0000	.286	103.2	. 945	-2.8	.944	-2.7	. 286	103.0
11500.0000	.3:.7	103.4	.938	-3.6	. 938	-3.5	.317	103.4
12000.0000	.379	96.1	.897	-3.8	.895	-3.8	.379	96.0
12200.0000	.398	92.7	.889	-3.1	.888	-3.0	.398	92.7
12400.0000	373	93.1	.891	-2.0	. 89ઇ	-2.0	.373	93.1
	.327	93.6	.898	-2.9	.898	-2.8	.326	93.6
12800.0000		93.0	.920	-3.4	.920	-3.3	.268	92.9
12800.0000	.268	92.7	.937	-3.9	.937	-3.8	.206	92.6
13090.0000	.207		.953	-5.1	.952	-5.1	.160	94.6
13200.0000	.161	94.9		-6.6	.962	-6.5	. 191	98.9
13400.0000	. 191	99.2	. 962		.961	-7.1	.203	97.1
13600.0000.	.204	97.2	.961	-7.2		-8.4	.231	92.3
13800.0000	. 231	92.5	. 956	-8.4	. 956			86.3
14000.0000	.255	86.4	.948	-9.6	.947	-9.6	. 255	
14200.0000	.282	81.5	.937	-10.8	.937	-10.7	. 282	81.6
14400.0000	.306	78.6	.930	-12.2	.930	-12.1	.306	78.5
14600.0000	.328	76.8	.918	-13.0	.918	-12.9	.328	76.5
14890.0000	.349	75.6	.915	-12.9	.914	-12.8	.349	75.5
15000.0000	.362	75.1	.904	-12.8	. 904	-12.7	.362	74.9
110001000								

THRUT PER # 4.74 CM OUTPUT REF = 4.74 CM



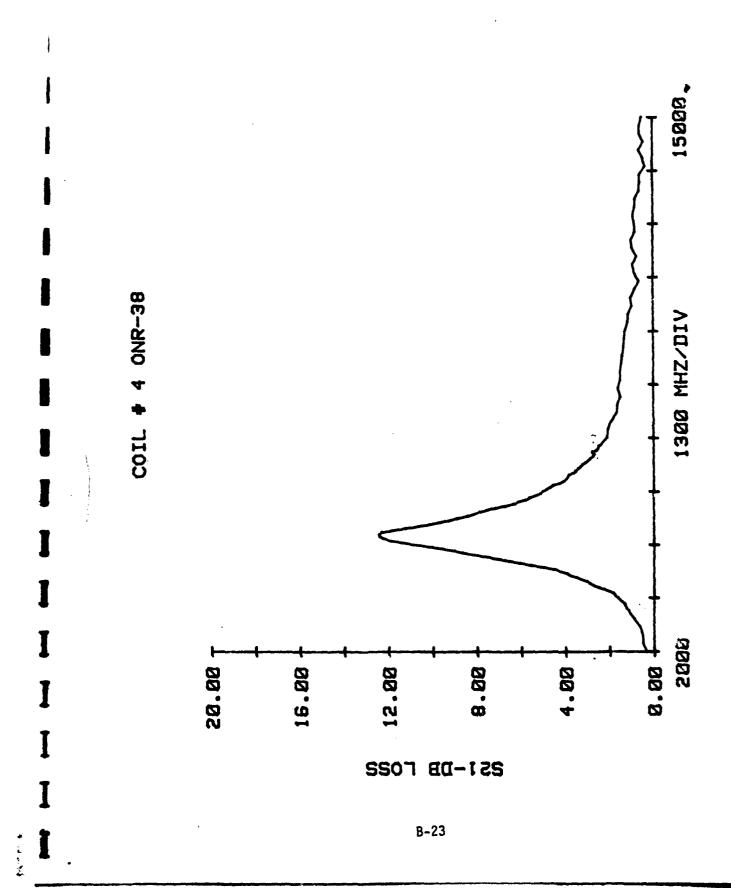
FREQUENCY	REFL COEFF -IN	LOSS-FOR	WARD	LOSS-REV	ERSE I	REFL COEF	
	S11	S21 Mag	ANG	S12 Mag	ANG	S21 MAG	2 ANG
MHZ	MAG ANG	nnu	ma				
2000.0000	.229 -109.1	.965	-14.8		-15.1		-105.7
2200.0000	.250 -108.8	.948	-15.6		-15.8		-105.7
2400.0000	.273 -112.8	.946	-16.9		-17.1		-109.5
2600.0000	.287 -118.0	.933	-19.8		-20.1		-114.8
2800.0000	.303 -123.6	.904	-21.7		-22.0		-119.9
3000.0000	.338 -127.3	.877	-24.8		-25.2		-123.6
3000.0000	.338 -127.2	.879	-24.8		-25.2		-123.5
3050.0000		.868	-25.5	.869	-26.1		-124.8
3100.0000	.360 -127.7	.864	-26.5	.864	-27.0		-123.9
3150.0000	.371 -129.5	.862	-27.7	.862	-28.1		-125.6
3200.0000	.383 -132.7	.849	-28.9	.847	-29.4		-128.8
3200.0000	.383 -132.7	.850	-28.9	.847	-29.4		-128.7
3250.0000	.394 -133.8	.841	-29.6	.838	-30.1		-129.6
3300.0000	.4:0 -133.2	.833	-30.0	.834	-30.6		-129.1 -130.8
3350.0000	.421 -134.8	.820	-30.4	.820	-31.0		
3400.0000	.434 -137.4	.813	-31.2	.814	-31.7		-133.6
3400.0000	.434 -137.4	.813	-31.1	.814	-31.6		-133.6
3450.0000	.446 -140.3	.797	-32.1	.797	-32.8		-136.3 -136.8
3500.0000	.457 -141.0	.776	-33.2	.773	-33.9		-137.6
3550.0000		.754	-34.1	.752	-34.8		-140.3
3600.0000	.483 -144.4	.734	-34.6	.734	-35.3		
3600.0000		.734	-34.5	.734	-35.2		-140.3 -143.0
3650.0000	.495 -147.2	.719	-35.1	.719	-35.9		-143.9
3700.0000		.709	-36.0	.710	-36.7		-145.2
3750.0000	.524 -149.6	.687	-37.1	.684	-37.6		-146.8
3800.0000	.539 -150.9	.671	-37.1	.667	-37.7		-146.8
3800.0000	.541 -151.0	.672	-37.0	.668	-37.6		-149.4
3850.0000	.558 -153.5	.649	-37.2	.647	-37.8		-152.2
3900.0000	.574 -156.6	.638	-37.4	.638	-37.9		-153.8
3950.0000	.587 -158.5	.617	-38.3	.616	-38.8		-155.3
4000.0000	.599 -159.8	.596	-40.1	.593	~40.6		-155.5
4000.0000	.598 -160.0		-40.1	.594	-40.7 -41.0		-157.6
4050.0000			-40.6	.559	-41.6 -42.5		-161.5
4100.0000	6:.7 -165.9		-42.0	.528 .497	-42.8		~165.2
4150.0000	629 -169.7	.500	-42.2	.470	-42.9		-165.8
4200.0000			-42.3 -42.2	.470	-42.8		-165.9
4200.0000			-42.2	.446	-43.1		-168.1
4250.000		.448	-42.7	.419	-43.1	~30	-170.4
4300.000		.419	-40.9	.393	-41.5		-172.7
4350.000	4 - 4 - 4 - 4		-39.1	.369	-39.4		-173.2
4400.000		.371	-39.0	.369	-39.4		-173.3
4400.000			-36.2	.354	-36.6		-173.0
4450.000			-34.7		-35.1		-173.9
4500.000			-32.5		-32.9		-177.2
4550.000			-29.4		-29.7		-179.3
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4600.000			-25.1	.271	-25.4		
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4700.000	- · · · · · · · · · · · · · · · · · · ·		-15.6		-16.2		
4750.000	•		-9.4		-10.6	3 .742	
4888.000	و محمد ما ساست		-9.6		-10.1		
4800.000	- · · · · · · · · · · · · · · · · · · ·				-4.3		
4850.000		·			2.0	0 .743	
4900.000			_		8.		
4950.000		· .	14.1	B-20-275			
5000.000			14.2	28-20.275			3 168.8
5000.000	. 100 103.						

5050.0000	.778	161.6	. 296	17.5	. 296	17.0	.776	166.6
5100.0000	.778	157.4	.313	20.1	.312	19.5	.779	162.9
5150.0000	.774	155.9	.328	21.7	. 330	21.4	.773	161.6
5200.0000	.765	155.9	. 347	24.4	.349	23.9	.765	161.5
5200.0000	.765	155.9	.347	24.4	.349	23.9	.764	161.5
5250.0000								
	.744	153.5	.362	24.8	. 364	24.2	.744	158.8
5300.0000	.725	149.1	.381	24.8	. 383	24.0	.725	154.6
5350.0000	.7:0	148.0	. 394	25.5	.396	24.7	.710	153.8
5400.0000	.698	149.0	. 406	25.7	.409	24.9	. 698	154.6
5400.0000	.698	149.0	.406	25.7	.408	24.8	. 699	154.6
5450.0000	.689	147.7	.422	26.9	.423	25.9	.690	152.8
5500.0000	.679	143.3	.439	28.3	.441	27.2	. 680	148.4
55:0.0000	.681	141.0	.463	28.6	. 464	27.6	.680	146.6
5600.0000	.690	142.3	.486	29.6	.486	28.6	.688	148.0
5600.0000	.689	142.3	.486	29.5	.486	28.5	.687	
5650.0000								148.0
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5780.0000	.687	138.3	.516	29.5	.515	28.5	.687	143.9
5750.0000	.685	136.2	.525	29.7	. 524	28.8	.683	141.9
5800.0000	.676	136.9	.543	29.7	.542	28.6	.676	142.8
5800.0000	.677	137.0	.543	29.7	.541	28.5	.676	142.8
5850.0000	.670	136.0	.557	28.5	.556	27.4	.671	141.5
5900.0000	.655	133.2	.562	27.5	.560	26.4	.656	138.4
5950.0000	.652	131.1	.573	27.2	. 571	26.0	.651	136.4
6000.0000	.644	131.3	.585	27.8	.583	26.6	.646	136.6
6000.0000	.645	131.1	. 585	27.7	.583	26.5	.647	136.5
6050.0000	.636	130.1	.593	27.3	.591	26.2		135.3
6100.0000							.638	133.3
	.632	128.4	.615	27.3	.613	26.0	.634	133.6
6150.0000	.631	128.0	.627	27.4	.623	26.2	.634	133.2
6203.0000	.627	129.0	.636	26.6	.630	25.5	.629	134.1
6200.0000	.627	128.9	.636	26.7	.630	25.6	.629	134.1
6250.0000	.620	127.4	.641	26.5	.637	25.5	.623	132.3
6300.0000	.6:3	125.4	.645	26.0	. 640	25.9	.615	130.3
6350.0000	.6∴0	126.2	.660	25.7	.655	24.7	.615	131.1
6400.0000	.602	126.8	.671	25.4	. 665	24.4	.608	131.4
6400.0000	.602	126.8	.668	25.2	.663	24.2	.607	131.3
6450.0000	.596	124.3	.677	24.1	.671	23.1	. 601	128.8
6500.0000	.591	122.6	.685	24.1	.677	23.3	. 596	127.2
6550.0000	.588	123.9	.693	23.6	.685	22.8	.593	128.4
6600.0000	.587	125.1	.704	23.6	.698	22.8	.591	129.4
	.586	125.1	.704	23.6				
6600.0000					.698	22.9	.590	129.4
6650.0000	.579	122.4	.714	22.9	.709	22.2	.584	126.3
6700.0000	.568	119.1	.721	22.2	.716	21.5	.572	123.4
6750.0000	.571	121.4	.731	21.7	.725	21.1	. 575	125.6
6800.0000	.554	122.9	. 737	21.4	.731	20.8	.558	126.8
$\epsilon$ 800.0000	.555	122.9	.738	21.4	.731	20.8	.559	126.8
6850.0000	.551	119.9	.729	21.1	.723	20.5	. 554	123.5
6900.0000	.540	117.7	.748	21.1	.743	20.5	. 544	121.4
6950.0000	.538	118.0	.753	20.4	.745	19.8	.540	121.9
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7200.0000	.5:.6	119.2	.789	19.0	.788	18.5	.515	123.0
7400.0000	.506	119.5	.793	18.8	.793	18.3	.502	123.3
7600.0000		113.7	.806	17.1	.809			
	. 489					16.5	.481	118.2
7800.0000	. 476	112.6	.830	15.1	.835	14.3	.468	118.2
8000.0000	.444	109.9	. 834	15.0	.840	13.9	.434	116.8
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8490.0000	.419	104.7	.836	9.4	. 83 <del>9</del>	7.7	.416	114.4
8600.0090	.420	103.7	.847	9.8	.847	8.1	.421	114.4
8800.0000	.423	98.7	.846	9.1	.844	7.3	.429	110.2
9000.0000	.4:8	97.5	.850	9.2	.847	7.4	.430	109.6
9200.0000	.4:8	96.6	.855	8.4	.844	6.5	.435	108.9
9400.0000	.4:4	95.2	. 861	7.7	.851	6.1	. 434	107.3
9600.0000	.408	93.9	.864	7.5	.853	6.1	.428	105.7
9800.0000	.396	93.3	.868	6.0	.859	4.6	.414	104.5
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	.374	98.2	.883	6.3		5.0	.382	
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21.0

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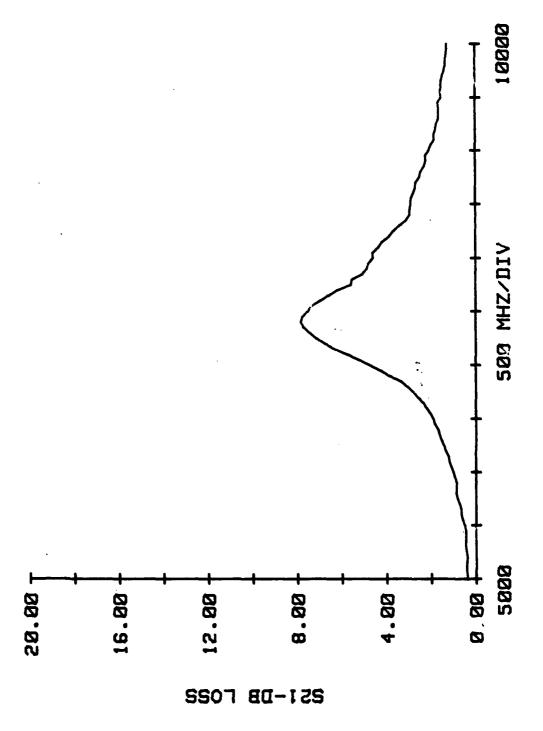
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11630.0000	.269	74.4	.923	-1.5	.925		.264	99.7
11800.0000	.267	72.4	.901	-2.2	.911	-5.7		
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12800.0000	294	84.1	.914	8	.896	-3.6	.322	100.2
13000.0000	291	84.7	.914	8	.900	-3.6	.310	99.2
13200.0000	292	87.1	.934	-2.3	. 923	~5.0	.297	99.7
	.280	88.1	.938	-4.3	. 936	-7.3	.269	100.7
13400.0000		94.7	.939	-3.5	, 938	~7.1	.227	109.7
13600.0000	. 256	• -	.966	-4.0	.960	-7.9	.204	123.7
13800.0000	.236	101.8	.955	-7.2	.957	-11.5	. 203	129.9
14000.0000	.229	103.6		-7.0	,935	-12.8	,199	127.1
14200.0000	.229	100.0	. 935			-14.1	.205	115.6
14400.0000	. 249	89.5	.957	-8.1	.945		.203	99.8
14600.0000	. 247	75.3	.938	-11.2	.933	-17.7		93.4
14800.0000	. 246	70.7	.939	-10.4	.920	-18.3	.234	
15000.0000	.241	69.7	.949	-11.5	.917	-19.7	.274	88.5



			1000	I OCC_PEU	, EDGE E	eel coee	F -OUT
FREQUENCY	REFL COEFF -IN	LOSS-FORWARD S21		LOSS-REVERSE S12		REFL COEFF -OUT \$22	
MHz	MAG ANG		ANG	MAG	ANG	MAG	ANG
5000.0000	.073 -109.1	.958 -	15.9	.958	-16.0	.073 -	
5050.0000	.068 -123.6	.957 -	15.6	.952	~15.7	.067 -	
5100.0000	.062 -154.2		15.2	.953	-15.3		-154.3
5150.8000	.079 -166.8		14.9	.952	-15.0		-167.0
5200.0000	.083 -176.9		-15.3	. 957	-15.3	.083 -	-177.2
5250.0000	.096 176.1		-16.2	.953	-16.2	.096	175.9
5300.0000	.098 176.3		-17.2	.950	-17.2	.098	176.3
5350.0000			-18.5	.949	-18.5	.094	176.3
5400.0000			-19.6	. 951	-19.6		-178.2
5450.0000	_	.951 -	-20.4	. 951	-20.5		-162.9
5500.0000		.943 -	-20.9	.943	-21.0		-148.9
5550.0000		.934 -	-20.9	.934	-21.0		-139.4
5600.0000		.928	-20.9	.928	-20.9		-125.9
5650,0000		.928 -	-21.0	.928	-21.0		-120.0
5700.0000	.131 -116.4		-21.0	.921	-21.0		-116.5
5750.0000			-21.2	.911	-21.2		-113.7
5800.0000			-21.6	. 905	-21.6		-117.1
5850.0000	.168 -119.5		-22.3	.907	-22.3		-119.4
5900.0000	.182 -123.6		-23.6	.906	-23.6		-123.4
5950.0000			-24.9	.898	-24.9		-125.2
6000.0000	.206 -128.4		-25.9	.891	-25.9		-128.2
6050.0000	.2:8 -128.8		-26.4	.881	-26.5		-128.8
6100.0000	.224 -130.7		-26.4	.873	-26.4		-130.7
6150.0000			-26.5	.872	-26.6		-131.2
6200.0000	.244 -131.2		-26.8	.857	-26.9		-131.2
6250.0000			-27.1	.851	-27.1		-131.6
6300.0000			-27.4	.839	-27.4		-132.2
6350.0000			-28.5	.831	-28.6		-133.0 -134.1
6400.0000			-29.1	.824	-29.2		-135.0
6450.0000			-29.3	.810	-29.4 -29.3		-137.2
6500.0000			-29.3 -29.8	.804 .792	-29.8		-140.8
6550.0000			-30.6	.777	-30.8		-144.9
6600.0000			-32.1	.763	-32.1		-147.3
6650.0000			-33.2	.743	-33.3		-148.9
6700.000			-34.5	.727	-34.7		-151.3
6750.000( 6800.000(			-36.1	.792	-36.2		-151.2
6850.000			-37.5	.679	-37.5		-153.3
6900.000			-38.1	.641	-38.3	.417	-155.1
6950.000			-38.1	.613	-38.0	.436	-157.3
7000.000			-36.9	.579	-37.1		-158.9
7050.000			-35.8	.548	-35.8		-159.4
7100.000			-33.5	.515	-33.7		-158.9
7150.000			-31.1	.483	-31.3		-160.4
7200.000			-27.2	.461	-27.2		-161.4
7250.000			-24.9	. 439	-24.9		-163.4
7300.000	0 .557 -165.1	. 424	-21.4	. 424	-21.4		-165.0
7350.000			-17.2	.412	-17.4		-165.0
7400.000			-14.2	. 406	-14.2		-165.7 -166.5
7450.000			-6.6	.409	-9.8		-170.2
7500.000			-7.9	.421	~7.8		-173.2
7550.000			-4.6	.428	~4.7		-176.0
7600.000			-1.1	.449	-1.2 1.0		-179.4
7650.000			1.1	.468	2.8		177.9
7700.000			2.9	.491			
7750.000			3.5	B-24.526	4.5	-	
7800.000	0 .470 166.9	.529	4.6	. 549	4.5	. 710	.00,9

		•						
7850.0000	.480	160.5	.558	4.4	.558	4.2	. 489	160.6
7900.0000	.471	152.6	.571	5.1	. 571	5.0	.471	152.8
7950.0000	.480	146.8	.575	4.7	. 575	4.6	.480	146.9
- 8000.0000	.488	141.2	.590	4.8	.588	4.7	.487	141.4
8050.0000	.495	135.8	.588	5.6	.588	5.6	. 494	135.8
8100.0000	.5:0	133.2	.606	7.6	. 606	7.5	.510	133.3
\$150.0000	.5:9	130.3	.618	8.0	.618	8.0	.518	130.3
8200.0000	.525	131.8	.641	9.9	.640	9.8	. 522	132.1
8250.0000	.536	131.4	.656	10.1	.656	10.1	.536	131.4
8300.0000	.525	132.0	. 675	9.7	.675	9.5	.525	132.1
8350.0000	.525	130.0	.700	9.1	.696	9.0	. 525	130.0
8400.0000	.526	130.8	.713	6.3	.713	6.1	.526	130.7
8450.0000	. 564	132.2	.714	5.7	.711	5.6	.504	132.2
8500.0000	.5:.0	132.7	.717	4.5	.717	4.3	.510	132.7
8550.0000	. 489	133.2	.719	4.3	.719	4.3	. 489	133.1
8600.0000	. 485	130.4	.727	4.6	.727	4.5	. 485	130.4
8650.0000	.474	128.2	.735	4.2	.735	4.1	.474	128.1
8700.0000	.469	125.4	.736	5.1	.736	5.1	.469	125.4
8750.0000	.464	126.1	.750	5.5	.750	5.3	.465	126.1
8800.0000	. 451	125.1	.75 <b>5</b>	5.6	. 755	5.5	.451	125.0
8850.0000	.448	124.1	.769	4.9	.769	4.8	.448	124.0
8900.0000	.430	121.5	.776	4.5	.776	4.5	.430	121.5
8950.0000	.429	119.3	.774	4.2	.773	4.1	.429	119.3
9000.0000	.4:3	118.4	.788	3.6	.788	3.2	.413	118.4
9050.0000	.409	117.7	.797	2.9	.794	2.8	.408	117.7
9100.0000	.399	118.2	.810	2.6	.810	2.4	.399	118.1
9150.0000	.387	116.7	.809	2.3	.809	2.2	.386	116.6
9200.0000	.379	115.4	.816	2.7	.815	2.6	.379	115.4
9250.0000	.373	114.1	.819	2.8	.819	2.7	.373	114.2
9300.0000	.367	114.1	.829	2.4	.829	2.3	.367	114.1
9350.0000	. 361	114.1	.829	2.1	.829	1.9	.361	114.1
9400.0000	.359	113.3	.830	1.6	.830	1.4	.359	113.3
9450.0000	.356	112.6	.827	1.0	.827	. 9	.356	112.5
9500.0000	.355	111.5	.839	.7	.839	.5	. 355	111.5
9550.0000	. 354	110.7	.837	. 2	.837	. 1	.354	110.7
9600.0000	,352	109.8	.840	. 2	.840	. 1	.352	109.7
9650.0000	.348	107.9	.841	. 0	.837	0	.348	107.8
9700.0000	.344	105.3	.846	.3	.846	. 2	.344	105.2
9750.0000	342	103.3	.854	1	.854	3	.342	103.2
9800.0000	.337	103.2	.859	5	.860	~.7	.337	103.1
9850.0000	.334	103.6	.860	9	.860	-1.0	.334	103.5
9900.0000	.335	104.8	.862	-1.6	.862	-1.8	. 335	104.9
9950.0000	.332	104.8	.866	-2.2	.866	-2.3	.331	104.8
10000.0000	.340	104.3	.865	-2.7	.865	-2.9	.339	104.3
.0000.0000	. 0.10			<b></b>				

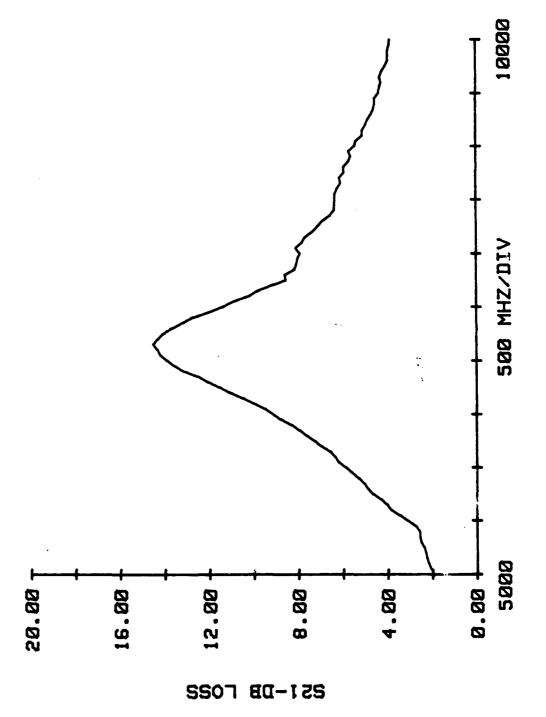




FREQUENCY	REFL COEFF -IN	LOSS-FORW S21	IARD	LOSS-REV		REFL COL	EFF -OUT
MHz	MAG ANG	MAG	ANG	MAG	ANG	MAG	ANG
5000.0000	.406 -151.3		36.6	.804	-36.6	.408	-151.4
5050.0000	.4:3 -156.0		37.1	.788	-37.1		-156.1
5100.0000	.4:1 -160.2		·37.6 ·38.1	.778	-37.7		-160.4
5150.0000 5200.0000	.428 ~162.1 .433 ~162.5		39.8	.773 .768	-38.1 -39.9		-162.4 -162.6
5250.0000	.448 -163.4		41.5	.762	-41.4		-163.4
5300.0000	.470 -164.3		42.8	.749	-42.8		-164.1
5350.0000		•	44.6	.746	-44.5	. 492	-165.0
5400.0000	.508 -165.3	•	45.9	.744	-45.9		-165.3
5450.0000	.528 -163.4		47.5	.729	-47.4		-163.5
5500.0000 5550.0000	.538 -162.0 .545 -162.1		·48.7 ·48.3	.700 .673	-48.7 -48.2		-162.1 -162.1
5600.0000	.555 -162.3		48.1	.643	-48.1		-162.4
5650.0000	.560 -163.6		48.6	.630	-48.6		-163.7
5700.0000	.574 -164.0	.611 -	48.5	.611	-48.4	.574	-164.1
5750.0000	.586 -164.4	•	49.2	.587	-49.3		-164.5
5800.0000	.598 -165.2		49.7	.570	-49.5		-165.3
5850.0000	.6:2 -166.8		50.9	. 559	-50.9		-166.9
5900.0000 5950.0000	.622 -170.0 .631 -173.1		·52.8 ·53.5	.543 .526	-52.7 -53.5		-170.1 -173.0
6000.0000	.643 -174.7		·53.1	.509	-53.1		-174.7
6950.0000	.652 -174.9		52.8	.490	-52.8		-174.9
6100.0000	.663 -175.1		52.4	.482	-52.3		-175.2
6150.0000	.677 -176.1	.470 -	52.3	.470	-52.2		-176.3
6200.0000	.684 -177.3		52.5	. 449	-52.4		-177.4
6250.0000	.691 -178.6		-52.2	.434	-52.1		-178.8
6309.000 <b>0</b> 6350.0000	.698 179.9		-51.8 -51.9	.416 .401	-51.8 -52.0	.698	179.9
6400.0000	.700 178.6 .707 176.9		-51.4	.385	-51.4	.700 .707	178.4 176.8
6450.0000	.7.5 174.6		-50.5	.365	-50.3	.715	174.5
6500.0000			-49.3	.350	-49.3	.721	172.6
6550.0000	.728 171.5		-48.2	.335	-48.2	.730	171.5
- 6600.0000			-48.0	.317	-47.8	.732	170.1
6650.0000			-47.6	.299	-47.5	.741	167.5
6700.0000 6750.0000			-45.9 -44.4	.281 .265	-45.9	.745	165.1
6800.0000			-42.9	. 253	-44.3 -42.7	.749 .759	163.5 163.2
6850.0000			-41.2	.238	-41.2	.773	162.6
6980.0000			-37.4	. 221	-37.2	.774	162.5
6950.000 <b>0</b>	.784 161.5	.211 -	-32.7	.211	-32.6	.784	161.5
7000.0000			-27.2	. 203	-27.1	.786	
7050.0000			-21.7	. 196	-21.7	.786	
7100.0000			-15.3 -8.6	. 193	-15.3 -8.5	.789	
7150.0000 7200.0000		.189 .193	-1.1	.189 .193	-1.0	.782 .790	161.3 163.0
7250.0000		.199	3.9	. 199	4.0	.790	162.2
7300.0000		.208	9.7	.208	9.7	.778	161.8
7350.0000		.220	14.4	.220	14.5	.789	160.5
7400.0000		.231	17.4	.231	17,5	.772	161.0
7450.0000		.252	21.3	. 252	21.3	.766	161.5
7500.0000		.271	20.6	.271	20.7	.753	158.1
7550.0000 7600.0000		.286 .309	21.5	.286 .309	21.6	.717 .709	155.8 152.2
7650.0000		.325	21.6	.325	21.6	.678	
7700.0000		.348	21.6	.348	21.6	.676	148.1
.7750.0000		.375		-27.375	19.4	.678	
78 <b>00.0000</b>	.667 140.5	.373	18.8	.373	18.9	.667	140.4

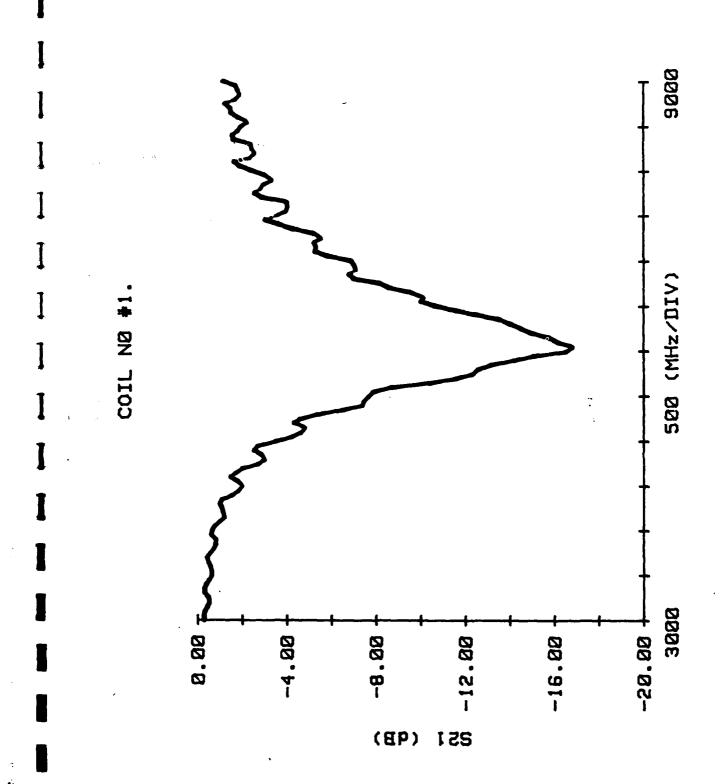
7850.0000	. 489	136.4	. 392	16.7	.392	16.7	.691	136.3
7900.0000		132.0	.396	16.7	.396	16.8	.687	132.0
7950.0000		130.3	.398	16,5	.399	16.5	.704	130.4
8000.0000		127.2	.403	15.7	.403	15.8	.715	127.2
3050.0000		125.0	.394	16.6	.395	16.6	.720	125.0
3100.0000		124.1	.407	18.7	.407	18.7	.751	124.2
8130.0000		122.5	.413	19.2	413	19.4	.756	122.4
8200.0000		125.1	.430	22.1	.430	22.2	. 775	125.0
8250.0000		125.5	.442	22.2	.442	22.3	.794	125.4
8300.0000		125.9	.453	22.1	.453	22.2	.777	125.9
8350.0000		123.8	.471	22.5	.471	22.4	.783	123.7
8400.0000	.768	123.3	. 482	19.0	. 482	19.0	.768	123.2
8450.0000	.746	124.3	.482	18.8	.482	18.8	.746	124.3
8500.0000	739	125.4	.483	16.7	.483	16.9	.739	125.3
8550.0000	.7:3	125.8	.483	16.7	.483	16.9	.712	125.9
8600.0000	.709	124.5	.489	16.9	.489	17.0	.709	124.5
8650.0000	. 693	121.9	.498	16.1	.498	16.2	.693	121.9
8700.0000	696	120.1	. 495	17.2	. 495	17.3	.696	120.1
8750.0000	697	120.6	.507	17.4	.507	17.5	. 697	120.5
8800.0000	.688	121.3	.505	18.3	.505	18.5	.688	121.2
8850.0000	.684	120.4	.518	18.0	.518	18.0	.684	120.3
8900.0000	.678	118.6	.524	18.4	.524	18.4	.678	118.6
8950.0000	.682	117.8	.519	18.6	.519	18.7	.682	117.8
9000.0000	.675	117.0	.536	18.9	.536	18.9	.673	116.9
9050.0000	.679	117.4	.540	18.8	.540	18.7	. <del>6</del> 79	117.4
9100.0000	.675	117.8	.557	18.4	.557	18.5	. 675	117.7
9150.0000	.667	116.8	.557	17.7	.559	17.7	.667	116.7
9200.0000	. 661	115.1	.567	17.9	.567	17.8	.661	115.0
9250.0000	. 656	113.9	.573	18.3	.572	18.3	. 656	113.8
9300.0000	.651	113.8	.584	18.1	. 584	18.0	.651	113.7
9350.0000	.645	113.6	.591	17.7	.591	17.8	.644	113.6
9400.0000	.643	112.9	.595	17.5	. 595	17.5	.643	112.9
9450.0000	.640	112.0	. 595	16.5	.595	16.6	. 640	111.9
9500.0000	.639	111.4	.607	15.9	.607	15.9	.639	111.3
9550.0000	.641	110.9	.610	15.3	.610	15.3	.642	110.8
9600.0000	.639	110.7	.614	15.0	.614	15.1	. 639	110.6
9650.0000	.637	109.3	.610	14.6	.610	14.6	.637	109.3
9700.0000	.633	107.3	.617	15.3	.617	15.3	.633	107.2
9750.0000	.634	106.1	.627	15.2	.627	15.1	.634	106.1
9800.0000	.634	106.3	.636	14.9	. 636	15.0	.634	106.2
9850.0000	.634	107.5	.636	14.7	. 636	14.7	.634	107.4
9900.0000	.633	107.8	.637	13.8	.637	13.8	.633	107.7
9950.0000	. 628	106.4	.642	13.6	.642	13.7	.628	106.3
10000.0000	.630	106.1	.643	13.1	.643	13.0	.630	106.1

INPUT REF = 4.74 CM OUTPUT REF = 4.74 CM



	FL COEFF -IN	L055-F0	RWARD L	OSS-REVE	RSE REF	L COEFF -OUT
FREQUENCY REF		MAG	ANG	MAG	ANG	MAG ANG
MHz	MAG ANG	nna	HIIG		. = .	.111 -104.4
0000 0000	.110 -104.3	.974	-17.1	• • • •	-17.0	.111 -106.0
3000.0000	.110 -105.		-18.3		-18.3	.111 -107.8
3050.0000	.111 -107.	972	-19.4		-19.6	.114 -109.9
3100.0000	.114 -110.	958	-19.8		-19.9	.117 -111.9
3150.0000	.116 -112.	-	-19.0		~18.9	117 -113.9
3200.0000	.116 -114.		-19.0	-	~18.9	.119 -115.6
3250.0000	.118 -115.	5 .973	-19.8		-19.7	.125 -117.6
3300.0000	.125 -117.	6 .974	-20.9		-20.8	130 -120.0
3350.0000	.129 -119.	9 .963	-22.7		-22.6	.132 -122.1
3400.0000	.132 -122.	2 .947	-23.3	.947	-23.2	.136 -124.2
3450.0000	.135 -124.	1 .938	-23.1	.936	-23.1	.142 -125.6
3500.0000	.142 -125.	5 .938	-23.0	, 936	-22.9	151 -126.9
3550.0000	.151 -126.	9 .944	-23.1	.941	-23.1	.160 -129.3
3600.0000	.160 -129.	4 .955	-24.1	,952	-24.0	,165 -131.3
3650.0000	.164 -131.	3 .960	-25.4	.959	-25.3	.170 -133.1
3700.0000	169 -133.	1 .941	-27.5	.936	-27.4	181 -134.5
3750.0000	.181 -134	5 .924	-28.3	.923	-28.2	.194 -134.5
3800.0000	.193 -134	6 .914	-27.2	.913	-27.1	.203 -136.8
3850.0000	.203 -136	8 .916	-26.4	.915	-26.4	.211 -139.3
3900.0000	.211 -139	. 939		.938	-27.7	.222 -139.9
3950.0000	.222 -139	,8.934		.934	-30.1	.237 -139.7
4000.0000	.237 -139	.g .922		.919	-32.6	253 -141.6
4959.8888	.253 -141	.6 .897	-32.9	.896	-32.8	268 -142.7
4100.0000	.268 -142	.7 .873		.871	-32.8	.277 -144.2
4150.0000	.276 -144	.3 .882	-31.7	.881	-31.5	293 -145.8
4200.0000 4250.0000	.292 -145	.8 .887		.885	-31.9	.313 -145.7
4300.0000	,313 -145	.8 .899		.897	-34.3	330 -147.0
4358.0000	.330 -147	.9 .886		.883	-37.4 -39.8	.343 -149.2
4400.0000	.343 -149	.2 .838		.839		360 -149.5
4450.0000	.359 -149	.4 .809	-40.1	.807	-40.2 -38.8	.378 -151.2
4500.0000	.378 -151	.2 .79		.792	-39.3	405 -152.0
4550.0000	.405 -152	.0 .81		.818	-39.6	:423 -153.4
4600.0000	.422 -153	3,4 .85		.849	-44.3	.436 -154.7
4658.8000	.435 -154	1.7 .82		.822	-47.0	.458 -156.2
4700.0000	.457 ~156	5.1 .79		.797	-46.6	.482 -157.7
4750.0000	.481 -15	7.7 .73		.729		.504 -159.1
4800.0000	.503 -15	9.1 .70	7 ~45.6	.703 .724	-44.6	.519 -160.5
4850.0000	.517 -16	0.6 .72	2 -44.7	.749		.532 -161.4
4900.0000	.531 -16	1.3 .75	2 -46.2	.735		.556 -163.3
4950.0000	.555 -16	3,3 .73		.668		.590 -165.1
5000.0000	.589 -16	5.1 .66		.612		.608 -166.5
5050.0000	.607 -16	6.5 .61		.582		.617 -167.9
5100.0000	.615 -16	7.9 .58		.573	_	.640 -170.1
5150.0000	.638 -17	0.0 .57		.612		.663 -172.0
5200.0000	.661 -17	1.9 .61		.598		.680 -172.9
5250.0000	.677 -17	2.8 .59				.697 -175.0
5300.0000	.696 -17	4.9 .5		.474		.713 -177.1
5350.0000	.713 -17	7.1 .4				.731 -179.0
5480.0000	.734 -17	9.9 .43 80.0 .43	_			.746 180.0
5450.0000						.761 178.5
5500.0000						.775 176.0
5550.0000						.787 174.0
5600.0000	.784	74.1 .3	02 -F1.4		2 -61.4	.795 173.3
5650.0000	.795	_	64 -57.7			.809 172.0
5780.0000	,807 1		42 -52.9			.817 169.7
5750.0000	.815		35 -48.4			.822 167.7
5800.0000	, 823		20 -47.5		·	.831 166.4
5850.0000	.827 1		96 -47	·	7 -47.4	.834 165.0
5963.0000	,832 1		77 -48.4		• .	.839 163.5
5950.0000	,841 1		49 -25.			.841 161.8
6000.0000	.838 1	61.8 .1	, -, -	B-30		
				-		

						4	040	1/0 7
6050.0000	.842	160.8	.144	-16.0	. 144	-15.9	.843	160.7
6100.0000	.842	159.4	. 157	-2.4	. 158	-1.9	.843	159.4
6150.0000	.840	158.1	. 165	6.0	.165	6.1	. 848	158.0
6200.0000	.842	156.8	.181	8.8	. 181	8.9	.845	156.7
6250.0000	.842	155.6	.198	13.3	. 198	13.4	.842	155.6
			.201	19.9	.201	19.9	.845	154.0
6300.0000	.838	154.1			.213	28.5	.836	152.8
€750.0000	.835	152.7	.213	28.3				
6400.0000	.834	152.3	. 23 <del>9</del>	34.4	.239	34.8	.831	152.3
6450.0000	.829	151.2	.266	35.7	. 266	35.8	.832	151.1
6500.0000	.822	149.8	.296	32.6	. 295	32.8	.824	149.8
6550.0000	.814	148.6	.319	30.6	.319	30.8	.818	148.5
6600.0000	.809	148.3	.313	31.6	.313	31.8	.813	148.2
-	.805	147.5	.335	32.0	.334	32.2	.807	147.5
6650.0000			.375	38.5	.375	38.6	,800	145.8
6760.0060	.796	145.9			.395	41.3	.790	144.5
6750.0000	.791	144.6	.394	41.1				
6800.0000	.779	143.9	.450	36.8	.451	37.0	.783	143.8
6850.0000	.776	143.7	.462	35.3	.461	35.5	.778	143.7
6900.0000	.763	142.7	.444	32.5	,444	32.7	.765	142.7
6950.0000	.751	141.5	. 449	34.4	.449	34.6	.752	141.4
7000.0000	.747	141.0	. 456	37.1	. 455	37.2	.748	140.9
7050.0000	735	140.5	.514	37.2	.513	37.5	.735	140.5
		139.2	549	37.0	.547	37.2	. 725	139.1
7190.0000	.723		.546	30.2	.545	30.5	.718	137.9
7150.0000	.718	138.1			.554	27.8	.703	137.6
7200.0000	.703	137.6	.552	27.5			.698	136.5
7250.0000	. 699	136.6	.529	30.1	.528	30.0		136.2
7300.0000	.688	136.0	.552	30.8	.552	30.9	.691	
7350.0୧୯୦	.672	135.2	.617	34.1	.617	34.3	.671	135.1
7400.0000	.653	134.2	.664	32.2	.664	32.4	.654	134.2
7450.0000	.648	134.2	.710	27.1	.711	27.4	. 653	134.0
7500.0000	.642	133.4	.664	25.3	.663	25.5	.642	133.3
7550.0000	.63	131.7	.632	23.6	. 633	23.7	.633	131.7
7600.0000	.620	130.9	.629	28.9	.630	29.0	.621	130.7
7650.0000	.602	129.3	.632	30.7	.634	30.9	.605	129.3
		129.0	.723	29.3	.722	29.4	.598	128.9
7700.0000	.595		.750	27.7	.749	27.8	.583	129.0
7750.0000	.583	129.0			.722	21.1	.577	127.7
7800.0000	.575	127.8	.723	20.8		18.6	.571	125.3
7850.0000	.569	125.3	.713	18.4	.713			
7900.0000	.557	125.3	.681	21.6	.681	21.8	.557	125.1
7950.0000	.535	124.3	.710	22.9	.710	23.2	.536	124.3
8000.0000	.532	124.1	.760	25.2	.760	25.5	.532	124.0
8050.0000	.530	122.9	.809	21.4	.811	21.7	.532	122.7
8100.0000	.520	120.6	.834	19.2	.833	19.5	.522	120.4
8150.0000	.506		.759	17.8	.758	18.0	.507	119.1
8200.0000	.492	119.7	.743	17.8	.745	17.3	.490	119.7
		118.9	.760	21.5	.758	21.6	.480	118.9
8250.0000	.479			21.8	.761	22.0	.485	117.8
8300.0000	.485	117.2	.764	19.6	.832	18.8	.477	116.1
8350.0000	.477	116.2	.835			16.5	.459	114.7
8403.0000	.459	114.6	.841	16.3	.839			112.9
8450.0000	. 453	113.0	.814	13.0	.816	13.3	. 454	
8500.0000	. 447	112.0	.800	13.7	.799	13.8	.448	111.9
8550.0000	.439	111.3	.773	14.9	.771	15.1	.448	111.2
8600.0000	.440	110.0	.818	15.9	.818	16.1	.442	109.8
8650.0000	.437	109.4	.846	17.2	.845	17.5	.437	109.4
8700.0000	. 425	107.5	.849	13.5	.849	13.9	. 424	107.4
8750.0000	. 421	106.5	.872	12.1	.873	12.2	.423	106.5
	.414	106.7	.822	11.3	.823	11.6	.415	106.3
8800.0000		105.2	. 804	11.2	.883	11.3	.410	105.1
8850.0000	.408			12.3	.814	12.5	,412	103.6
9900.0000	.412	103.6	.815		.823	12.1	.404	102.8
8950.0000	.404	102.9	.824	11.7			.392	101.4
9000.0000	.392	101.5	.883	10.8	.881	11.0	. 372	

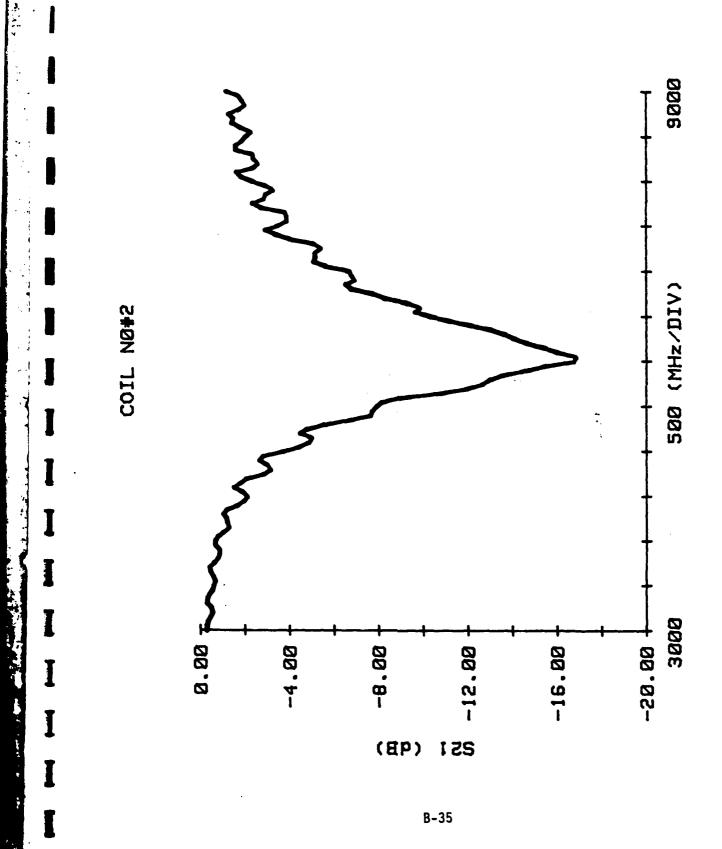


B-32

FREQUENCY	REFL COEFF -IN	LOSS-FORWARD	LOSS-REVERSE	REFL COEFF -OUT
MHz	MAG ANG	MAG ANG	MAG ANG	MAG ANG
3000.0000	.119 ~104.9	.975 -18.	1 .970 -18.1	.120 -105.0
3050.0000		.973 -19.		.120 -106.9
3100.0000	.121 -108.6	.968 -20.	8 .968 -20.9	.121 -108.8
3150.0000	.124 -111.0	.956 -21.		
3200.0000	.127 -113.2	.946 -20.		
3250.0000	.127 -115.4	.952 -20.		
3300.0000		.975 -21.		
3350.0000		.972 -22.		
3400.0000		.960 -24.		
3450.0000		.944 -24. .938 -24.		
3500.0000		.938 -24. .933 -24.		
3550.0000 3600.0000		.943 -24.		
3650.0000		.955 -25.		
3700.0000		.959 -26.		
3750.0000		.937 -29.		
3800.0000		.919 -30.		.198 -136.9
3850.0000	.211 -136.8	.912 -28.	7 .910 -28.7	.212 -136.7
3900.0000	.221 -139.1	.911 -28.		
3950.0000		.935 -29.		
4000.0000		.932 -31.		
4050.0000		.920 -34.	-	
4100.0000		.892 -34.		
4150.0000		.866 -34.		
4200.0000		.876 -33. .880 -33.		
4250.0000 4300.0000		.893 -36.		
4350.0000		.878 -39.		
4400.0000		.831 -41.		
4450.0000		.800 -42.		
4500.0000		.787 -40.	5 .788 -40.5	.397 -153.5
4550.0000		.810 -41.		.425 -154.5
4600.0000	.442 -155.7	.846 -41.		
4650.0000		.816 -46.		
4700.0000		.790 -49.		
4750.0000		.722 -48.		
4800.0000		.697 -47.	_	
4850.0000		.713 -46. .741 -47.		
4900.0000 4950.0000		.727 -52.		
5000.0000		.655 -56.		
5050.0000		.601 -57.		
5100.0000		.571 ~53.		
5150.0000		.562 -53.	9 .564 -53.9	.653 -171.9
5200.0000	.676 -173.7	.601 -56.	0 .601 -56.1	
5250.0000		.578 -60.		
5300.0000		.527 -64.		
5350.0000		.463 -63.		
5400.0000		.415 -61.		
5450.0000		.412 -59.		
5500.0000		.403 -57. .392 -63.		
5550.0000 5600.0000		.392 -63. .354 -63.		
5650.0000		.290 -62.		
5700.0000		.253 -58.		
- 5750.0000		.233 -53.		
5800.0000		.225 -48.		
5850.0000		.210 -47.		
5900.0000		.187 -46.		2 .840 163.9
5950.0000		170 -38.	2 .169 -38.0	
6000.0000	.843 160.8	.146 -23.	2 <sub>B-33</sub> .146 -23.6	846 150.8
			0-33	

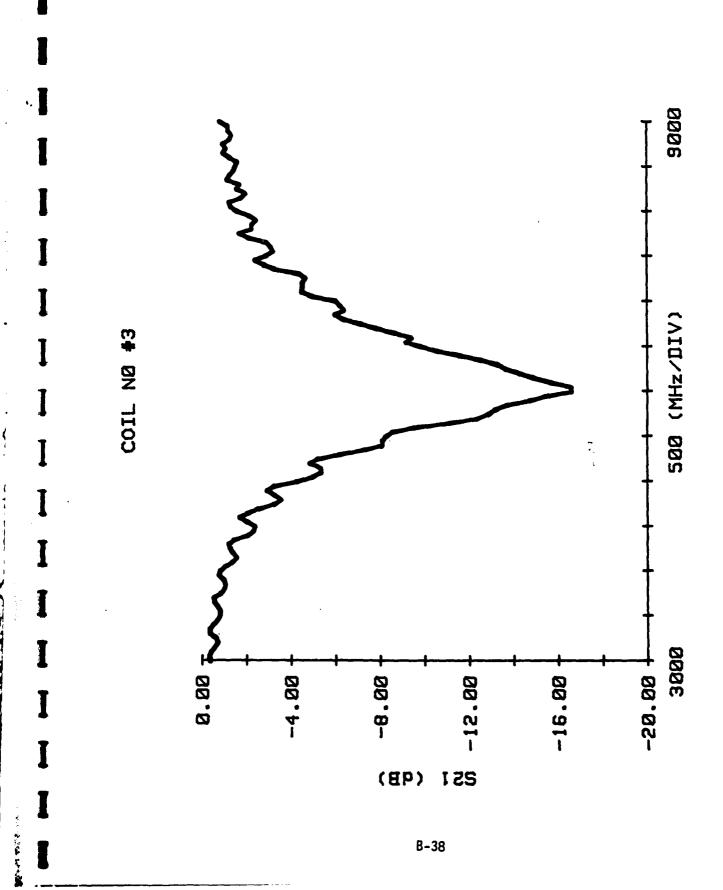
- 6050.0000	.845 159.7	. 144	-12.8	.144	-12.4	.848	159.7
6100.0000	.845 158.5	.160	. 1	.160	. 4	.847	158.5
6150.0000	.843 157.2	.171	8.2	. 172	8.4	.845	157.2
6200.0000	.844 155.9	.:37	10.4	.187	10.4	.846	155.7
6250.0000	.845 154.8	.199	14.2	.199	14.2	.843	154.7
6300,0000	.843 153.3	.210	20.3	. 209	20.3	.844	153.3
6350.0000	.833 151.9	.225	28.2	. 226	28.3	.834	151.8
6460.0000	.830 151.5	.251	33.9	. 252	34.1	.832	151.5
6450.0000							
		.280	34.7	. 281	34.7	.832	150.4
6500.0000	.819 149.2	.308	31.1	.308	31.2	.825	149.1
6550.0000	.812 148.0	.332	28.9	.332	29.0	.815	147.9
6600.0000	.807 147.6	.323	30.2	.323	30.1	.808	147.6
6650.0000	.804 147.0	.347	30.4	.347	30.4	.804	146.8
6700.0000	.796 145.3	.389	36.5	.388	36.6	.797	145.2
6750.0000	.789 144.2	.414	38.6	.413	38.7	.788	143.9
6800.0000	.778 143.4	.461	34.4	.461	34.5	. 779	143.2
6850.0000	.770 143.2	.475	32.3	.475	32.3	.772	143.1
6900.0000	.761 142.3	. 452	30.5	.452	30.6	.758	142.1
6950.0000	.748 141.0	.460	32.0	.459	32.1	.749	141.0
7000.0000	.743 140.5	.467	34.9	.466	35.0	.744	140.4
7050.0000	.731 140.2	.527	34.6	.527	34.7	.734	140.0
7100.0000	.723 138.9	.560	34.0	.561	34.1	.721	138.7
7150.0000	.714 137.8	.555	27.7	.555	27.8	.716	137.7
7200.0000	.702 137.4	.556	25.1	.556	25.2	.702	137.1
7250.0000	.695 136.4	.538	27.7	.538	27.8	.696	
		.561	28.7				136.2 135.8
7300.0000	.685 135.8			.561	28.7	.685	
7350.0000	.669 135.0	.633	30.9	.634	31.0	.669	134.9
7400.0000	.648 134.1	.678	29.1	.675	29.2	.651	133.8
7450.0000	.650 133.9	.718	23.4	.718	23.5	.650	133.7
7500.0000	.641 133.2	.671	22.3	.668	22.3	.638	133.1
7550.0000	.630 131.5	.640	21.1	.638	21.1	.629	131.3
7600.0000	.615 130.6	.642	<b>26.1</b>	.642	26.1	.616	130.5
7650.0000	.597 129.3	.649	28.2	.648	28.3	. 599	129.0
7700.0000	.594 128.8	.733	25.9	.735	25.9	. 596	128.5
7750.0000	.581 128.9	.766	24.1	.765	24.0	. 584	128.6
7800.0900	.576 127.6	.721	17.7	.722	17.8	. 574	127.3
7850.0000	.568 125.0	.716	15.3	.716	15.3	.567	124.8
7900.0000	.556 124.6	.686	19.3	.686	19.2	.556	124.6
7950.0000	.535 124.0	.719	19.9	.721	19.9	.535	123.8
8000.0000	.532 123.6	.773	22.1	.771	22.2	.533	123.4
8050.0000	.532 122.1	.815	17.6	.817	17.8	.532	121.9
8190.0000	.522 119.8	.834	15.5	.836	15.5	.522	119.6
8150.0000	.507 118.5	.761	14.3	.760	14.6	.507	118.2
8200.0000	.494 119.0	.741	14.1	.740	14.1	.494	118.9
8250.0000	.482 118.4	.764	18.2	.767	18.3	.483	118.1
8300.0000	.488 116.1	.767	18.7	.765	18.8	.490	115.9
8350.0000	.483 114.9	.837	14.9	.836	14.9	.484	114.7
8400.0000	.460 113.7	.835	12.7	.835	12.8	.462	113.3
8450.0000	.456 111.8	.808	9.5	.806	9.6	.456	111.5
8500.0000	.453 111.0	.792	10.8	.793	10.8	. 454	110.6
1550.0000	.446 110.2	.770	11.8	.769	11.9	.445	109.6
5500.0000	.448 108.5	.816	12.8	.816	12.9	.448	108.2
8650.0000	.444 107.6	.851	14.0	.849	14.0	. 447	107.3
8700.0000	.433 105.9	.846	10.3	.847	10.3	.434	105.7
8750.0000	.430 105.2	.867	8.5	.868	8.7	.430	104.7
8880.0000	.425 104.7	.818	8.5	.817	8.5	.427	104.5
8850.0000	.419 103.4	.795	8.1	.797	8.2	.420	103.1
8900.0000	.423 101.6	.809	9.6	.809	9.5	.424	101.5
8950.0000	.415 101.0	.822	8.7	.821	8.8	.415	100.6
9000.0000	.403 99.5	.877	7.5	.881	7.5	.403	99.1
	• •		-			= =	

INPUT REF = 4.74 CM OUTPUT REF = 4.74 CM



FREQUENCY	REFL COEFF -IN	LOSS-FORW	ARD	LOSS-REV	ERSE	REFL	COEFF	-out
MHz	MAG ANG	MAG	ANG	MAG	ANG	MA	G	ANG
3000.0000	.172 -114.1	.965 -	20.3	. 966	-20.2	. 1	74 -1	14.2
3050.0000	.172 -114.9		22.1		-22.0	. 1	74 -1	115.2
3100.0000	.175 -115.5	.962 -	23.6	.961	-23.6	. 1	76 -1	115.8
3150.0000	.181 -116.5	.944 -	23.8		-23.9			116.6
3200.0000	.186 -117.4	.928 -	22.5		-22.5			117.1
3250.0000	.185 -118.6	.937 -	22.3		-22.4			113.2
3300.0000	.189 -118.9		23.3		-23.3			118.7
3350.0090	.197 -120.1		24.6		-24.7			119.7
3400.0000	.203 -121.1		27.1		-27.1			120.9
3450.0000	.206 -122.3		27.6		-27.7			122.2
3500.0000			27.1 26.7		~27.2 ~26.6			123.5
3550,0000			26.7		-26.7			124.2
3600.0000 3650.0000			28.2		-28.3			125.7
3700.0000			30.1		-30.1			126.7
3750.0000			32.4		-32.3			127.4
3800.0000			33.1		-33.0	. 2	62 -1	128.6
3850.0000			31.2	.889	-31.2			128.7
3900.0000		.899 -	30.3	.899	-30.3			130.3
3950.0000	.288 -132.4		31.9		-31.8			132.5
4000.0000			-35.2		-35.1			132.9
4050.0000			37.7		-37.7			132.5
4100.0000			38.0		-38.0			133.9
4150.0000			-37.1		-37.1			135.4 136.7
4200.0000			-35.8 -36.1		-35.9 -36.1			138.0
4250.0000			-39.6		-39.6			137.9
4300.0000 4350.0000			-42.7		-42.8			139.2
4400.0000			-44.7		-44.8			141.4
4450.0000			-44.8		~43.8			142.0
4500.0000			-42.8		-43.0	. 4	51 -:	143.2
4550.0000		.794 -	-43.6	.795	-43.6			144.2
4600.0000	.491 -145.9		-45.1		-45.1			145.9
4650.0000			-49.5	.791	-49.5			147.0
4700.0000			-52.3	.746	-52.3			148.7
4750.0000			-50.8	.689	-50.9			150.1
4800.0000			-48.7 -48.7	.662 .698	-49.0 -48.7			151.6 152.9
4850.0000			-40.7 -51.3	.716	-51.2			154.0
4900.0000 4950.0000			-55.8	.692	-55.9			155.8
5000.0000			-59.1	.614	-59.0			159.0
5050.0000			-59.4	.565	-59.4			159.2
5100.0000			-55.2	.541	-55.2			160.6
5150.0000		.543 -	-54.9	.544	-54.8			162.6
5200.0000			-57.9	.574	-58.1			164.6
5250.0000			-62.6	.549	-62.5			165.7
5300.0000			-66.1	.492	-66.0			167.6
5350.0000			-64.1	.432	-63.8 -61.3			169.8 171.7
5400.0000			-61.4 -58.4	.394 .394	-58.3			172.8
5450.0000			-58.1	.388	-58.1			174.4
5500.0000 5550.0000			-63.1	.374	-63.1			177.0
5600.0000			-64.1	.334	-64.8			178.9
5650.0000			-61.1	.278	-61.0			179.6
5700.0000			-56.8	.242	-56.7	. 8	14	179.0
- 5750.0000		.228 -	-51.3	.228	-51.1			176.4
5800.0000			-47.0	. 220	-47.0			174.4
5850.0000			-45.8	. 207	-45.0			173.1
5900.0000			-44.7	. 185	-44.4			171.6
5950.0000			-35.4	.170	-35.2			170.0
6000.0000	.837 168.0	.149	-20.7 <sub>B-</sub>	-36 .148	-20.4	. 5	335	100.0

					_9 7	. 158	-9.6	.840	166.8
	6350.0000		166.8	.149	-9.7	.166	1.9		165.4
	6190.0000		165.4	.166	1.7	.181	10.0	.835	163.9
	6150.0000		164.0	. 181	9.8	.195	11.3	.829	162.3
	6200.0000		162.4	. 195	11.1		14.4	.829	160.8
	6250.0000		161.0	.210	14.5	.210		.828	159.4
	6300.0000	.828	159.4	.219	20.7	.219	20.6	.817	157.9
	-6350.0000	.817	158.0	.239	27.9	. 239	27.8		157.3
	6400.0000	.814	157.3	. 265	33.5	. 267	33.5	.813	155.9
	6450.0000	.811	156.0	.298	33.9	.299	34.0	.814	154.4
	6500.0000		154.5	.324	29.8	.324	29.8	.800	153.0
	6550.0000		153.1	.350	27.9	.351	28.0	.789	152.6
	6600.0000	.782	152.6	.339	28.9	.339	29.0	.783	151.5
	6650.0000	.775	151.6	.371	29.3	.371	29.4	.773	149.7
	6700.0000	.765	149.7	.408	34.9	.409	34.9	.766	
	6750.0000	.753	148.5	.443	<b>36.5</b>	.444	36.5	. 755	148.4
	6800.0000	.742	147.6	.484	32.6	. 485	32.6	.742	147.5
	6850.0000	.732	147.2	.505	29.7	.506	29.8	.733	147.2
	6900.0000	717	146.1	.480	28.7	.481	28.8	.720	145.9
}	6950.0000	.703	144.5	. 492	29.8	. 491	29.8	.706	144.6
1		.696	144.0	.503	32.5	.503	32.5	.696	143.8
	7000.0000 7050.0000	.681	143.6	.566	31.6	.565	31.7	.681	143.5
	7100.0000	.668	141.9	.599	30.8	. 599	30.8	.668	141.9
	7150.0000	.657	140.8	.596	25.0	. 594	25.0	. 658	140.7
}		.643	140.4	.595	22.8	.594	22.8	.645	140.4
	7200.0000	.629	139.3	.587	24.8	.586	24.9	.629	139.3
•	7250.0000	.619	138.7	.607	25.7	.607	25.8	.619	138.7
	7300.0000	.598	137.9	. 688	26.4	.687	26.4	.598	138.0
•	7350.0000	.577	137.2	.727	24.8	.725	24.8	.578	137.4
	7400.0000	.573	136.7	.762	19.1	.760	19.2	.572	136.9
	7450.0000	.559	136.3	.718	18.6	.721	18.8	.561	136.2
	7500.0300		134.4	691	17.3	.693	17.3	.544	134.3
	7550.0000	.546	133.9	.702	21.2	.701	21.3	.528	133.8
_	7600.0000	.526	132.7	.717	22.8	.716	22.9	.509	132.8
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•	7700.0000	.503		.824	17.5	.825	17.6	. 493	132.7
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	7900.0000	.449	129.5	.783	13.4	.783	13.6	. 431	129.1
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•	8450.0000	.326	121.6	.848	4.8	.840	4.9	.322	121.0
	a500.0000	.322	120.9	.840	4.7	.830	4.8	.309	120.6
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1	8800.0000	.283		.865	2.4	.854	1.4	.280	
	8850.0000	.280		.856	1.2	.872	3.0	.279	
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APPENDIX C

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#### सर्भाष्ट्रमञ्जू ONE PREAMP estanss , 23 Hai 429 $\mathbb{F}[\mathbb{R}[\mathbb{R}]]$ SMHILL OHE 何つら BHS MAG ANG MAG भाषक 1 1 2 1 1 3 1 30 . 019 2000 000 - 93 .099 .651 - <del>- -</del> --199 42 2:00.000 -169 .013 **-** 0.6 -153 .6:3 . 51 . 11.3 2400.000 9.2 .014 191 -33 10.30 . 155 2300.000 -11 -169 .001 -137 .615 -93 .754 - 54 . . . . 3339.373 197 -118 .ស្ពុន 169 . 50 / 3 בים, כבוי ~ 1 j · 31 .533 -- 1 17 .005 132 . 354 3200.300 -133 1.034 .095 169 106 .597 -170 .351 3100.919 -1.512.136 36 .003 79 .516 151 4. 34 3609.339 .333 .093 179 -124 37 .505 100 . 737 3309.939 155 1.114 30 .006 74 .433 100 .706 .045 4000.000 117 31 .095 38 .325 7.9 .798 -6 4200.000 .673 នេះ -47 .629 51 .១១5 .546 3 <del>-</del> 5 4400.000 08 .560 -101 .003 -13 .592 -136 ~19 .5 5 4600.000 26 . 205 .ព្ទុន .765 .440 4999.000 33 122 .007 -52 .513 . 744 .403 5000.000 $\rightarrow 0$ 53 .097 -71 .475 .707 .376 .276 5390.000 -39 .429 -11 .007 -85 .647 5400.000 -69 . 111 ~71 .098 -102 5699.999 .551 -99 .406 -126.019 -131 .210 -69 5300.000 .421 -126 .499 172 -153 .009 .278 -81 . .292 6000,000 .280 -146.533 194 .039 -162 -105 6200.000 .206 -151 .544 29 .011 -176 . .275 -129 .588 6499,000 .133 -154-52 .015 162 . .250 -15% 66**99.**899 .210 -175.019 .754 -142 135 .234 170 5339.909 .156 147 .999 108 .023 95 .223 105 .071 -3 7000,000 147 .631 63 .017 .179 16 -70 7239.993 .934 136 .174 - - 47 .318 .916 54 7499.999 .030 27 .222 -97 42 .293 -90 .017 7500,009 .299 .339 .013 -45 -142 .021 25 .243 -123 7899,099 .299 .030 -35 150 .025 3 -153 • • કરેલ -51 74 30**33.**000 .030 .312 -17 .925 .កាក់ខ . 393 4 3230.303 ~79 .339 .029 -33 140 -52 3499.301 .130 -27 .137 -53 .033 .393 112 .109 .373 0400.300 -122 .043 .326 -77 -73 32 ივო**ი.**იიე .034 .212 -144 -36 .969 -97 .014 54 13.20 .110 2020.203 - 1 15 15 ~117 .039 -128 .3:3 2 13 176 929**0.**000 .100 .237 -154 166 .199 .385 -164 -0 .175 9499.309 .143 .116 .399 158 - 3 : 769**0.**000 197 .145 120 .424 -94 .126 129 29 0333.303 5.1 .112 .462 - 37 .127 ខូឲូ 0.2 10000.00 .139 -- 26 54 .503 .118 41 -114 19399.09 .177 .122 -113 35 .998 5 .555 .130 . 733 .602 .603 .603 (14)9.00 .972 - t 35 -4 -26 $\pm 1 \pm 4$ . . . . - 0.3 177 19399.09 1.4.5 .959 -38 10000.00 3.5 -- 24 .055 -44 .353 -67 -71 . 330 -34330.0: -1 / <del>1</del> / <del></del> .6 \ ; .5 ! · .332 -109 32.50 .112 -109 f +, t 1:130.23 -133 28. 3

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5590.00	.429 115	.223 -71	.251 -51	.374 63
16000,00	.153 -4	.365 157	.408 173	.191 -22
16500.00	.247 -18	.387 25	.445 34	.181 -76
17000.00	259 -96	.356 -/12	.029 -103	.335 -126
7599.00	.316 -164	.235 1მხ	.225 137	.566 145
୍ଟ୍ରପ୍ର ପ୍ର	.564 126	.160 6	.152 17	.679 42
<b>-</b> -				

REF PLANE EXT(CM): IN= .00, OUT= .00

.00 VOLTS,	.00 MA (M	EAS 1)	V D = 4 V	I=60MA/STAGE
FREQ	S 1 1	\$21	\$12	\$22
(MHZ)	MAG ANG	MAG ANG	MAG ANG	MAG ANG ,
2000.000	.578 57	.020 142	.003 -118	.515 -1
	.517 60	.061 125	.005 -135	.494 3
2200.000		.184 96	.006 176	.481 9
2400.000		.610 65	.005 119	.495 14
2600.000	.405 58		.002 60	.455 17
280 <b>0.0</b> 00	.353 52		.001 67	.416 31
3000.000	.236 54		.003 122	.382 51
3200.000	.222 110	5.668 ~148	.014 115	.516 69
3400.000	.625 106	3.925 137		.477 91
3600.000	.828 79	4.096 177		.546 93
3800.000	.423 50	7.013 100	.004 -35	• • • •
4000.000	.252 98	7.170 52	.003 -17	
4200.000	.375 123	5.739 1	.003 1	.651 107
4400.000	.466 128	5.726 -38	.004 10	.636 113
4600.000	.524 132	5.909 -72	.005 19	.620 122
4800.000	561 134	6.026 -99	.007 24	.610 133
5000.000	.573 137	6.150 -124	.010 27	.609 142
5200.000	.548 139	6.143 -148	.014 29	.574 148
5400.000	.478 143	5.660 -170	.019 25	.438 155
5600.000	370 160	5.220 170	.026 12	.247 ~157
	.440 -177	5.166 139	.025 -12	.567 -123
5800.000	.439 -174	5.228 113	.017 -21	.670 ~130
6000.000		5.257 94	.012 -5	.555 -125
6200.000	.359 -168 .265 -159	5.318 77	.010 21	.426 -110
6400.000	T.157 -150	5,309 55	.012 47	302 -87
6600.000		5.113 20	.020 61	.256 -22
6800.000	i.052 -67	4.817 -16	.026 18	.639 -22
7000.000		4.683 -31	.011 17	.457 -31
7200.000	199 -52	4.820 -50	009 51	.334 -22_
7400.000		5.041 -83	.010 70	.175 -16
7600.000	.037 165	5.074 -116	.012 72	.079 98
7800.000	113 117	4.903 -142	.011 71	.202 112
0000.000	, ,		.010 77	.200 113 2
8200.000	2 .095 133		.009 85	133 125
8400.000	097 151		.009 88	.081 -161
8600.000	.078 173		.008 93	.171 -130
8800.000	.054 -136		.007 117	.238 -124
9000.000	.082 -88		.009 146	.270 -126
9200.000	.135 -71	1.301 65 .754 43	.013 159	.273 -131
9400.000	.193 -73		.018 171	.273 -133
9600.000	<b></b> 261 -82	.335 26	.028 -177	.294 -130
9800.000	.371 -97	.072 17	.060 -176	.389 -117
10000.00	.550 -116	.093 162	100 -110	.683 -132
19200.00	.742 -140	.134 137	.102 129	.602 -139
19400.00	.813 -165	.109 147	.045 104	.580 -129
19600.00	.919 146	.051 -164	.078 123	
10800.00	.099 151	.198 -173	.016 147	.590 -114 .637 -98
11000.00	.092 -113	.190 176	.022 174	.653 -81
11200.00	.135 -59	.170 177	.027 -164	
11400.00	.225 -27	.163 -178	.036 -149	• • • •
11600.00	.304 -12	.155 -171	.044 -138	
11300.00	.331 1	.150 -164	.052 -130	.717 -26
12000.00	.276 20	.139 -152	.056 -121	.723 -6
12200.00	.278 64	.146 -138	.062 -108	.730 12
		C-8		

12400.00	.330 87	.158	-127	.073	-97	.704	30
12600.00	.319 108	.173	-116	.087	-86	.670	47
12800.00	.291 135	.189	-109	098	-80	.642	61
13000.00	.293 163	.200	-101	.104	-72	.613	72
13200.00	.306 -176	.215	-93	.112	-61	.575	80
13400.00	.312 -158	.232	-85	.123	-48	.533	86
13600.00	.314 -144	.258	-80	.150	-36	.467	91
13800.00	.323 -131	.279	-79	.188	-31	388	97
14000.00	.342 -123	.282	-79	.220	-32	.317	108
14200.00	.361 -119	.255	-80	.227	-35	.287	123
14400.00	.364 -117	.213	-78	.206	-36	.293	129
14600.00	.359 -116	.161	-68	.170	-31	.310	125
14800.00	.331 -118	.122	-46	.132	-13	.346	115
15000.00	.302 -123	.119	-12	.131	18	.388	105
15200.00	.296 -131	.162	13	.185	41	.412	99
15400.00	.291 -145	.227	21	.263	46	.377	97
15600.00	.225 -152	.278	23	.334	47	.292	104
15800.00	.140 -133	.321	28	.389	43	.212	119
16000.00	.117 -97	.371	26	.409	39	.149	139
16200.00	.124 -55		23	.434	37	.107	166
16400.00	163 -25	.404	21	.438	33	.064	-180
15600.00	· .192 -9	.411	19	.441	28	.030	57
16800.00	159 17	.402	15	.395	19	.174	38
17000.00	.184 65	.345	8	.284	17	.301	36
17200.00	.258 88	.255	10	.222	26	.427	41
17400.00	.259 107	.230	28	.206	45	.520	45
17600.00	.304 139	.238	31	.224	48	.581	54
17800.00	.429 160	.214	31	.202	45	.645	65
18000.00	.571 171	.163	35	.147	48	.670	78

REF PLANE EXT(CM): IN=10.92, OUT=10.92

.00 YOLT	s, .00	MA (MEAS	1)		VD=3 ID=5	5MA/STAGE
FREQ	GA MAX	GU MAX	\$21	\$12	K	U
(MHZ)	DB	DB	DB	DB	MAG	MAG
2000.000	-34.43	-34.43	-37.45	-50.32	999.90	.00
2200.000	-26.54	-26.54	-29.01	-45.40	999.90	.00
2400.000	-17.84	-17.84	-19.94	-43.44	455.46	.00
2600.000	-9.03	-9.03	-10.86	-46.22	234.56	.00
2800.000	-1.28	-1.28	-2.73	-51.00	174.07	.00.
3000.000	4.09	4.09	3.67	-58.08	222.36	.00
3200.000	7.40	7.41	6.68	-50.27	64.03	.00
3400.000	8.18	8.04	5.13	-33.76	6.73	.02
3600.000	11.22	10.71	3.61	-38.32	4.77	.05
3800.000	12.43	12.41	9.75	-45.95	17.41	.01
4000.000	12.36	12.38	10.27	-51.05	33.79	.00
4200.000	11.53	11.56	9.17	-50.72	34.69	.00
4400.000	12.18	12.19	9.61	-49.34	26.83	.00
4600.000	12.67	12.63	9.92	-47.46	20.04	.01 .01
4800.000	12.90	12.82	10.05	-45.34 -43.27	15.11 12.30	.01
5000.000	12.74	12.67 12.07	10.02 9.78	-43.27 -40.67	10.31	.01
5200.000 5400.000	12.09 10.57	10.62	8.90	-38.34	10.12	.01
5600.000	9.62	9.68	8.10	-36.11	8.88	.01
5800.000	9.91	9.84	7.53	-35.63	7.37	.02
6000.000	9.48	9.38	7.23	-37.45	9.70	.01
6200.000	8.40	8.36	_6.85	-39.26	14.61	.00
6400.000	7.60	7.59	6.55	-39.45	17.34	.00
6600.000	6.87	6.88	6.00	-37.88	16.08	.00
6800.000	6.32	6.33	5.03	-34.89	11.58	.00
7000.000	5.03	5.01	3.65	-35.86	14.85	.00
7200.000	3.98	3.97	3.20	-39.41	26.99	.00
7400.000	3.38	3.38	2.91	-38.64	27.44	.00
7600.000	3.12	3.12	2.66	-38.08	26.55	.00
7800.000	2.43	2.44	1.92	-39.13	32.24	.00
8000.000	1.14	1.14	.68	-40.22	42.67	.00
8200.000	-3.48	-3.47	-3.89	-40.23	73.08	.00 .00
8400.000	-4.88	-4.88	-5.27 -6.73	-39.31 -37.97	77.44 77.91	.00
8600.000	-6.30 -8.31	-6.30 -8.31	-6.72 -8.79	-37.14	88.55	.00
3890.000 9000.000	-10.57	-10.57	-11.13	-36.49	105.61	.00
9200.000	-13.40	-13.40	-14.02	-35.61	131.41	.00
9400.000	-16.93	-16.93	-17.64	-34.38	169.42	.00
9690.000	-22.32	-22.32	-23.22	-32.79	256.79	.00
9800.000	-31.97	-31.97	-33.24	-30.51	575.01	.00
10000.00	-18.48	-18.47	-20.67	-23.80	50.47	.00
10200.00	-13.04	~12.86	-18.33	-19.04	10.94	.02
10400.00	-17.62	-17.58	-22.43	-24.76	37.80	.01
10600.00	-26.20	-26.21	-29.03	-19.61	70.40	.00
10800.00	-14.30	-14.30	-16.24	-34.01	104.15	.00
11000.00	-14.40	-14.40	-16.72	-29.72	61.50	.00
11290.00	-14.60	-14.59	-17.11	-27.60	48.21 34.57	.00 .00
11400.00	-14.07	-14.06	-17.03	-25.68 -34.33	34.57 26.95	.00
11600.00	-13.61	-13.62 -13.89	-16.92 -17.38	-24.32 -23.24	23.94	.01
11890.00 12000.00	-13.87 -14.59	-13.89	-17.38	-23.24	24.89	.01
12200.00	-14.94	-14.98	-18.37	-22.11	24.00	.00

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12400.00	.329	82	.130	-135	.085	-122	.679	30
12600.00	.345	108	.140	-123	.091	-112	.654	47
12300.00	.345	128	.149	-114	.097	-102	.632	61
13000.00	.313	149	.160	-102	.102	-90	.606	72
13200.00	.293	173	.182	-92	.114	-76	.571	80
13400.00	.295	-165	.211	-85	.132	-65	.532	87
13600.00	.317	-150	.234	-82	.158	-57	.478	94
13800.00	.331	-139	.251	-81	.182	-54	.429	101
14000.00	.346	-132	.251	-81	.198	-52	.389	109
14200.00	.356	-127	.234	-81	.201	-52	.357	115
14400.00	.356	-124	.204	-79	.186	-51	.338	118
14600.00	.349	-122	.165	-75	.157	-46	.337	115
14800.00	.317	-123	.114	-62	.121	-31	.367	107
15000.00	.285	-127	.087	-25	.109	2	.407	100
15200.00	.277	-135	.124	13	.158	30	.424	96
15400.00	.260	-151	.200	20	.234	34	.386	97
15600.00	.176	-160	.244	16	.293	33	.300	105
15800.00	.063	-110	.244	20	.340	30	.226	122
16000.00	.137	-57	.291	24	.354	28	.172	141
16200.00	.191	-41	.322	23	.381	26	.136	160
16400.00	.215	-25	.332	19	.387	23	.081	166
16600.00	232	-10	.334	18	.394	18	.046	72
16300 <b>.00</b>	.200	15	.327	15	.355	9	.170	37
17000.00	.205	54	.286	1 1	.254	7	.293	40
17200.00	.245	82	.228	14	.199	19	.432	43
17400.00	.265	108	.217	27	.202	35	.522	46
17600.00	.316	135	.222	30	.207	36	.588	55
17800.00	.420	158,	.200	26	.180	34	.651	66
18000.00	.563	171	.146	31	.136	42	.680	79

REF PLANE EXT(CM): IN=10.92, OUT=10.92

### 8-STAGE PREAMP. WAFER #21

.00 VOLTS,	.00 MA (M	EAS 1)	<b>V D = 6</b>	ID=53MA/STAGE
FREQ	\$11	\$21	S12	\$22
(MHZ)	MAG ANG	MAG ANG	MAG ANG	MAG ANG
2000.000	.571 58	.011 144	.003 -122	.512 -1
2200.000	.508 61	.028 125	.005 -140	.494 3
2400.000	.452 61	.078 88	.006 171	.483 8
2600.000	.395 59	.233 54	.004 114	.488 13
2800.000	.339 55	.709 5	.002 57	.462 18
3000.000	.236 57	1.965 -59	.001 68	.430 29
3200.000	.212 114	3.429 -149	.003 130	.382 46
3400.000 3600.000	.656 111 .798 75	2.112 113 2.266 180	.017 111 .013 -44	.391 68 .634 83
3800.000	.412 49	4.143 94	.005 -50	.599 87 `
4000.000	.245 98	3.890 52	.003 -29	.645 96
4200.000	.354 122	3.866 17	.003 -0	.658 103
4400.000	.434 129	4.029 -18	.004 10	.641 111
4600.000	.488 133	4.112 -49	.005 19	.622 120
4800.000	.524 137	4.144 -78	.007 27	.606 131
5000.000	.543 140	4.087 -106	.010 33	.591 142
5200.000	536 143	3.985 -131	.015 38	.568 153
5400.000	490 146	3.759 -153	.024 32	.498 163
5600.000	.351 157	3.557 -168	.031 6	.404 -166
5800.000	.392 -173 .405 -167	4.211 172 4.408 145	.023 -15	.540 -144 .579 -135
6000.000 6200.000	.346 -159	4.428 121	.016 -9 .013 7	.579 -135 .542 -125
6400.000	.277 -147	4.429 100	.012 29	.467 -112
6600.000	.205 -131	4.478 80	.013 55	.376 -94
6800.000	.121 -112	4.789 59	.019 77	.270 -67
7000.000	.141 -28	5.264 29	.039 63	.411 -15
7200.000	.253 -56	4.310 4	.024 24	.434 -39
7400.000	.174 -81	4.727 -9	.015 35	.273 -35
7600.000	.093 -120	5.484 -35	.013 52	.134 -24
7800.000	.109 -159	5.882 -65	.014 54	.046 77
8000.000 8200.000	.173 -175 .248 174	6.079 -95 5.298 -134	.009 46 .007 63	.093 102 .080 134
8400.000	.263 169	4.893 -165	.006 76	.065 -179
8600.000	.241 168	4.383 165	.005 83	.101 -110
8800.000	.191 161	3.992 131	.004 71	.239 -89
9000.000	.071 130	3.233 88	003 -49	.386 -96
9200.000	.095 -41	1.823 43	.010 -128	.429 -111
9400.000	.192 -66	.740 11	.016 -150	.382 -119
9600.000	.277 -79	.220 -14	.023 -156	.351 -121
9800.000	.398 -95	.028 -137	.036 -159	.363 -119
10000.00	.573 -115	.112 163	.067 -171	.466 -112
10200.00	.744 -141	.122 140	.095 129	.709 -130
10400.00	.802 -169 .702 124	.110 159 .073 152	.032 101 .069 120	.597 -135 .576 -126
10500.00 19300.00	.075 161	.073 152 .167 -169	.012 164	.582 -111
11000.00	.080 -76	.170 179	.017 -161	.635 -95
11200.00	.184 -38	.159 179	.025 -142	.654 -79
11400.00	.289 -22	.150 -179	.032 -131	.688 -62
11300.00	.361 -7	.142 -175	.040 -120	.712 -43
11800.00	.409 8	.125 -171	.047 -110	.722 -25
12000.00	.412 23	.106 -159	.054 -97	.728 -6
12200.00	.360 45	.106 -159 C-1	<sup>14</sup> .068 -85	.736 12

12400.00	.358 75	.107 -121	.086 -77	.704 29
12600.00	.350 98	.121 -106	.104 -74	.663 45
12800.00	.307 118	.139 -97	.108 -71	.635 59
13000.00	.250 146	.155 -87	.115 -62	.606 70
13200.00	.245 179	.173 -80	.120 -54	.570 77
13400.00	.276 -157	.191 -72	.125 -39	.530 83
13600.00	.311 -144	.209 ~66	.156 -23	.462 86
13800.00	.326 -133	.232 -64	.209 -18	.360 89
14000.00	.343 -125	.241 -64	.256 -22	.258 105
14200.00	.368 -119	.222 -65	.262 -28	.245 130
14400:00	.382 -116	.186 -62	.230 -30	.281 138
14600.00	.390 -115	.147 ~52	.185 -25	.309 130
14800.00	.373 -116	.114 -29	.146 -5	.336 116
15000.00	.347 -122	.117 3	.160 24	.366 103
15200.00	.337 -131	.159 27	.220 40	.382 97
15400.00	.322 ~145	.233 34	.291 42	.362 94
15600.00	.244 -156	.278 31	.331 40	.286 91
15800.00	.112 ~138	.298 34	.343 43	.147 81
16000.00	.113 -78	.349 37	.383 45	.022 165
16200.00	.144 -46	.385 33	.421 43	.073 -125
16400.00	.170 -19	.392 28	.439 39	.086 -110
16600.00	.221 4	.381 26	.448 34	.051 -37
16800.00	.232 24	.367 23	.402 26	.179 20
17000.00	.237 54	.321 19	.321 23	.290 27
17200.00	.287 79	.254 19	.247 25	.412 37
17400.00	.267 97	.209 35	.212 44	.516 44
17600.00	.293 136	.233 43	.240 49	.593 52
17800.00	.425 159	.223 36	.219 42	.653 63
18000.00	.568 170	.154 36	.146 39	.676 76

REF PLANE EXT(CM): IN=10.92, OUT=10.92

.00 VOLTS,	1) AM 00.	IEAS 1)	VD=5	ID=54MA/STAGE
FREQ	S 1 1	<b>S21</b>	S12	\$22
(MHZ)	MAG ANG	MAG ANG	MAG ANG	MAG ANG
2000.000	.573 57	.012 144	.003 -119	.505 -1
2200.000	.512 61	.032 130	.005 -135	.485 2
2400.000	.458 61	.089 98	.006 176	.473 8
2600.000	.401 58	.275 68	.005 118	.479 13
2800.000	.348 54	.857 21	.003 59	.452 18
3000.000	.240 55	2.417 -42	.001 61	.418 29
3200.000	.217 114	4.181 -135	.003 129	.368 46
3400.000	.653 109	2.435 131	.017 109	.395 72
3600.000	.780 77	3.089 -164	.014 -45	.625 81
3800.000	.420 '50	5.270 109	.005 -51	.585 86
4000.000	.250 98	5.090 65	.003 -30	.626 96
4200.000	.359 123	4.799 27	.003 0	.643 103
4400.000	.443 130	4.917 -8	.004 11	.631 111
4600.000	.504 135	5.027 -40	.005 19	.613 121
4800.000	.550 139	5.094 -69	.007 26	.599 131
5000.000	.576 141	5.058 -96	.010 32	.587 142
5200.000	.571 143	4.923 -122	.014 37	.566 152
5400.000	.497 144	4.501 -144	.022 31	.492 162
5600.000	.358 163	4.355 -157	.029 9	.375 -168
5800.000	.428 -173	4.846 180	.023 -12	.516 -141
6000.000	.437 -167	5.083 152	.016 -8	.577 -133
6200.000	.381 -159	5.184 129	.013 7	.545 -124
6400.000	.310 -149	5.200 107	.011 27	.465 -111
6600.000	.233 -139	5.200 89	.015 22	.366 -94
6800.000	.115 -131	5.515 69	.018 78	.249 -65
7000.000	.185 -44	5.720 32	.038 65	.422 -7
7200.000	.165 -61 .115 -56	5.419 14	.024 23	.462 -36
7400.000 7600.000	.115 -56 .082 -64	5.701 -9 5.908 -33	.015 35	.286 -32
7800.000	.108 -123	5.908 -33 6.449 -59	.013 52 .013 54	.138 -20 .059 82
8000.000	.197 -173	6.767 -96	.009 47	.059 82 .117 102
8200.000	190 164	4.557 -142	.007 63	.104 126
8400.000	.208 165	4.342 -168	.006 77	.079 161
8600.000	.192 169	3.882 163	.005 89	.086 -127
8800.000	.150 167	3.544 132	.005 90	.207 -98
9000.000	050 154	2 022 97	.001 104	.330 -103
9209.000	.071 -38	1.923 57	.007 -148	.372 -113
9400.000	.170 -61	.926 26	.013 -160	.349 -121
9600.000	.255 -78	.324 2	.021 -162	.328 -124
	.377 -95		.033 -163	.344 -122
10000.00	.562 -116	.115 166	.066 -174	.451 -114
10200.00	.741 -141	.130 140	.094 126	.702 -132
10400.00	.821 -165	.111 158	.035 100	.596 -137
10600.00	.890 139	.071 163	.067 116	.575 -127
10800.00	.120 159	.188 -167	.013 158	.581 -112
11000.00	.084 -116	.192 -179	.017 -168	.631 -97
11290.00	.146 -53	.178 179	.024 -146	.646 -80
11400.00	.239 -29	.172 -180	.032 -135	.681 -63
11600.00	.307 -11	.159 -177	.039 -123	.705 -44
11800.00	.356 7	.142 -173	.046 -112	.716 -26
12000.00	.364 23	.117 -162	.054 -100	.721 -7 .
12200.00	.317 47	.107 -143 C-1	4.066 -88	.729 11

12400.00	.323	78	.120	-124	.084	-80	.701	28
12600.00	.310	103	.135	-111	.102	-75	.664	44
12800.00	.277	128	.152	-102	.108	-73	.633	58
13000.00	.256	158	.170	-92	.113	-65	.603	69
13200.00	.274	-174	.190	-85	.117	-56	.568	77
13400.00	.304	-155	.207	-78	.124	-40	.527	82
13600.00	.324	-142	.229	-73	.155	-26	.460	85
13800.00	.333	-131	.250	-72	.204	-21	.362	98
14000.30	.346	-124	.255	-73	.247	-24	.266	104
14200.00	.359	-118	.228	-73	.252	-30	.249	127
14400.00	.370	-115	.191	-70	.220	-32		134
14600.00	.376	-114	.145	-60	.177	-26	.305	126
14800.00	.354	-115	.110	-36	.139	-6	.334	112
15000.00	.326	-121	.117	- 1	.155	24	.369	100
15200.00	.320	-130	.161	- 20	.215	39	.387	95
15400.00	.308	-145	.219	26	.284	41	.365	93
15600.00	.224	-153	.257	28	.325	40	.292	91
15800.00	.137	-122	.305	35	.342	41	.161	84
16000.00	.137	-92	.364	33	.387	43	.034	133
16200.00	.126	-56	.395	29	.421	41	.057	-132
16400.00	.162	-18	.395	25	.432	36	.072	-107
16600.00	.221.	0	.400	24	.439	31	.055	-29
16800.00	.212	18	.396	20	.391	22	.184	20
17000.00	.207	55	.351	12	.306	20	.296	27
17200.00	÷ .263	82	.264	. 10	.235	23	.420	36
17400.00	.251	102	.223	27	.206	42	.520	43
17600.00	.290	139	.234	32	.231	46	.592	51
17800.00	.422	161	.210	29	.207	39	.650	63
18000.00	.580	171	.150	31	.137	38	.673	76

REF PLANE EXT(CM): IN=10.92, OUT=10.92

# ONR-21 PREAMP. CHARACTERIZATION 8 STAGE UNIT 2

2000,000 .523 -116 .012 -49 .002 78 .441 -168	75mA/s

### ONR-28 PREAMP. CHARACTERIZATION 8-STAGE

.00 VOLTS,	.00 MA (M	EAS 1)	V 1 = 4	V2=5.1 I=40MA/S
FREQ	S11	\$21	\$12	<b>S22</b>
(MHZ)	MAG ANG	MAG ANG	MAG ANG	MAG ANG
2000.000	.544 -119	.024 4	.000 -2	.542 -169
2500.000	.079 84	.852 126	.008 -69	.562 78
3000.000	.235 62	4.346 -155	.003 84	.445 -35
3500.000	.287 -49	8.217 -81	001 -17	.433 -166
4000.000	.439 132	7.217 57	.003 25	.693 132
4500.000	.439 -21	9.527 155	.001 -158	.504 -4
5000.000	.456 -89	4.943 -25	.017 -133	.521 -15
5500.000	.122 111	7.472 120	.003 136	465 -159
6000.000	.115 131	6.844 -81	.004 55	.460 102
6500.000	.166 23	5.497 84	.005 -29	.430 2 '
7000.000	.12839	4.621 -108	.007 -118	.320 -93
7500.000	.252 -109	3.924 53	.011 147	
8000.000	.281 143	2.525 -151	.015 51	1.152 111
8500.000	.200 60	1.153 9	.027 -60	.159 88
9000.000	.044 19	.410 -163	.018 -163	.279 -6
9500.000	.214 -51	.121 52	.035 93	
10000.00	.253 176	.061 -64	.046 -34	
10500.00	.265 20	.037 159	.038 -172	
11000.00	.137 -26	.107 -48	.060 21	.214 -78
11500.00	.441 -151	.100 54	.011 99	:.649 -154
12000.00	.570 110	.061 -47	.027 8	.685 102
12500.00	.576 15	.073 -148	.046 -110	.687 10
13000.00	.476 -77	.107 99	.078 128	.642 -86
13500.00	.366 -169	.140 -23	.110 1	:.563 169
14000.00	.263 73	.170 -143	.149 -119	.505 49
14500.00	.229 -79	.226 85	.218 103	.445 -66
15000.00	.252 109	.121 -48	.124 -38	:.520 -163
15500.00	.149 3	.134 -134	.124 -133	.618 89
16000.00	.116 -52	.132 98	.121 96	
16500.00	.155 -27	.074 -10	.035 -30	
17000.00	.251 -150	.093 -98	.073 -50	
17500.00	.109 83	.088 117	.092 155	
18000.00	.255 -172	.024 -126	.006 39	.450 -130

REF PLANE EXT(CM): IN= .00, OUT= .00

APPENDIX D
STAGE AMPLIFIER TEST DATA

The gain of each amplifier was determined by measuring the transmission coefficient ( $S_{21}$ ) in a 50 system. The input power level was -30 dBm. The measured gain as a function of frequency is shown in Figures D1-D6. In general, the gain is highest at 2 GHz and decreases to 0 dB at 9 GHz. The maximum gain measured was 35 dB, however, the data (Figure D-2) indicate that the measurement system saturated at that level. The bias conditions for each measurement are listed in Table D-1.

Noise figure data are given in Table D-2. The noise figure and associated gain were measured at 6 GHz. The amplifiers have a noise figure of 7 dB with 20 dB of associated gain. The corresponding bias conditions for minimum noise are also given in Table D-2. Note that the gain spectrum for ONR-38 1-5 as biased for minimum noise figure is included as Figure D-4.

Table D-1. Bias Conditions for ONR Amplifiers During Gain Measurements

FIGURE NUMBER	1	2	3	4	5	6
AMPLIFIER	ONR-38 1-7	ONR-38 1-6	ONR-38 1-5	ONR-38 1-5	ONR-37 2-1	ONR-38 43-03
BIAS:						
Vd1	3	3	3	3	3	3
Idl	65	65	70	40	75	95
Vd2	3	3	4	3 ,	3.57	3
Id2	170	180	140	130	300	210
Vgl	-1.0	-1.0	-1.0	-1.8	-2.0	-0.2
Vg2	-1.0	-1.0	-1.0	-1.8	-2.0	~0.5
Vg3	-2.2	-1.7	-2.3	-2.3	-2.0	-1.2
Vg4	-1.7	-1.9	-1.8	-1.7	-2.0	-1.2
Vg5	-1.0	-1.0	-1.8	-1.8	-2.0	-1.2
Vg6	-1.2	-1.0	-1.6	-1.6	0.0*	-0.2
Vg7	-1.0	-1.0	-1.2	-1.2	-2.0	-0.7
Vg8	-1.0	-1.0	-1.7	-1.6	-2.0	-1.2

\*Gate is shorted. Do not apply gate bias.

Table D-2. Noise Figure and Associated Gain For ONR Amplifiers Measured at 6 GHz

			T
AMPLIFIER	ONR-38 1-6	ONR-38 1-5	ONR-38 1-7
NOISE FIGURE	6.9	6.7	7.1
ASSOCIATED GAIN	20.6	20.6	19.6
BIAS:			
Vd1	3	3	3
Idl	40	40	55
Vd2	3	3	4
Id2	165	130	150
Vg1	-1.6	-1.8	-1.2
Vg2	-1.4	-1.8	-1.5
Vg3	-1.8	-2.3	-2.5
Vg4	-2.0	-1.7	-1.7
Vg5	-1.0	-1.8	-1.7
Vg6	-1.0	-1.6	-1.1
Vg7	-1.0	-1.2	-1.0
Vg8	-1.0	-1.6	-1.0

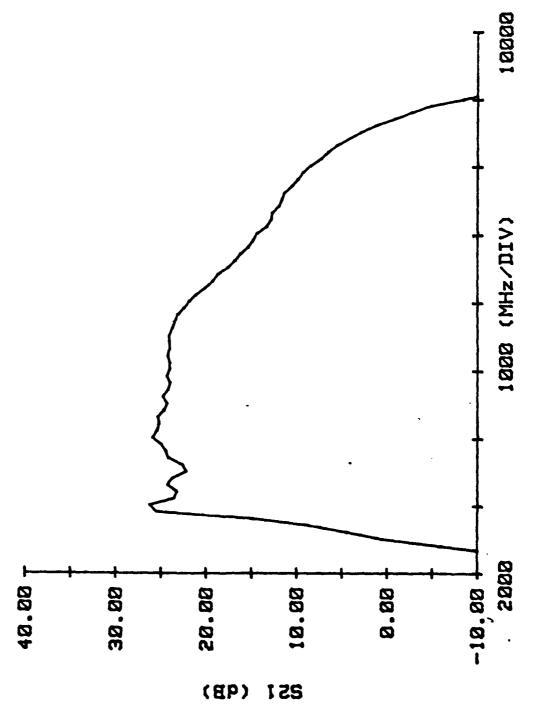


Figure D-2

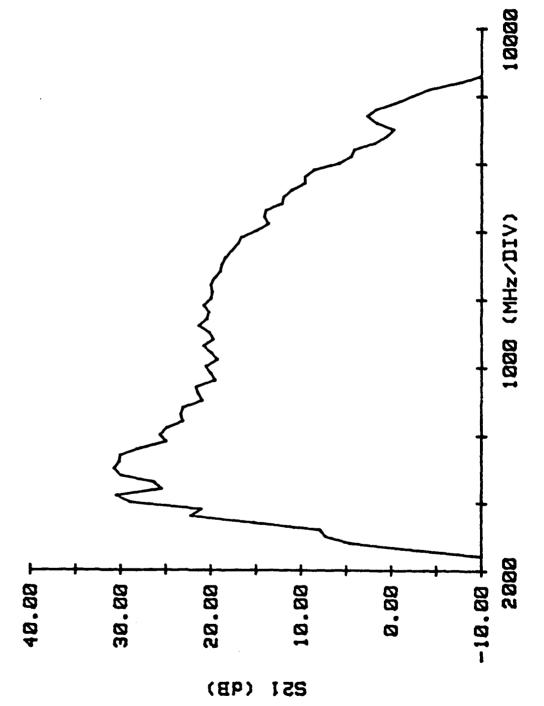
8 STAGE AMP RUN 3

1-6

**ONR-38** 

D-6

Figure D-3



8 STAGE AMP

ONR-38 1-5

#### ONR-37 2-1 8 STAGE RUN 3

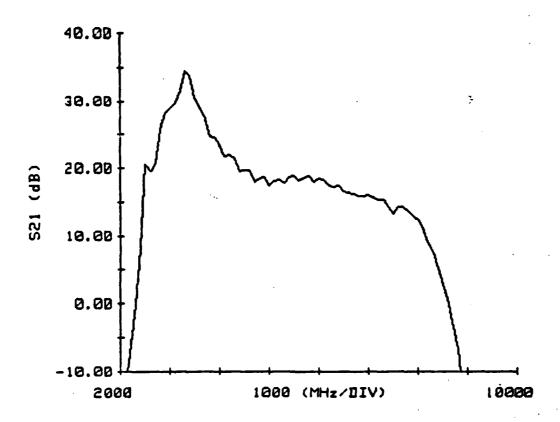
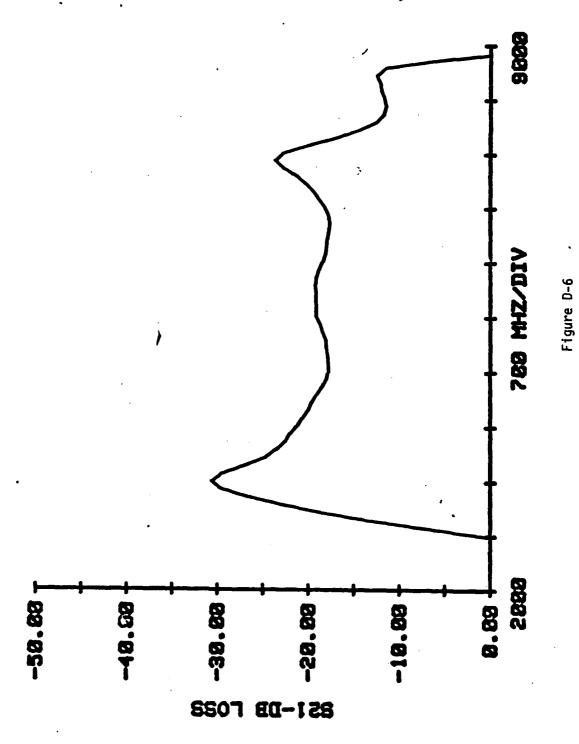


Figure D-5



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